Appendix E Revised Bank Assessment of Non-Point Source Consequences of Sediment at Siltronic Corporation Memorandum (January 27, 2022)



| To:   | File                      | Date:    | January 27, 2022 |
|-------|---------------------------|----------|------------------|
| From: | Michael R. Murray, RG, PE | Project: | 8128.02.04       |
|       | Jesse Hall, GIT           |          |                  |

RE: Revised Bank Assessment of Non-point Source Consequences of Sediment at Siltronic Corporation

This memorandum presents the results of an erosion potential assessment, conducted by Maul Foster & Alongi, Inc. (MFA), of the Willamette River bank adjacent to the Siltronic Corporation (Siltronic) property in Portland, Oregon. MFA used the Bank Assessment for Non-point Source Consequences of Sediment (BANCS) model to predict the erosion potential and channel stability of the riverbank. The BANCS model uses the quantitative assessment of the Bank Erosion Hazard Index (BEHI), developed by David L. Rosgen of Wildland Hydrology, Inc. (Rosgen, 2001). The BEHI is a procedure for assessing streambank erosion condition and potential. The U.S. Fish and Wildlife Service and the Oregon Department of Environmental Quality use the BEHI in the Portland Harbor to evaluate bank erosion potential. This assessment was originally finalized on August 29, 2016 and has been revised based on feedback provided by CDM Smith on behalf of the United States Environmental Protection Agency via electronic mail (CDM Smith, 2021). The results of this revised BANCS assessment are essentially the same as the results of the 2016 BANCS assessment both of which determined BEHI erosion potential adjective ratings of "very low" or "low" for all transects along the Siltronic riverbank.

### **ASSESSMENT METHODS**

On May 5, 2016, personnel from MFA conducted a survey of the riverbank along the Siltronic property adjacent to the Willamette River to obtain the site-specific data of the current bank conditions necessary for completing the erosion assessment. The riverbank survey was conducted both on foot along the top of riverbank and in other accessible areas, as well as by boat to access the riverbank from the Willamette River.

The BEHI was assessed along 12 transects spaced at 200-foot intervals along the riverbank. Figure 1 shows the location of the 12 transects. The elevation profiles of transects 1 through 4, 5 through 8, and 9 through 12 are presented in Figures 2, 3, and 4, respectively. Representative photographs of the bank conditions are provided in Attachment 1.

To evaluate the BEHI, MFA conducted a visual inspection of the riverbank transects at high and low tide by boat to measure the following characteristics:

- Bank height
- Bankfull height
- Root density and depth
- Type of surface protection (e.g., boulders, cobbles, sand, gravel, silt/clay)
- Vegetation
- Bank angle
- Condition of bank materials

A complete BEHI field sheet with ratings for each transect is provided in Attachment 2. The measured stream bank characteristics were converted to a risk rating system, to find the applied BEHI value for each bank characteristic (Rosgen, 2014). The assessment of the BEHI assigns point values to the following six characteristics:

- 1. Ratio of bank height to bankfull height
- 2. Ratio of root depth to bank height
- 3. Weighted root density
- 4. Bank angle
- 5. Surface protection
- 6. Bank material composition

The methods for determining each of these characteristics are described in the following subsections.

### Ratio of Study Bank Height to Bankfull Height

The ratio of study bank height to bankfull height requires the identification of the top of bank elevation, toe of slope elevation, bankfull stage elevation, and mean high water (MHW) level. Study bank height is defined as the top of bank elevation minus the toe of slope elevation. Bankfull height is defined as the bankfull stage elevation minus the toe of slope elevation. The toe of slope is defined as the first significant change in slope below the OHW but above the MHW level. If there is no geomorphic feature demonstrating a change in slope below the OHW but above the MHW, then the MHW from the Portland, Oregon Morrison Street Bridge gage was used as the toe of the slope for the BANCS model evaluation. Bankfull stage is defined as 'an established gage height at a given location along a river or stream, above which a rise in water surface will cause the river or stream to overflow the lowest natural stream bank somewhere in the corresponding reach'<sup>1</sup>. The opposite

<sup>&</sup>lt;sup>1</sup> National Weather Service Manual 10-950, Definitions and General Terminology. November 26, 2019. U.S. Department of Commerce, National Oceanic and Atmospheric Administration, National Weather Service. https://www.nws.noaa.gov/directives/

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river bank from the BANCS transect area is a large bluff of greater elevation, and as such this evaluation will use top of bank elevation as the bankfull stage at each transect location.

### Root Depth Ratio and Weighted Root Density

Root depth is the ratio of average plant root depth to the bank height, expressed as a percent (e.g., roots extending 10 feet into a 20-foot-tall bank = 0.50). Because of a lack of exposed roots, the root depth was estimated based on reference values for the rooting depth of the plant species present along the bank.

Root density is the proportion of the streambank surface covered by plant roots, expressed as a percent. Rooting density was estimated with the percentage of vegetation on bank. Weighted root density was found by multiplying root depth ratio and root density.

### **Bank Angle**

Bank angle is the angle of the bank from the top of bank elevation to the toe of slope elevation. Bank angle was calculated at each transect using the elevation profile of the bank (Figures 2 through 4).

### Surface Protection

Surface protection is the amount of stream bank covered by plant roots, logs, branches, rocks, etc. expressed as a percent. This was visually estimated for each transect.

### **Bank Material Composition**

Elements of the bank material composition assessed in the field included the grain size distribution of the bank material and the presence of stratification. The bank along the entire shoreline of the Siltronic property is covered with riprap; no stratified materials are exposed in the bank. Due to the relatively uniform coverage of riprap along the bank, grain size distribution for the bank materials was measured by choosing an area (about 1 meter square) representative of the 200-foot-long bank segments between transects.

The following Bank Material Adjustment was applied in the BEHI calculation:

- Bedrock (overall very low BEHI)
- Boulders: >10 inches (overall very low BEHI)
- Cobble: 2.5 inches to 10.1 inches (subtract 10 points of uniform medium to large cobble)
- Gravel or Composite Matrix (add 5 to 10 points, depending on percentage of bank material that is composed of sand)
- Sand: 0.04 inch to 0.2 inch (add 10 points)
- Silt/Clay: 0.0002 inch to 0.04 inch (no adjustment)

### **BEHI RATING METHODS**

The sum of the six bank characteristics (ratio of bank height to bankfull height, ratio of root depth to bank height, weighted root density, bank angle, surface protection, and bank material composition adjustment) was applied to the BEHI scale (Attachment 2) to determine the rating for each transect. All transects and corresponding BEHI ratings are summarized in Table 1.

The total BEHI value of each transect can be correlated with the BEHI adjective ratings on the following table:

| Total BEHI | BEHI adjective rating |
|------------|-----------------------|
| 5–9.5      | Very Low              |
| 10–19.5    | Low                   |
| 20–29.5    | Moderate              |
| 30–39.5    | High                  |
| 40–45      | Very High             |
| 46–50      | Extreme               |

### CHANNEL STABILITY

The channel stability characteristics were also recorded at each transect and used to assign a channel stability rating for each transect (Rosgen, 2001). The channel stability assessment categories and criteria for assigning channel stability ratings are shown in Table 2. The channel stability ratings for each transect are summarized in Table 3.

The following 15 channel stability characteristics were assessed at each transect:

- 1. Landform slope
- 2. Mass erosion
- 3. Debris jam potential
- 4. Vegetative bank protection
- 5. Channel capacity
- 6. Bank rock content
- 7. Obstructions to flow
- 8. Cutting
- 9. Deposition
- 10. Rock angularity
- 11. Brightness
- 12. Consolidation of particles
- 13. Bottom size distribution
- 14. Scouring and deposition
- 15. Aquatic vegetation

### RESULTS

### **BEHI Ratings**

Overall, the physical characteristics (bank material, surface protection, slope, root density, bankfull ratios, etc.) of the Siltronic bank were generally uniform at all 12 transects. BEHI results from each transect are provided in Table 1 and summarized below:

- The study bank height to bankfull height ratio was uniform with a corresponding risk rating of "very low" (1.0 BEHI).
- Root depth to study bank height ratio BEHI risk ratings were "moderate" to "high," depending on placement of mature trees along the top of bank (4.2 to 7.0 BEHI).
- Because of lack of vegetation along the bank, weighted root density was rated as "moderate/high" to "extreme" (5.9 to 9.5 BEHI).
- The bank angles (slopes) of all transects ranged between 22 and 25.7 degrees as measured from the top of bank to toe of slope, and scored a BEHI risk rating of "low."
- Surface protection was uniform along the entire bank, with approximately 95 percent coverage and a BEHI risk rating of "very low." The approximate 5 percent of unprotected surface consists of localized sediment deposits along the OLW.
- Bank material along all transects was found to be cobbles to boulders. The presence of uniform cobbles and boulders along the entire bank resulted in a bank material adjustment of -10 points for the total BEHI score for each transect.

The total BEHI model scores for all transects ranged between 3.8 and 10.2 with adjective ratings of "very low" to "low". See Table 1 for BEHI transect summary.

### Channel Stability

The channel stability characteristics were found to be generally uniform in all transects surveyed and resulted in overall channel stability scores of 42 to 48, corresponding to an overall channel stability rating of "good and stable" for all transects. See Table 3 for the channel stability summary.

### REFERENCES

CDM Smith. 2021. Electronic mail (re: Request for Clarification - EPA Comment #36 on Gasco Sediments Site Combined BOD-PDR) from L. Peterson, CDM Smith to R. Barth, Anchor QEA. December 21.

National Weather Service Manual 10-950, Definitions and General Terminology. November 26, 2019. U.S. Department of Commerce, National Oceanic and Atmospheric Administration, National Weather Service. Available at: <u>https://www.nws.noaa.gov/directives/</u>

Rosgen, D. L. 2001. A practical method of computing streambank erosion rate. Vol. 2, pp. 9-15. Proceedings of the 7th Federal Interagency Sedimentation Conference, March 25, Reno, Nevada.

Rosgen, D. L. 2014. River stability field guide. 2d ed. Wildland Hydrology.

### ATTACHMENTS

Figures

- 1 Riverbank Transect Locations
- 2 Riverbank Transects 1–4
- 3 Riverbank Transects 5–8
- 4 Riverbank Transects 9–12

### Tables

- 1 BEHI Transect Summary
- 2 Channel Stability Ratings
- 3 Channel Stability Summary

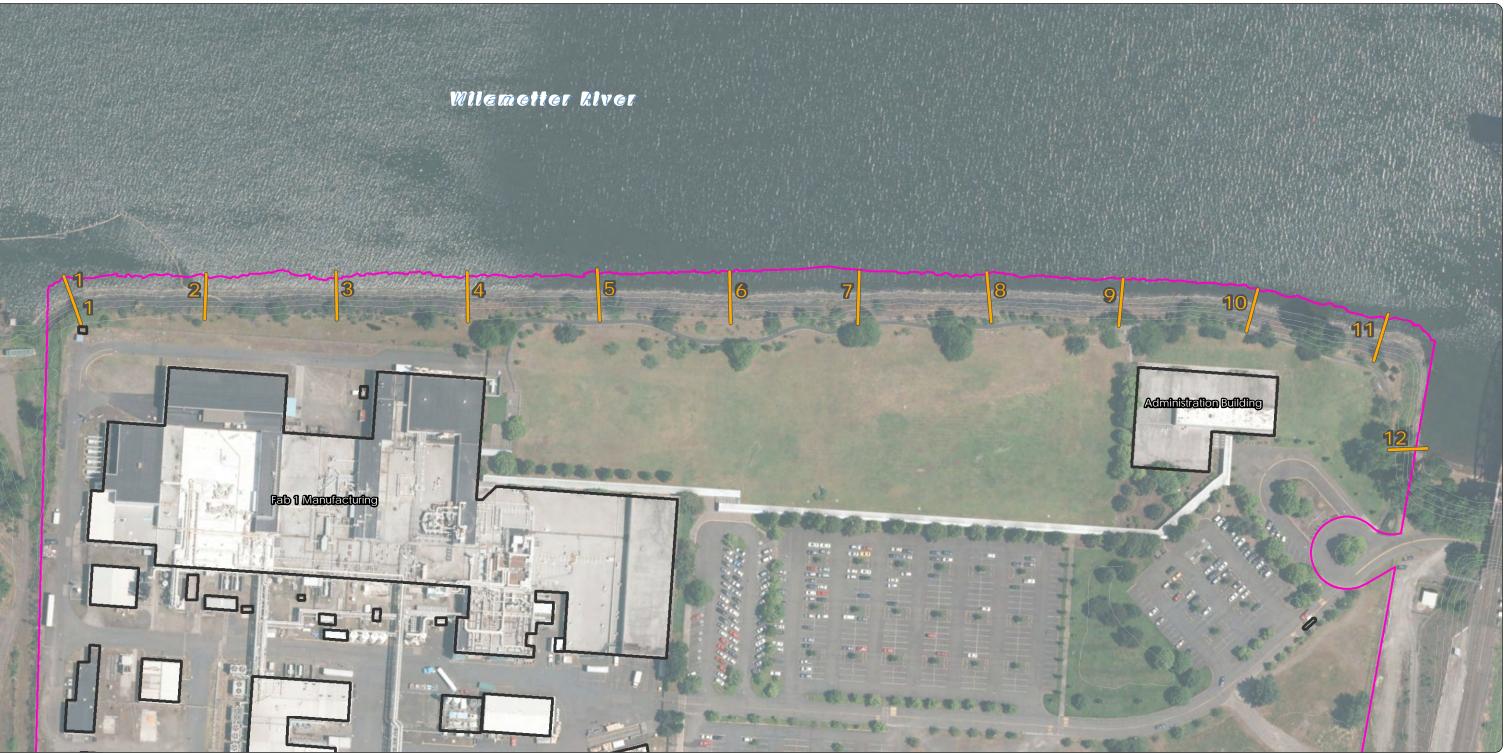
Attachment 1 Photographs

Attachment 2 BEHI Field Data Sheets

Attachment 3 NOAA Datums for 9439221 (Portland, Oregon, Morrison St. Bridge)

# FIGURES





NOTE: NAVD88 = North Americal Vertical Datum of 1988.

Source: Aerial photograph (2012) obtained from City of Portland; elevations obtained from 2005 Columbia River dataset, Puget Sound LiDAR Consortium.



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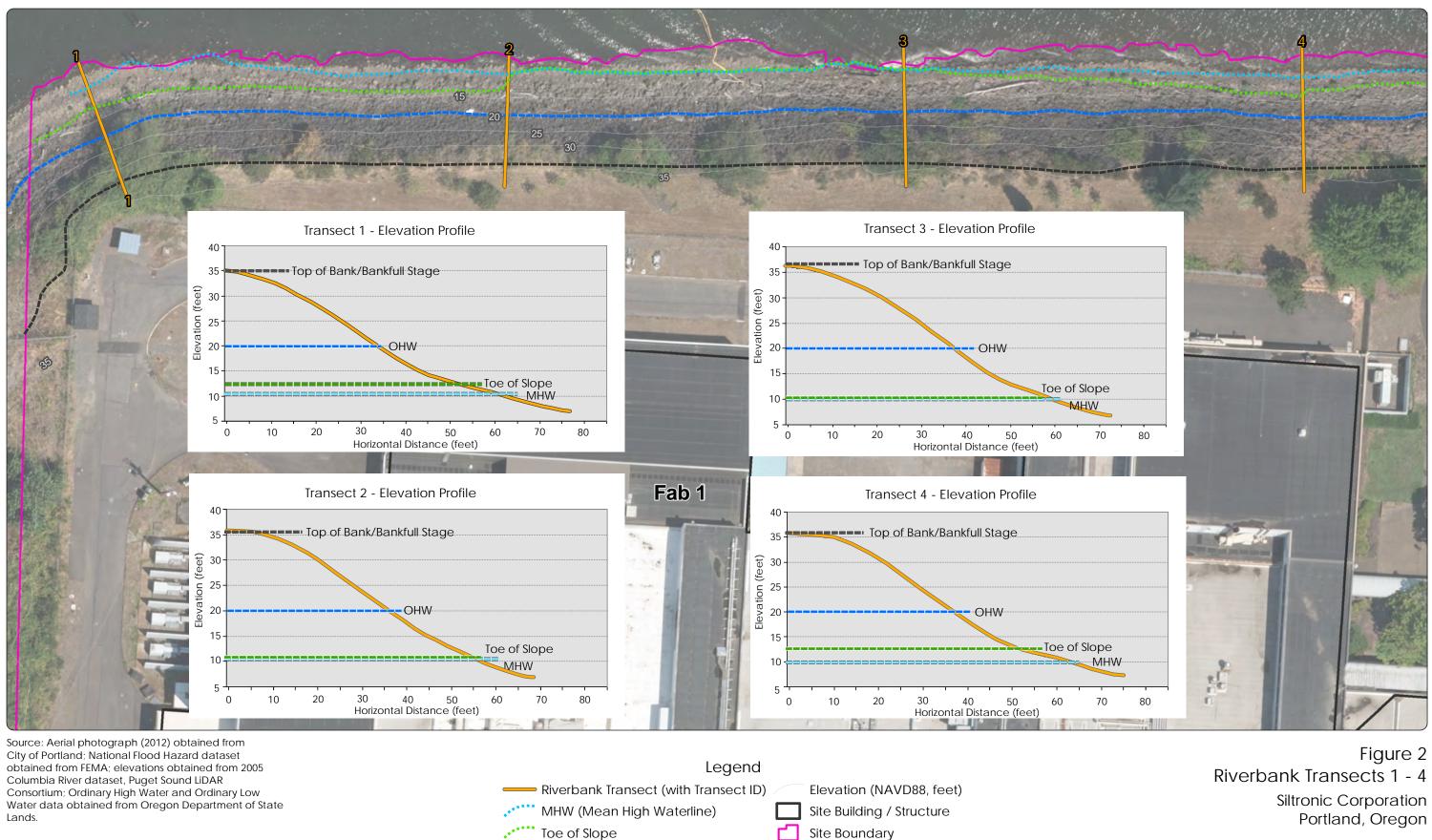
Legend —— Riverbank Transect (with Transect ID) Elevation (NAVD88, feet)

Site Boundary

## Figure 1 Riverbank Transect Locations

Siltronic Corporation Portland, Oregon







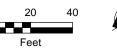
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Note: NAVD88 = North American Vertical Datum of 1988.

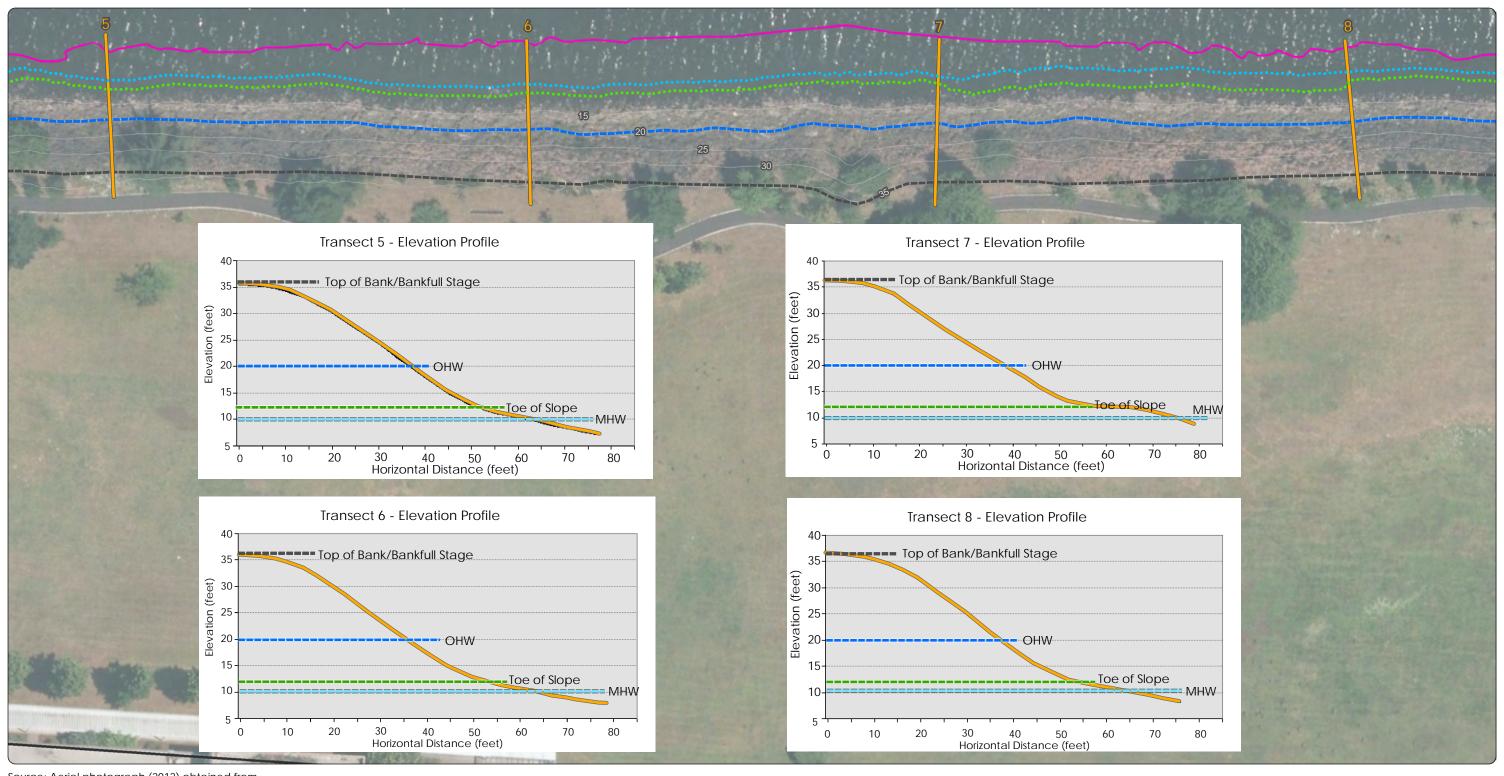
Toe of Slope

Top of Bank

Ordinary High Water







Source: Aerial photograph (2012) obtained from City of Portland; National Flood Hazard dataset obtained from FEMA; elevations obtained from 2005 Columbia River dataset, Puget Sound LiDAR Consortium; Ordinary High Water and Ordinary Low Water data obtained from Oregon Department of State Lands.



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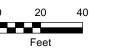
Note: NAVD88 = North American Vertical Datum of 1988.

### Legend

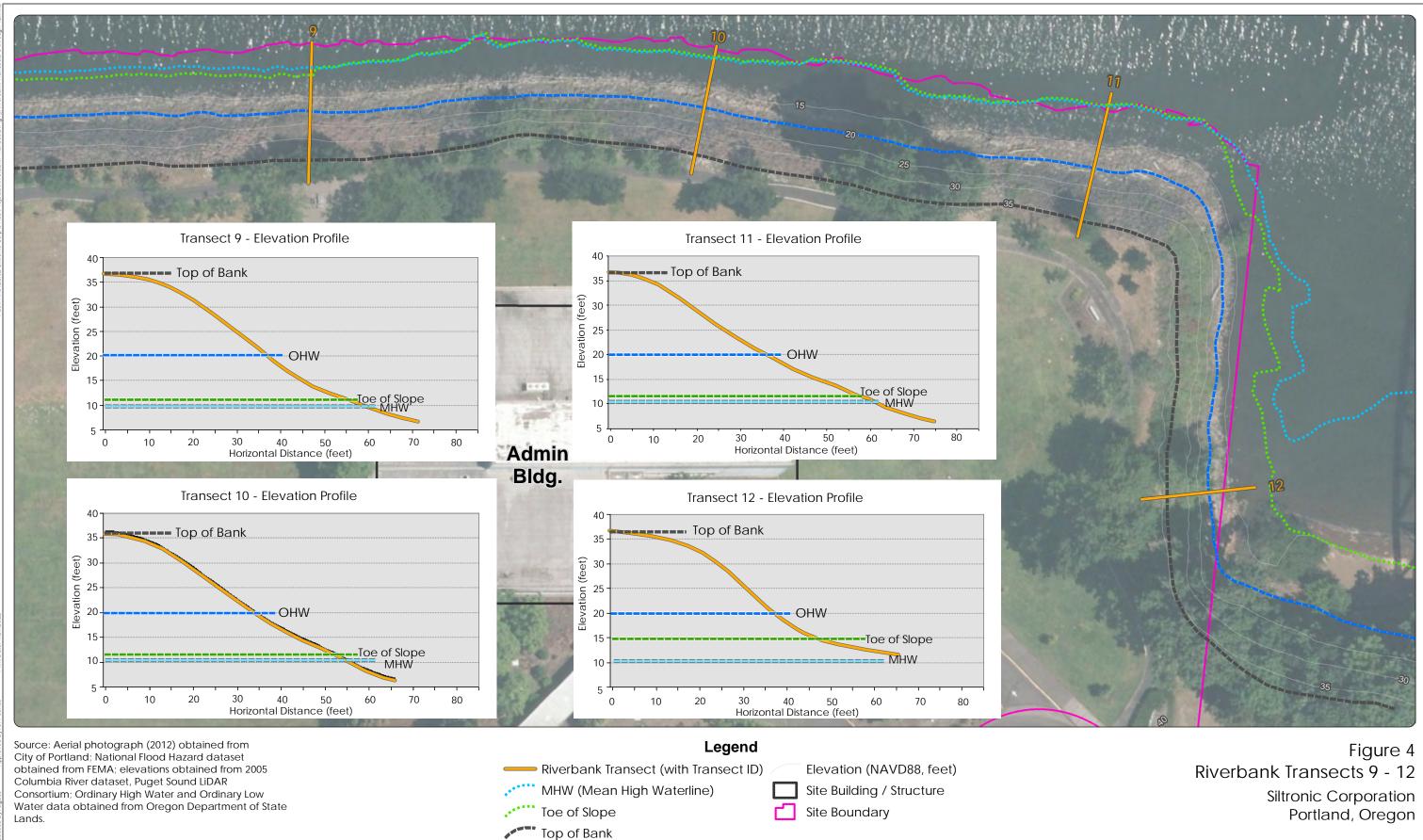
Ordinary High Water

- Riverbank Transect (with Transect ID)
  Elevation (NAVD88, feet)
  MHW (Mean High Waterline)
  Toe of Slope
  Site Building / Structure
  Site Boundary
  - undary

Figure 3 Riverbank Transects 5 - 8 Siltronic Corporation Portland, Oregon







Ordinary High Water



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Note: NAVD88 = North American Vertical Datum of 1988.





# TABLES



### Table 1 BEHI Transect Summary Siltronic Portland, Oregon

|   | Transect<br>1 | Transect<br>2 | Transect<br>3 | Transect<br>4 | Transect<br>5 | Transect<br>6 | Transect<br>7 | Transect<br>8 | Transect<br>9 | Transect<br>10 | Transect<br>11 | Transect<br>12 |
|---|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|----------------|----------------|----------------|
| Study bank height to<br>bankfull height ratio | 1             | 1             | 1             | 1             | 1             | 1             | 1             | 1             | 1             | 1              | 1              | 1              |
| BEHI  | 1             | 1             | 1             | 1             | 1             | 1             | 1             | 1             | 1             | 1              | 1              | 1              |
| Root depth to study bank<br>height ratio      | 0.22          | 0.19          | 0.19          | 0.21          | 0.21          | 0.19          | 0.42          | 0.2           | 0.37          | 0.19           | 0.19           | 0.45           |
| BEHI  | 6.9           | 7             | 7             | 7             | 7             | 7             | 4.2           | 7             | 5             | 7              | 7              | 4.2            |
| Weighted root density                         | 10.94         | 4.83          | 9.48          | 5.32          | 10.42         | 4.84          | 20.83         | 10            | 18.62         | 4.66           | 9.31           | 31.82          |
| BEHI  | 9             | 9.5           | 8.8           | 9.3           | 8.5           | 9.5           | 7             | 8.6           | 7.8           | 9.5            | 8.5            | 5.9            |
| Bank angle                                    | 24.5          | 25.2          | 24.7          | 25.2          | 23.9          | 22            | 22.8          | 25.7          | 24.9          | 25.6           | 24.1           | 25.1           |
| BEHI  | 2.1           | 2.2           | 2.1           | 2.2           | 2.2           | 2.1           | 2.1           | 2.1           | 2.2           | 2.2            | 2.2            | 2.2            |
| Surface protection                            | 95%           | 95%           | 95%           | 95%           | 95%           | 95%           | 95%           | 95%           | 95%           | 95%            | 95%            | 95%            |
| BEHI  | 0.5           | 0.5           | 0.5           | 0.5           | 0.5           | 0.5           | 0.5           | 0.5           | 0.5           | 0.5            | 0.5            | 0.5            |
| Total BEHI Score                              | 19.5          | 20.2          | 19.4          | 20            | 19.2          | 20.1          | 14.8          | 19.2          | 16.5          | 20.2           | 19.2           | 13.8           |
| Bank material adjustment<br>(Cobbles -10)     | -10           | -10           | -10           | -10           | -10           | -10           | -10           | -10           | -10           | -10            | -10            | -10            |
| Total BEHI with adjustment                    | 9.5           | 10.2          | 9.4           | 10            | 9.2           | 10.1          | 4.8           | 9.2           | 6.5           | 10.2           | 9.2            | 3.8            |
| BEHI adjective rating                         | Very Low      | Low           | Very Low      | Low           | Very Low      | Low           | Very Low      | Very Low      | Very Low      | Low            | Very Low       | Very Low       |
| NOTE:   | •             |               | •             |               | •             |               |               |               | •             |                | •              |                |
| BEHI = bank erosion hazard ind                | ex.           |               |               |               |               |               |               |               |               |                |                |                |

#### Table 2 Channel Stability Ratings Siltronic Portland, Oregon

| Stream:        | Willam  | ette R  | iver      |                       |                          |  | Loc        | ation:   | Portla | and, O  | regon                                     |   |   | Valley   | Type:   |  |             | Obse  | ervers:    | Justi   | n Pour   | ds                     |                       |                        | Date:  |         |
|----------------|---------|---|-----------|-----------------------|--------------------------|--|------------|----------|--------|---|---|---|---|--|---------|--|-------------|---|------------|---|--|------------------------|-----------------------|------------------------|--|---------|
| Loca-tion      | Key     | Cate  | gory      | Excellent             |                          |  |            |          | Good   |   |   |   | Fair                                      |  |         |  |             | Poor  |            |   |  |                        |                       |                        |  |         |
| Loca-tion      | Rey     | Cale  | gory      |                       | [                        | Descriptio                                 | n          |          | Rating |   | [   | Descriptic                                  | on  |  | Rating  |  | I           | Descriptio  | n          |   | Rating   |                        |                       | Desc                   | ription  | Rati    |
|                | 1       | Landfor<br>slope  | m         | Bank sl               | ope grad                 | dient <30                                  | )%.        |          | 2      | Bank sl   | ope grad                                  | dient 30-                                   | -40%.                                     |  | 4       | Bank sl  | ope gra     | dient 40-   | -60%.      |   | 6  | Bank slo               | pe gra                | dient >                | 60%.   | 8       |
| banks          | 2       | Mass e  | rosion    | No evid<br>erosion    |                          | past or f                                  | uture ma   | ass      | 3      | Infrequent. Mostly healed over. Low future potential.   |   |   | _ow                                       | 6  |         | nt or larg<br>rearlong   | ge, causi   | ng sedir  | ment       | 9   | Frequent or large, causi<br>yearlong OR imminent o |                        |                       |                        | / 12   |         |
| Upper          | 3       | Debris<br>potentia  |           | Essenti<br>channe     |                          | ent from                                   | immedia    | ate      | 2      | Present<br>limbs.                                       | t, but mc                                 | ostly sma                                   | all twigs a                               | and  | 4       | Modera<br>larger s   |             | avy amo   | unts, m    | ostly   | 6  | Moderate<br>larger siz |                       | avy am                 | ounts, predominant   | y 8     |
| 'n             | 4       | Vegeta<br>bank pr   |           |                       |                          | nsity. Vig<br>, dense,                     |            |          | 3      |   |   |   | species<br>e or dee                       |  | 6       |  | from a      | /. Lower<br>shallow,                                    |            |   | 9  | vigor ind<br>shallow r | icating<br>root ma    | poor, d<br>ass.        | er species and less<br>liscontinuous, and  | 12      |
|                | 5       | Channe<br>capacit   |           | Width/dep             | oth ratio de             | ent to conta<br>parture fro<br>I.0. Bank-H | m referenc | e        | 1      | Width/dep   | oth ratio de<br>th ratio = 1              | ntained with<br>eparture fro<br>1.0–1.2. Ba | hin banks.<br>om referenc<br>unk-Height f | e<br>Ratio   | 2       | departure  | from refer  | contained<br>rence width<br>nt Ratio (Bl                | /depth rat | io =  | 3  | common w               | ith flows<br>rom refe | less than<br>rence wid | d; over-bank flows are<br>bankfull. Width/depth rat<br>lth/depth ratio > 1.4. Bank |         |
| Jks            | 6       | Bank ro<br>content  |           | > 65% \<br>commo      |                          | e angula                                   | r boulde   | rs. 12"+ | 2      | 40–65%<br>cobbles                                       |   | y boulde                                    | rs and sr                                 | nall   | 4       | 20–40%<br>class.   | 6. Most i   | n the 3–  | 6" diam    | eter  | 6  | <20% ro<br>less.       | ck frag               | ments o                | of gravel sizes, 1–3   | or 8    |
| -ower banks    | 7       | Obstrue<br>flow   | ctions to |                       |                          | firmly in<br>ing or de                     |            |          | 2      | currents  |   | or pool fill                                | sive cross<br>ing. Obsti                  |  | 4       |  | th high flo | ent, unsta<br>ows caus                                  |            |   | 6  |                        | sion ye               | earlong.               | and deflectors cause<br>Sediment traps full,<br>urring.                            |         |
| Гом            | 8       | Cutting   |           | Little or             | none. Ir                 | nfrequent                                  | t raw bar  | nks <6". | 4      |   |   |   | outcurves<br>s may be                     |  | 6       |  |             | s 12–24'<br>sloughir                                    |            |   | 12   | Almost c<br>Failure o  |                       |                        | ts, some over 24" high.<br>frequent.   |         |
|                | 9       | Deposi  | ion       | Little or<br>point ba |                          | rgement                                    | of chanr   | nel or   | 4      | Some new bar increase, mostly from coarse gravel.       |   |   | 8   | Moderate depostion of new gravel and coarse sand on old and some new bars. |         |  | 12          | Extensive deposit of prece<br>particles. Accelerated ba |            |   | ,  | 16                     |                       |                        |  |         |
|                | 10      | Rock a  | ngularity | Sharp e<br>surface    |                          | nd corner                                  | rs. Plane  | •        | 1      | Rounded corners and edges. Surfaces<br>smooth and flat. |   |   | 2   | Corners and edges well-rounded in two dimensions.                          |         |  | 3           | Well-rou<br>smooth.                                     | nded ir    | nensions, surfaces                                  | 4  |                        |                       |                        |  |         |
|                | 11      | Brightn   | ess       |                       | es dull, d<br>Ily not bi | ark, or si<br>right.                       | tained.    |          | 1      | Mostly dull, but may have <35% bright surfaces.         |   |   | 2   | Mixture<br>mixture   |         | l bright, i  | .e., 35–    | 65%   | 3          | Predomi<br>scoured                                  |  |                        | > 65%, exposed or     | 4                      |  |         |
| Ę              | 12      | Consolio<br>particle  |           | Assorte<br>overlap    |                          | tightly pa                                 | acked or   |          | 2      | Moderately packed with some<br>overlapping.             |   |   |   |  | 4       | Mostly loose assortment with no apparent overlap. 6  |             |   | 6          | No packing evident. Loose assortment, easily moved. |  |                        |                       | sily 8                 |  |         |
| Bottom         | 13      | Bottom<br>distribu  |           | No size<br>80–100     |                          | evident.                                   | . Stable r | material | 4      | Distribution shift light. Stable material 50–80%.       |   |   |   |  | 8       | Moderate change in sizes. Stable    12      materials 20–50%.    12      30–50% affected. Deposits and scour    12 |             |   |            | 12  | Marked distribution change. Stable n<br>0–20%.     |                        |                       |                        | als 16   |         |
|                | 14      | Scourin<br>deposit  |           | <5% of<br>depositi    |                          | affected                                   | by scour   | ror      | 6      | and wh  |   | les steep                                   | at constr<br>pen. Som                     |  | 12      | at obstr   | uctions,    |   | tions, ar  |   | 18   | More tha<br>or chang   |                       |                        | bottom in a state of<br>ong.   | flux 24 |
|                | 15      | Aquatic<br>vegetat  |           |                       |                          |  |            |          |        |   | e or absent. Yellow-<br>m may be present. | 4   |   |  |         |  |             |   |            |   |  |                        |                       |                        |  |         |
|                |         |   |           |                       |                          | Exc  | ellent 1   | Fotal =  |        |   |   |   | Good 1                                    | Fotal =  |         |  |             |   | Fair       | Total =   |  |                        |                       |                        | Poor Tota  | 1 =     |
| Stream type    | )       | A1  | A2        | A3                    | A4                       | A5   | A6         | B1       | B2     | B3  | B4  | B5  | B6  | C1   | C2      | C3   | C4          | C5  | C6         | D3  | D4   | D5                     | D6                    | ]                      | Grand Total  | - 1     |
| Good (Stable)  |         | 38-43   | 38-43     | 54-90                 | 60-95                    | 60-95                                      | 50-80      | 38-45    | 38-45  | 40-60   | 40-64                                     | 48-68                                       | 40-60                                     | 38-50  | 38-50   | 60-85  | 70-90       | 70-90   | 60-85      | 85-107  | 85-107   | 85-107                 | 67-98                 |                        | Grand Total  | -       |
| air (Mod. uns  | stable) | 44-47   | 44-47     | 91-129                | 96-132                   | 96-142                                     | 81-110     | 46-58    | 46-58  | 61-78   | 65-84                                     | 69-88                                       | 61-78                                     | 51-61  | 51-61   | 86-105   | 91-110      | 91-110  | 86-105     | 108-132   | 108-132  |                        | 99-125                |                        | Existing   |         |
| Poor (Unstable |         | 48+   | 48+       | 130+                  | 133+                     | 143+                                       | 111+       | 59+      | 59+    | 79+   | 85+                                       | 89+   | 79+                                       | 62+  | 62+     | 106+   | 111+        | 111+  | 106+       | 133+  | 133+   | 133+                   | 126+                  | ]                      | Stream Type  | =       |
| Stream type    | )       | DA3   | DA4       | DA5                   | DA6                      | E3   | E4         | E5       | E6     | F1  | F2  | F3  | F4  | F5   | F6      | G1   | G2          | G3  | G4         | G5  | G6   |                        |                       |                        | *Potential   |         |
| Good (Stable)  |         | 40-63   | 40-63     | 40-63                 | 40-63                    | 40-63                                      | 50-75      | 50-75    | 40-63  | 60-85   | 60-85                                     | 85-110                                      | 85-110                                    | 90-115   | 80-95   | 40-60  | 40-60       | 85-107  | 85-107     | 90-112  | 85-107   |                        |                       |                        | Stream Type  |         |
| air (Mod. uns  | ,       | 64-86   | 64-86     | 64-86                 | 64-86                    | 64-86                                      | 76-96      | 76-96    | 64-86  | 86-105  | 86-105                                    | 111-125                                     |   | 116-130  | 96-110  | 61-78  | 61-78       | 108-120   |            | 113-125   | 108-120  |                        |                       |                        | Modified c   |         |
| Poor (Unstable | e)      | 87+    87+    87+    87+    97+    97+    87+    106+    126+    131+    111+    79+    79+    121+ |           |                       |                          |  |            |          |        |   |   |   |   |  |         |  |             |   |            |   |  |                        |                       |                        |  |         |
|                |         |   |           |                       |                          |  |            |          |        |   |   |   |   | *Rati  | ng is a | djusted  | l to po     | tential   | stream     | n type,   | not exi  | sting str              | ream t                | ype                    |  |         |

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Worksheet 3-10. Pfankuch (1975) channel stability rating procedure, as modified by Rosgen (1996, 2006b). River Stability Field Guide pages 3-46 to 3-47

### Table 3 Channel Stability Summary Siltronic Portland, Oregon

|              |                   | Up              | per Banks               |                                  | Lower Banks         |                      |                         |         |            |                    |            | ]                             |                             |                               |                       |       |                             |
|--------------|-------------------|-----------------|-------------------------|----------------------------------|---------------------|----------------------|-------------------------|---------|------------|--------------------|------------|-------------------------------|-----------------------------|-------------------------------|-----------------------|-------|-----------------------------|
| Transect No. | Landform<br>slope | Mass<br>erosion | Debris jam<br>potential | Vegetative<br>bank<br>protection | Channel<br>capacity | Bank rock<br>content | Obstructions<br>to flow | Cutting | Deposition | Rock<br>angularity | Brightness | Consolidation<br>of particles | Bottom size<br>distribution | Scouring<br>and<br>deposition | Aquatic<br>vegetation | Total | Channel Stability<br>Rating |
| 1            | 2                 | 3               | 2                       | 9                                | 1                   | 2                    | 2                       | 4       | 4          | 1                  | 1          | 2                             | 4                           | 6                             | 2                     | 45    | Good (Stable)               |
| 2            | 2                 | 3               | 2                       | 12                               | 1                   | 2                    | 2                       | 4       | 4          | 1                  | 1          | 2                             | 4                           | 6                             | 2                     | 48    | Good (Stable)               |
| 3            | 2                 | 3               | 2                       | 9                                | 1                   | 2                    | 2                       | 4       | 4          | 1                  | 1          | 2                             | 4                           | 6                             | 2                     | 45    | Good (Stable)               |
| 4            | 2                 | 3               | 2                       | 12                               | 1                   | 2                    | 2                       | 4       | 4          | 1                  | 1          | 2                             | 4                           | 6                             | 2                     | 48    | Good (Stable)               |
| 5            | 2                 | 3               | 2                       | 9                                | 1                   | 2                    | 2                       | 4       | 4          | 1                  | 1          | 2                             | 4                           | 6                             | 2                     | 45    | Good (Stable)               |
| 6            | 2                 | 3               | 2                       | 12                               | 1                   | 2                    | 2                       | 4       | 4          | 1                  | 1          | 2                             | 4                           | 6                             | 2                     | 48    | Good (Stable)               |
| 7            | 2                 | 3               | 2                       | 9                                | 1                   | 2                    | 2                       | 4       | 4          | 1                  | 1          | 2                             | 4                           | 6                             | 2                     | 45    | Good (Stable)               |
| 8            | 2                 | 3               | 2                       | 9                                | 1                   | 2                    | 2                       | 4       | 4          | 1                  | 1          | 2                             | 4                           | 6                             | 2                     | 45    | Good (Stable)               |
| 9            | 2                 | 3               | 2                       | 9                                | 1                   | 2                    | 2                       | 4       | 4          | 1                  | 1          | 2                             | 4                           | 6                             | 2                     | 45    | Good (Stable)               |
| 10           | 2                 | 3               | 2                       | 12                               | 1                   | 2                    | 2                       | 4       | 4          | 1                  | 1          | 2                             | 4                           | 6                             | 2                     | 48    | Good (Stable)               |
| 11           | 2                 | 3               | 2                       | 9                                | 1                   | 2                    | 2                       | 4       | 4          | 1                  | 1          | 2                             | 4                           | 6                             | 2                     | 45    | Good (Stable)               |
| 12           | 2                 | 3               | 2                       | 6                                | 1                   | 2                    | 2                       | 4       | 4          | 1                  | 1          | 2                             | 4                           | 6                             | 2                     | 42    | Good (Stable)               |

Page 2 of 2

## ATTACHMENT 1 PHOTOGRAPHS





<u>Photo No.</u> 1

### **Description**

Looking southeast on top of bank near Transect #9.

### Photo No.

2

**Description** Looking northeast on top of bank near Transect #4.

### **PHOTOGRAPHS**

Project Name:Siltronic BaProject Number:8128.02.03Location:7200 NorthDeath1.00

Siltronic Bank Survey 8128.02.03 7200 Northwest Front Avenue Portland, Oregon





R:\8128.02 Siltronic Corp\Documents\04\_2022.01.27 BANCs Assessment Memo\Attachment 1\Att 1 - Photo Log - Siltronic BANC assessment.doc



Photo No. 3

**Description** Looking northwest from water of Transect #10.

### **PHOTOGRAPHS**

Project Name:Siltronic BaProject Number:8128.02.03Location:7200 North

Siltronic Bank Survey 8128.02.03 7200 Northwest Front Avenue Portland, Oregon





Photo No. 4

### **Description**

Trees on top of bank, looking west at Transect #10 from water.



Project Name: Project Number: 8128.02.03 Location:

Siltronic Bank Survey 7200 Northwest Front Avenue Portland, Oregon

### Photo No. 5

### **Description**

Panoramic view of bank.





Project Name: Project Number: 8128.02.03 Location:

Siltronic Bank Survey 7200 Northwest Front Avenue Portland, Oregon

### <u>Photo No.</u>

6

### **Description**

Looking west at Transect #3 from water.



## Photo No. 7

### **Description**

Looking west at Transect #5 from water.





Project Name:Siltronic BaProject Number:8128.02.03Location:7200 North

Siltronic Bank Survey 8128.02.03 7200 Northwest Front Avenue Portland, Oregon



<u>Photo No.</u> 8

**Description** Looking west at Transect #9 from water.



<u>Photo No.</u> 9

**Description** Looking west at Transect #11 from water.



Project Name:Siltronic BaProject Number:8128.02.03Location:7200 North

Siltronic Bank Survey 8128.02.03 7200 Northwest Front Avenue Portland, Oregon



<u>Photo No.</u> 10

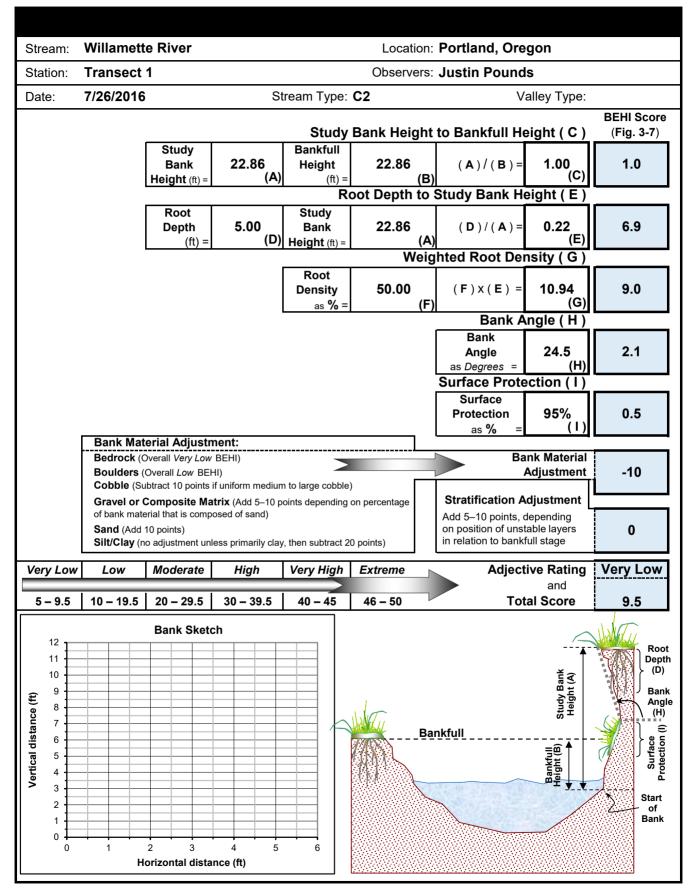
### **Description**

Looking west at Transect #12 from water.



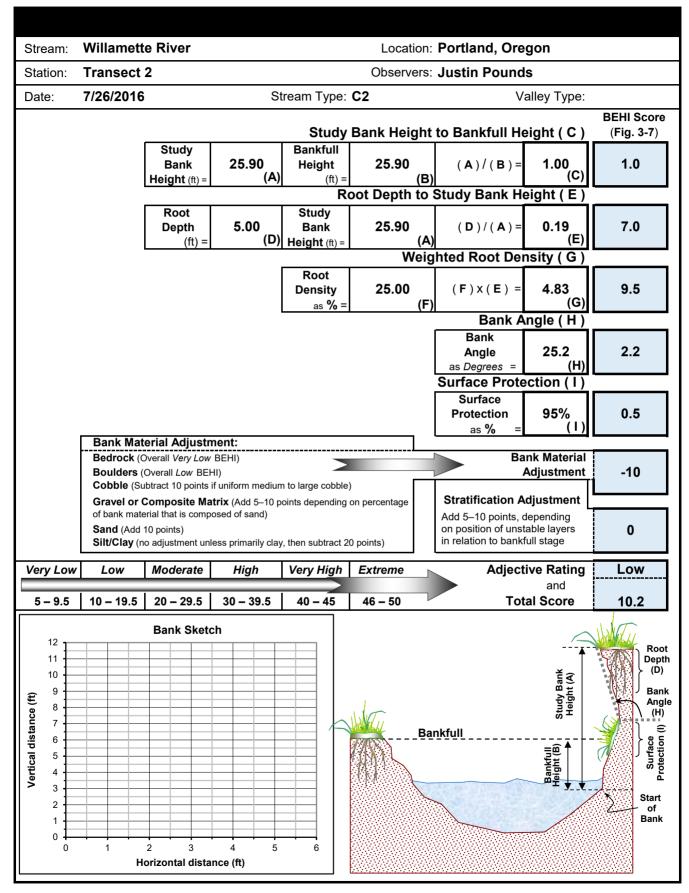
## ATTACHMENT 2 BEHI FIELD DATA SHEETS





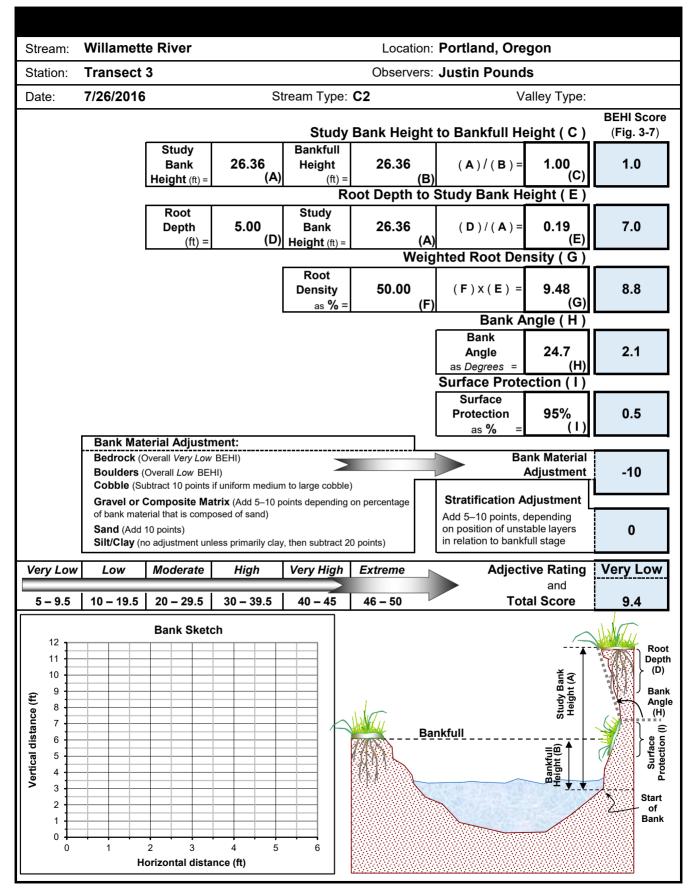
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River Stability Field Guide page 3-54



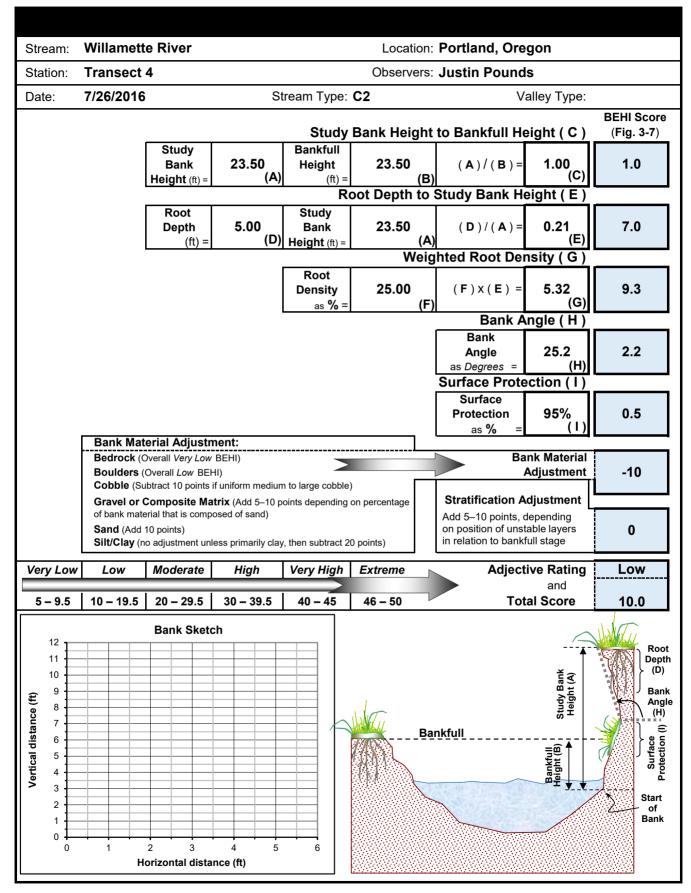
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River Stability Field Guide page 3-54



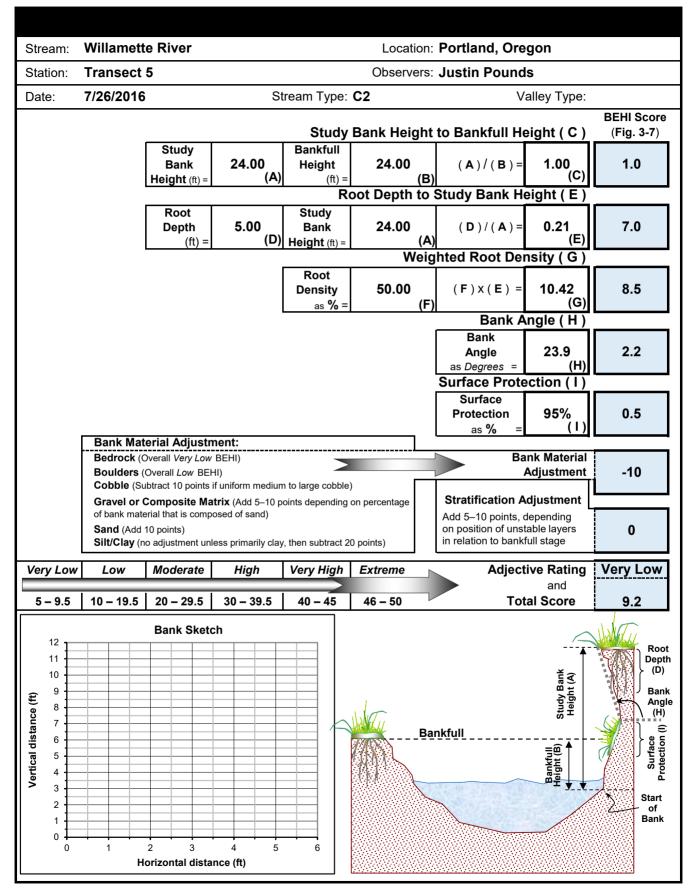
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River Stability Field Guide page 3-54



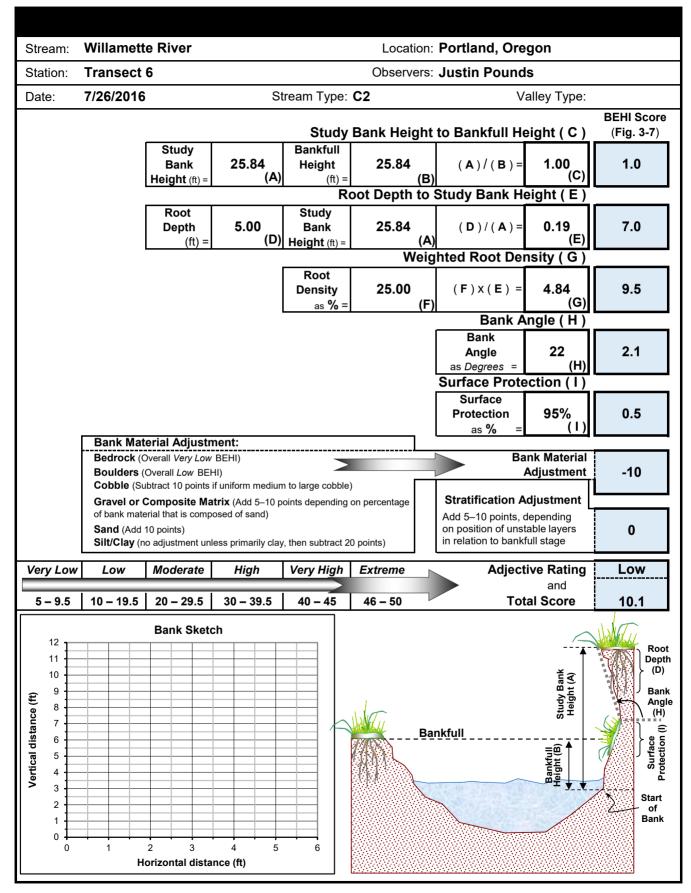
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River Stability Field Guide page 3-54



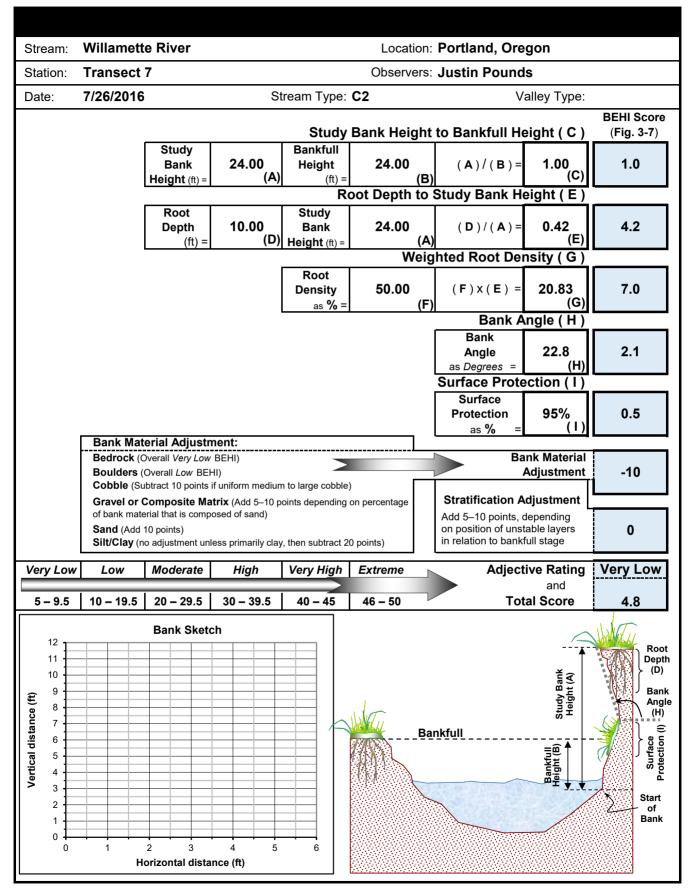
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River Stability Field Guide page 3-54



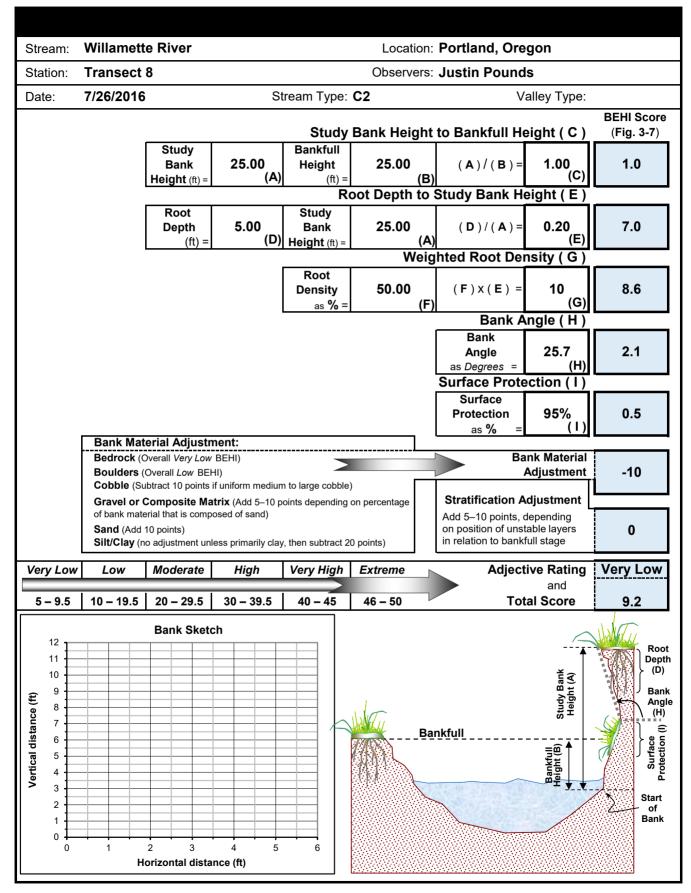
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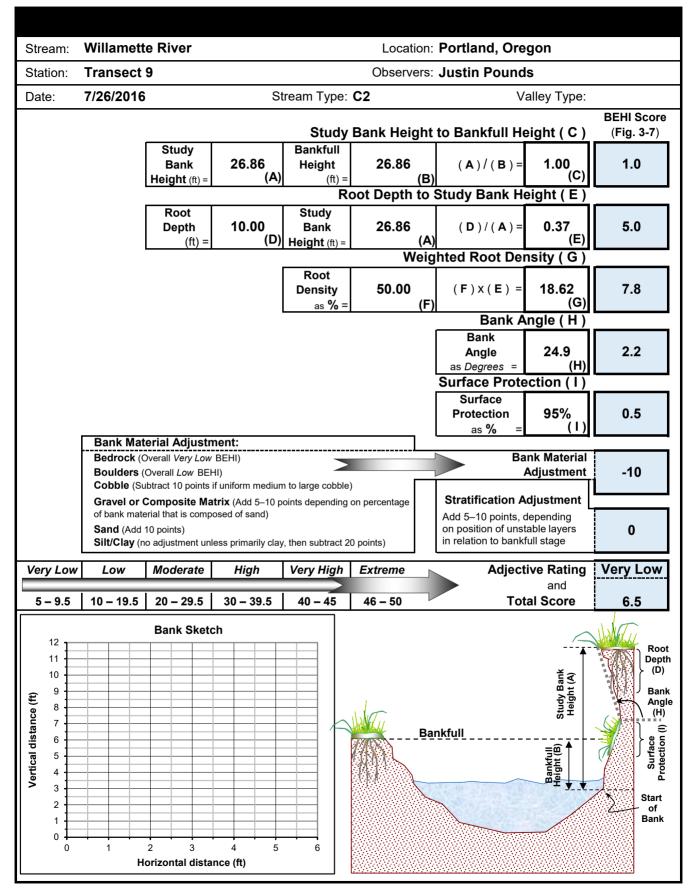
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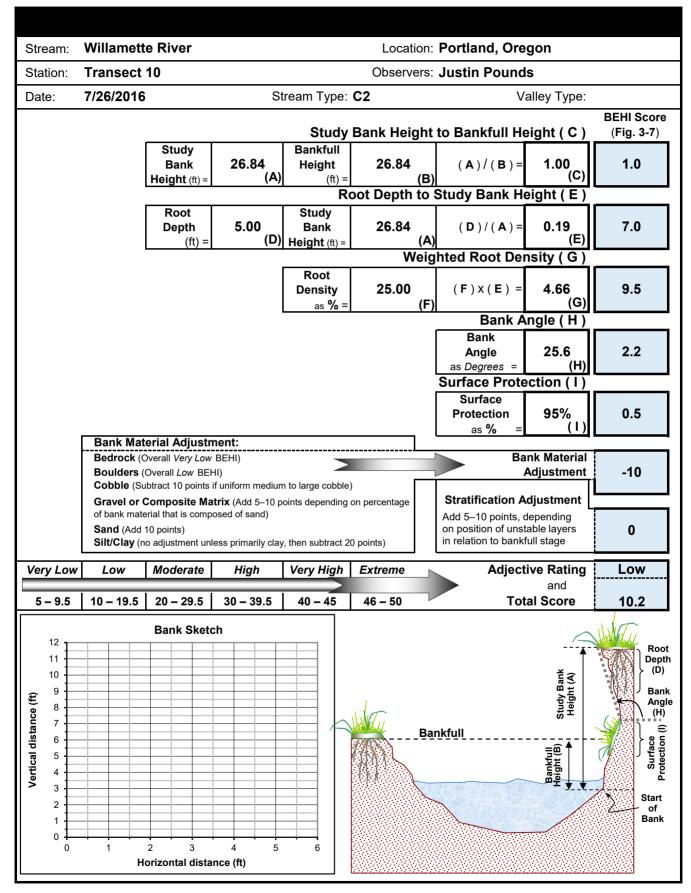
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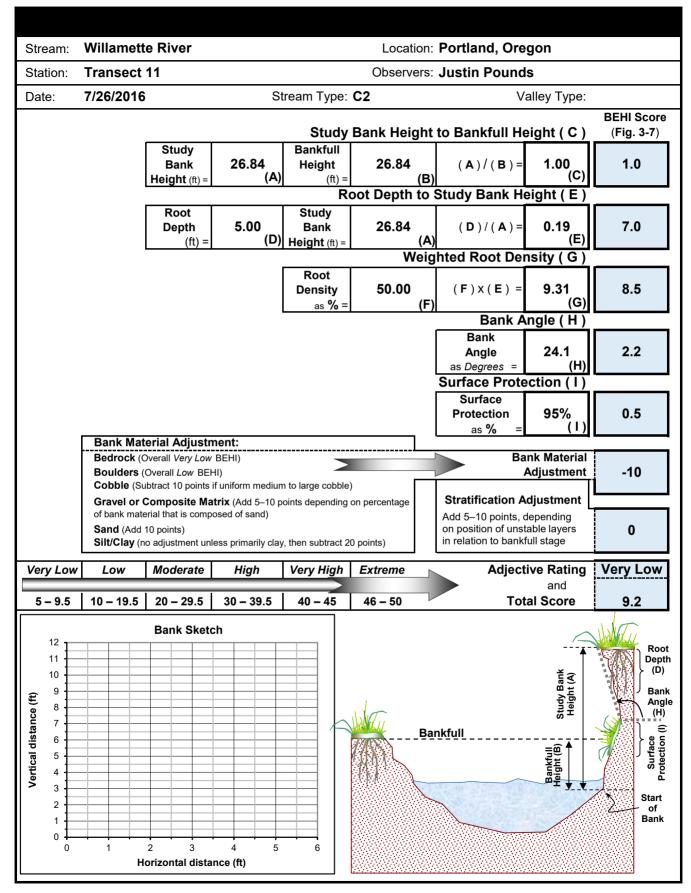
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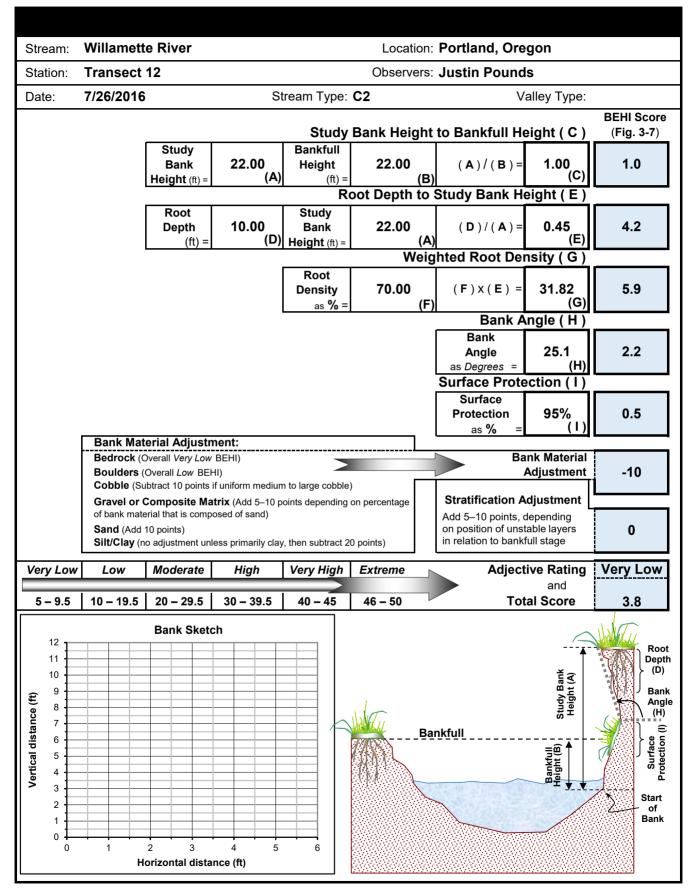
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## ATTACHMENT 3

NOAA DATUMS FOR 9439221 (PORTLAND, OREGON MORRISON ST. BRIDGE)





### Home (/) / Products (products.html) / Datums (stations.html?type=Datums) / 9439221 Portland Morrison Street Bridge, OR Favorite Stations

Station Info

Tides/Water Levels

Meteorological Obs.

Phys. Oceanography

OFS (/ofs/ofs\_station.html?stname=Portland Morrison Street Bridge&ofs=cre&stnid=9439221&subdomain=up)

### Datums for 9439221, Portland Morrison Street Bridge OR

NOTICE: All data values are relative to the NAVD88.

### **Elevations on NAVD88**

Station: 9439221, Portland Morrison Street Bridge, OR Status: Accepted (Feb 2 2012) Units: Feet Control Station: 9439040 Astoria, OR T.M.: 120 Epoch: (/datum\_options.html#NTDE) 1983-2001 Datum: NAVD88

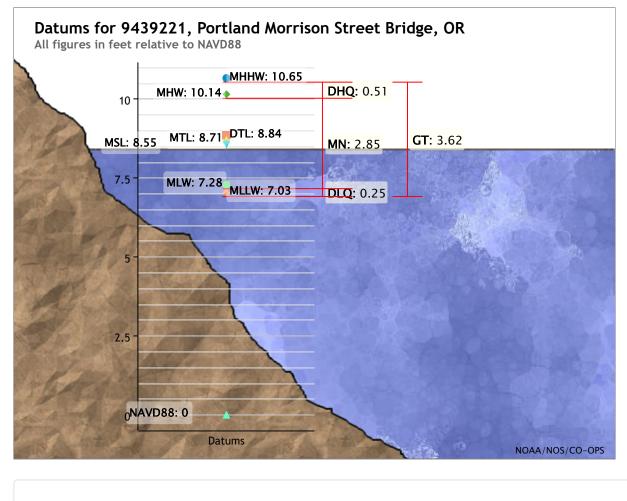
| Datum                           | Value | Description                           |
|---------------------------------|-------|---------------------------------------|
| MHHW (/datum_options.html#MHHW) | 10.65 | Mean Higher-High Water                |
| MHW (/datum_options.html#MHW)   | 10.14 | Mean High Water                       |
| MTL (/datum_options.html#MTL)   | 8.71  | Mean Tide Level                       |
| MSL (/datum_options.html#MSL)   | 8.55  | Mean Sea Level                        |
| DTL (/datum_options.html#DTL)   | 8.84  | Mean Diurnal Tide Level               |
| MLW (/datum_options.html#MLW)   | 7.28  | Mean Low Water                        |
| MLLW (/datum_options.html#MLLW) | 7.03  | Mean Lower-Low Water                  |
| NAVD88 (/datum_options.html)    | 0.00  | North American Vertical Datum of 1988 |
| STND (/datum_options.html#STND) | 5.38  | Station Datum                         |
| GT (/datum_options.html#GT)     | 3.62  | Great Diurnal Range                   |
| MN (/datum_options.html#MN)     | 2.85  | Mean Range of Tide                    |
| DHQ (/datum_options.html#DHQ)   | 0.51  | Mean Diurnal High Water Inequality    |

| Datum   | Value               | Description                              |
|---|---------------------|--|
| DLQ (/datum_options.html#DLQ)                           | 0.25                | Mean Diurnal Low Water Inequality        |
| HWI (/datum_options.html#HWI)                           | 1.10                | Greenwich High Water Interval (in hours) |
| LWI (/datum_options.html#LWI)                           | 9.51                | Greenwich Low Water Interval (in hours)  |
| Max Tide (/datum_options.html#MAXTIDE)                  |                     | Highest Observed Tide                    |
| Max Tide Date & Time<br>(/datum_options.html#MAXTIDEDT) |                     | Highest Observed Tide Date & Time        |
| Min Tide (/datum_options.html#MINTIDE)                  |                     | Lowest Observed Tide                     |
| Min Tide Date & Time (/datum_options.html#MINTIDEDT)    |                     | Lowest Observed Tide Date & Time         |
| HAT (/datum_options.html#HAT)                           | 13.63               | Highest Astronomical Tide                |
| HAT Date & Time   | 05/25/1994<br>12:18 | HAT Date and Time                        |
| LAT (/datum_options.html#LAT)                           | 4.94                | Lowest Astronomical Tide                 |
| LAT Date & Time   | 09/09/2000<br>18:24 | LAT Date and Time                        |

### **Tidal Datum Analysis Periods**

09/01/2002 - 10/31/2002

08/01/2005 - 10/31/2005



| Showing datur | ns for                   |
|---------------|--------------------------|
| 9439221 Portl | and Morrison S…          |
| Datum         |                          |
| NAVD88        | ~                        |
| Data Units    | Feet                     |
|               | ⊖ Meters                 |
| Epoch         | Present (1983-2001)      |
|               | ─ Superseded (1960-1978) |
|               | Submit                   |
|               |                          |
|               |                          |

Show nearby stations

### Products available at 9439221 Portland Morrison Street Bridge, OR

**TIDES/WATER LEVELS** Water Levels NOAA Tide Predictions (/noaatidepredictions.html?id=9439221) Harmonic Constituents (/harcon.html?id=9439221) Sea Level Trends Datums (/datums.html?id=9439221) Bench Mark Sheets (/benchmarks.html?id=9439221) Extreme Water Levels (/est/est station.shtml?stnid=9439221) Reports (/reports.html?id=9439221) **METEOROLOGICAL/OTHER** Meteorological Observations Water Temp/Conductivity PORTS® This station is not a member of PORTS® **OPERATIONAL FORECAST SYSTEMS** Columbia River Estuary (/ofs/creofs/creofs.html) OFS product page for Portland Morrison Street Bridge INFORMATION Station Home Page (/stationhome.html?id=9439221) Data Inventory (/inventory.html?id=9439221) Measurement Specifications (/measure.html)

### Website Owner: Center for Operational Oceanographic Products and Services

National Oceanic and Atmospheric Administration (http://www.noaa.gov) National Ocean Service (http://oceanservice.noaa.gov) Privacy Policy (/privacy.html) Disclaimer (/disclaimers.html) Take Our Survey (/survey.html) Freedom of Information Act (https://www.noaa.gov/foia-freedom-of-information-act) Contact Us (/contact.html)