EXHIBIT NO. \_\_\_\_\_ (WAG-4)

DOCKET NO. \_\_\_\_

2003 POWER COST ONLY RATE CASE
WITNESS: WILLIAM A. GAINES

#### BEFORE THE

#### WASHINGTON UTILITIES AND TRANSPORTATION COMMISSION

WASHINGTON UTILITIES ATTRANSPORTATION COMMI	ND SSION,	
	Complainant,	Docket No
v.		
PUGET SOUND ENERGY, IN	C.,	
	Respondent.	

DIRECT TESTIMONY OF WILLIAM A. GAINES ON BEHALF OF PUGET SOUND ENERGY, INC.

Ex. \_\_\_\_\_ (WAG-4) Page 1 of 219

## Overview of PSE Loads and Resources 2001-2010



Load Resource Balance February 2002

## Load Forecast Assumptions

- Villamor's forecast and adjusted by Energy Supply for GPI and On peak/off peak average demand for 2001-2010 based on Щ В В
- PSE Customer and Sales Forecasts 2002-2010 (attached as Appendix 1)

## Resource Forecast Assumptions

- Forecasted on peak/off peak average energy based on information submitted for the rate case.
- average). Maintenance schedule based on last three years. Colstrip: energy = capacity x forced outage rate (seven year
- PSE Hydro based on 30 year average.
- Mid-C hydro based on NWPP 60 year average.
- QF Hydro based on average annual energy
- PSE CTs: = 4% forced outage rate.
- PG&E Seasonal Exchange terminated 12/31/2006.

## Significant Loss of Contract Resources

- PSE's percentage of Rock Island II declined by 5% in 2000 and will further decline annually to a maximum aggregate reduction of 50%.
- By the end of 2003, PSE will lose 265 MW capacity; 160 aMW.
- At the end of 2006, PSE will lose 300 MW winter capacity due to termination of PG&E exchange.
- By the end of 2010, PSE will lose 107 MW capacity; 94 aMW.
- Note: At the end of 2011, contracts expire for March Point! March Point II, and Tenaska - 385 MW capacity; 357 aMW

## Significant Loss of Contract Resources

Expiring Resources	MIJOEUE	Fnerav	Recource	Fxpiration
		aMW	Type	
Avsta	33	25	25 Thermal	12/31/2002
CSPE	20	0	19 Hydro	3/31/2003
Supplemental & Entitlement Capacity		0	Hydro	3/31/2003
PacifiCoro	200	120	20 Thermal	10/31/2003
Port Townsend Paper	4.0	0.3	0.3 Hydro-QF	12/31/2003
Powerex/Pt.Roberts		က	Hydro	9/30/2004
Hutchison Creek	6.0	0.2	0.2 Hydro-QF	9/30/2004
Baker Replacement	_		Hydro	9/30/2006
PG&E Seasonal Exchange-PSE	300	0	0 Thermal	12/31/2006
Puyallup Energy Recovery Co.(PERC)	N	 	Biomass-QF	4/15/2009
Conservation Credit - SnoPUD	10	9	10 Hydro	2/28/2010
Montana Power	26	84	Colstrip	12/29/2010

## Significant Loss of Contract Resources

	1.50		oiring	Expiring Resources Annualized	ource	es An	nual	ized		
7	) 02	2002 2003 2004 2005 2006 2007 2008 2009 2010	2004	2005	2006	2007	2008	2009	2010	Total
	25 1	139.3	39.3 3.2	0	<b>\_</b>	0		0 1.8 94	<b>7</b> 6	264.3
(MW)	33	33 230.4 8.9	8.9		0 307		0	0 0 2 107	107	688.3

### Load/Resource Balance

- PSE is deficit for 2002-2010 on peak if CTs are not assumed.
- By the end of 2006, the deficit for on peak increases to approximately 500 MW if CTs are not assumed.
- Based on PIRA's 2002-2005 price forecast of \$3.24 per MMBtu and \$31.50 per MW for gas and on peak electric, PSE's CTs would not clear the market.

[Source: PIRA Oct 2001, Table VIII-30; U.S. Electricity Prices, On Peak 1998-2015; North American Gas Prices 1990-2015]

## Load/Resource Balance - Without CTs

		िं	Surplus/Deficit (-)	cit (-)		
			(MWe)			
		On Peak			Off Peak	
Year	Load R	Resources	Surplus (Deficit)	Load	Load Resources	Surplus (Deficit)
			ermed a specific			
2002	2587	2478	-1000 to exceed the second of	2025	2062	37
2003	2623	2481	-142	2058	2127	69
2004	2611	2306	-305	2049	2105	56
2005	2680	2296	-384	2102	2080	-22
2006	2735	2264	-471	2145	2043	-102
2007	2789	2254	-535	2185	2032	-153
2008	2851	2246	-605	2193	2027	-166
2009	2912	2247	-665	2253	2028	
2010	2974	2239	-735	2300	2020	280

# Load/Resource Balance - With CTs (588 MW)

		Ō	Surplus/Deficit (-)	cit (-)		
			(aMW)			
		On Peak		et verdag van be	Off Peak	
Year	Load	Resources	Surplus (Deficit)	Load	Resources	Surplus (Deficit)
2002	2587	3066	479	2025	2650	625
2003	2623	3069	446	2058	2715	657
2004	2611	2894	283	2049	2693	644
2005	2680	2884	204	2102	2668	566
2006	2735	2852		2145	2631	486
2007	2789	2842	53	2185	2620	435
2008	2851	2834		2193	2615	422
2009	2912	2835	77-	2253	2616	363
2010	2974	2827	-147	2300	2608	308

## Load Resource Balance - Resource Key

Colstrip: Colstrip 1&2, Colstrip 3&4

Cogens: March Point Phase I, Phase II, Sumas

Contracts

BC Hydro-Pt. Roberts, Baker Replacement, CSPE, Canadian Other:

Entitlement & Extension, Snohomish Conservation, North WASCO

Montana Power, Pacificorp, PERC, PG&E Exchange, WWP,

WNP3 Exchange

Hutchinson Creek, Kingdom Energy-Sygitowicz, Koma Kulshan, QF's:

Port Townsend Paper, Spokane, Twin Falls, Weeks Falls

CTs - Baseload: Encogen, Tenaska

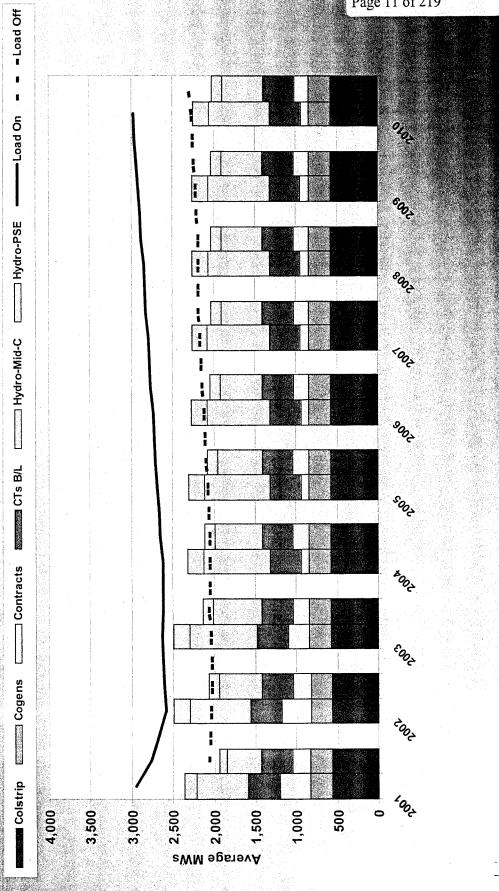
Hydro:

Wells, Rocky Reach, Rock Island I, Rock Island II, Wanapum, Priest Rapids Baker (Upper/Lower), White River, Snoqualmie Falls, Electron

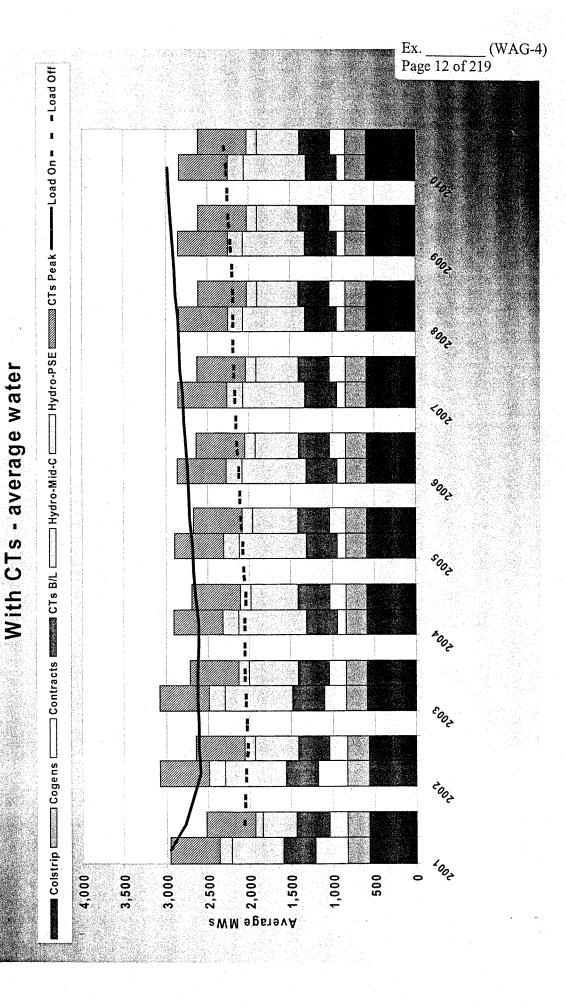
Frederickson, Fredonia, Whitehorn, Crystal Mountain CTs - Peaking:

# Load/Resource Balance - On Peak/Off Peak 2001-2010

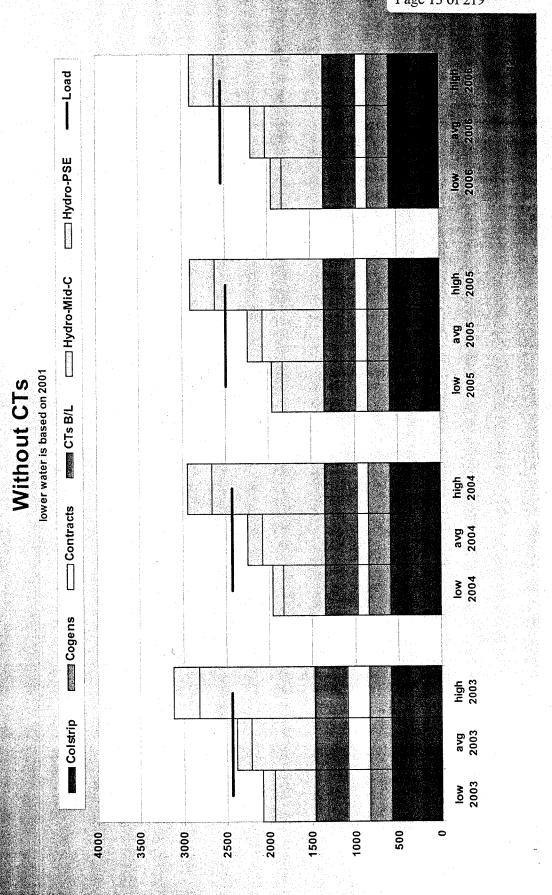
### Without CTs - average water







# \_oad/Resource Balance - Water Sensitivity 2003-2006



# Load/Resource Balance - Water Sensitivity 2003-2006

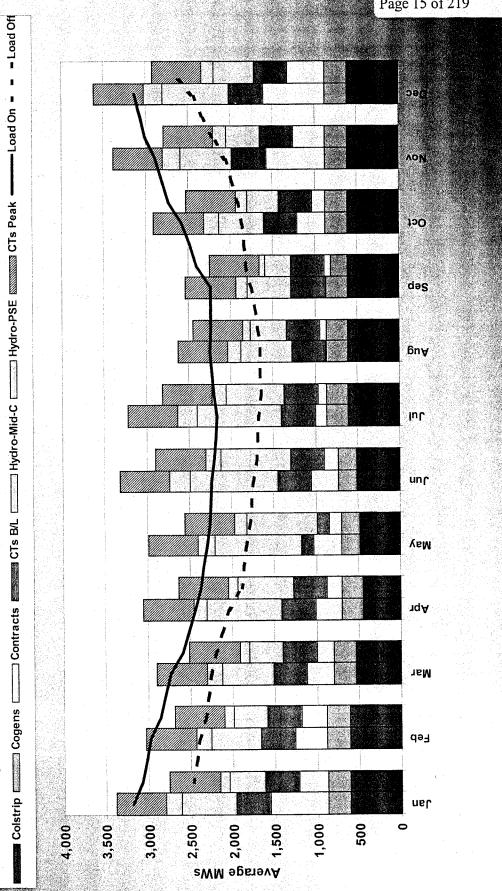
#### With CTs

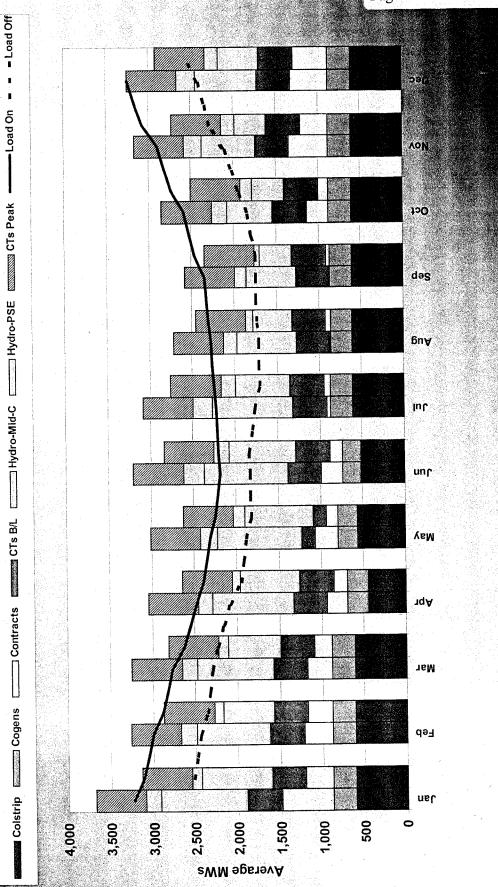
lower water is based on 2001

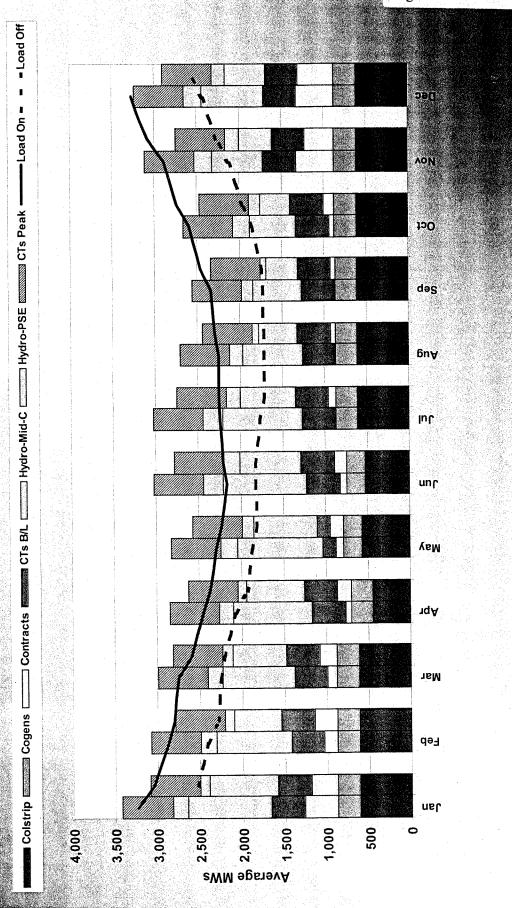


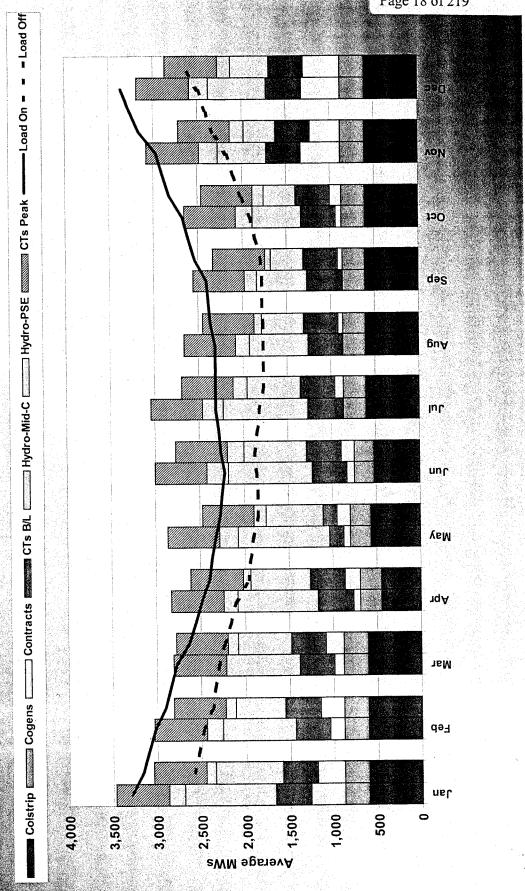
(WAG-4)

Ex. \_\_\_\_( Page 15 of 219

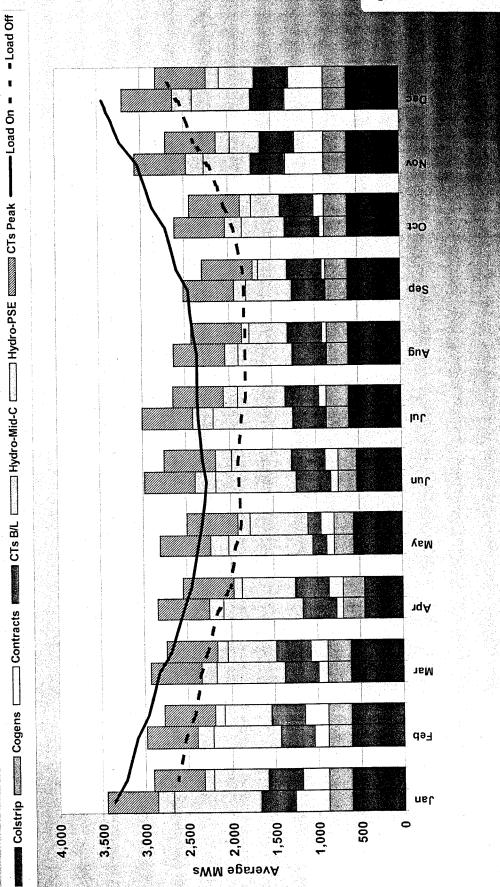


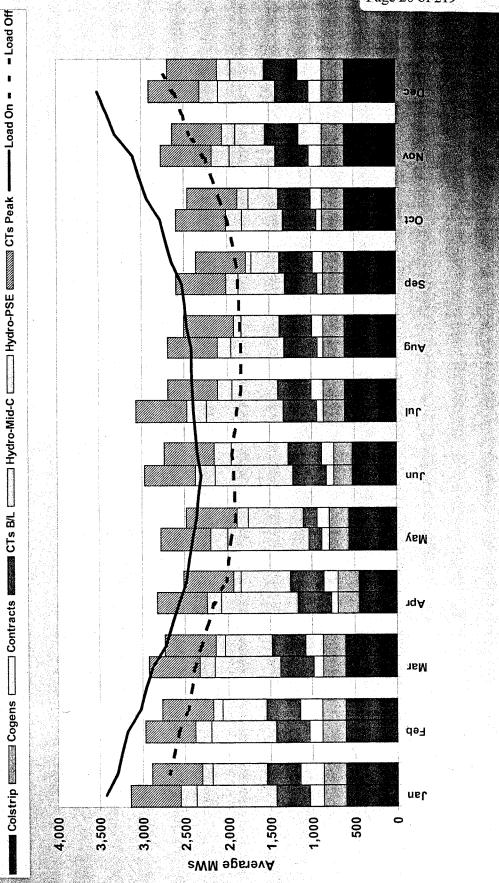






Ex. \_\_\_\_\_( Page 19 of 219 (WAG-4)

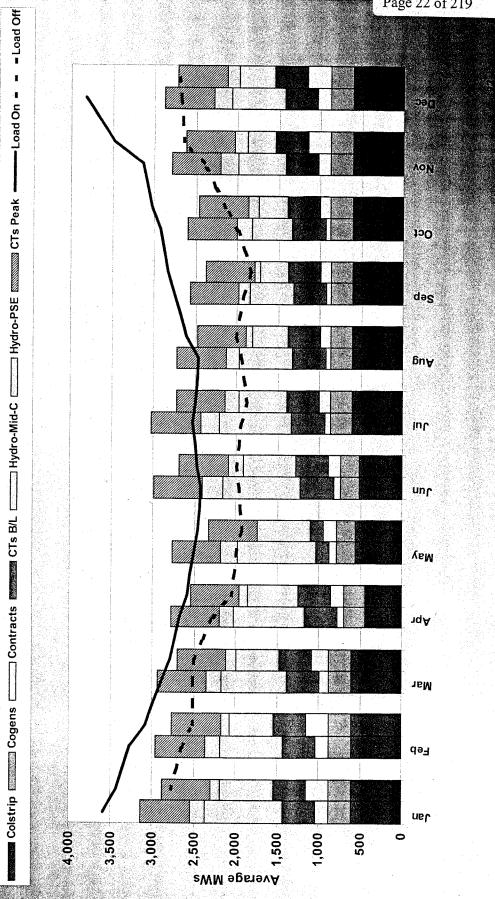


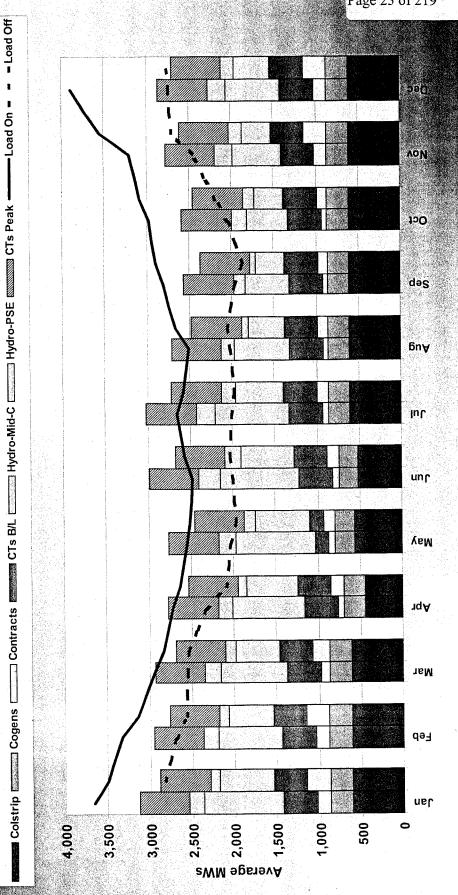


Page 21 of 219



Page 22 of 219





### Fransmission - Summary

Development/Purchase of new resources must include analysis of transmission issues due to current system constraints and unknown congestion management design of RTO-West.

- Delivery constrained from North (Whatcom/Skagit) due to PSE and BPA systems.
- Delivery from East constrained due to West of Hatwai cutplane.
- Delivery from South (Oregon) constrained subject to Northern Cascade flows/constraints.

## Transmission - System Constraints

- PSE Constraints
- Whatcom and Skagit Counties
- BPA Constraints Affecting PSE
- West of Hatwai
- Northwest to Canada (BPA Treaty Obligation)
- Canada to Northwest
- Cross Cascades North
- California Oregon Interconnect (COI)

### **PSE System Constraints**

### Whatcom and Skagit Constraints

- amount of transfer capacity between Whatcom, Skagit between 625 MW and 700 MW from the north into 115kV transmission lines and contracts with BPA Issue: Generation greater than load. PSE has a limited King County via PSE's ownership of 230kV and and King Counties. PSE has a right to transmit
- Magnitude: There is no more transmission capacity available to bring additional generation out of Whatcom and Skagit Counties.
- \$80 million. That cost may be mitigated by work BPA system has been determined to be between \$50 and The cost to integrate a 700 MW resource into PSE's s contemplating. Cost:

## **BPA Constraints Affecting PSE**

#### West of Hatwai

- Issue: Inability to transmit Colstrip to PSE system
- Magnitude: 150 MW to 200 MW max
- Cost: Approximately \$1,000,000 per week of curtailment at 175 MW and \$35/MWh.

## Northwest to Canada (BPA Treaty Obligation)

- Whatcom and Skagit Counties at PSE expense to fix Issue: May require the operation of PSE generation in a BPA problem.
- Magnitude: 280 MW max over the next few years, increasing to 420 MW max when all Canadian Entitlement must be returned.
- Cost: Approximately \$25,000 per day of forced out of market operation of the CTs.

## **BPA** Constraints Affecting PSE (cont.)

### Canada to Northwest

issue for our balancing purchases not a limitation on PSE's firm power supplies or PSE's ability to meet Inability to import energy from Canada. This is an load. - Issne:

### **Cross Cascades North**

requests for transfers over the path that, when added Issue: Inability to transmit all Mid-Columbia and Colstrip into to the existing firm commitments, exceed the transfer there is not an issue with imports. BPA has received transfer capability in excess of firm commitments, so the Puget Sound area. However, currently there is

## **BPA** Constraints Affecting PSE (cont.)

## California Oregon Interconnect (COI)

Deliveries from PG&E affect PSE's ability to meet its Issue: Limits ability to transfer energy to or from PG&E. Puget Sound area loads.

- Magnitude: Up to 150 MW on any hour

contractual flexibility to have energy delivered on any hour. The \$200,000 is based on the difference Cost: Less than \$200,000 annually because of the between HLH and LLH prices.

### Generation Opportunities

#### **PSE** Alternatives

- BP Amoco Whitehorn
- Frederickson Power Enhanced Cogeneration
  - PSE Development of Frederickson site
- PSE Development of Jackson Prairie site

### Large Merchant Plants

- BP Amoco
- Calpine Corporation
- Duke Energy of North America
  - Engage Energy
- Mirant Corporation
- Reliant Energy
- Westward Power Project

### Renewable Resources

- Zilkha -- wind
- King County -- methane/landfill
- Farmatic -- methane

### **PSE** Alternatives

- BP Amoco/PSE Participation
- Whitehorn upgrade from 150 MW to 200 MW.
- Frederickson Power Enhanced Cogeneration
- Waste heat from PSE's existing combustion turbines can be steam would be used to generate incremental electricity for Frederickson Power facility. By displacing natural gas, this utilized to generate steam, which can then be sold to the shared economic benefit.
- Development of Frederickson site
- Development of Jackson Prairie

### -arge Merchant Plants

### Calpine Corporation

- Gas fired plant in Turner, OR
   Heat Rate: 7,000 Btu/kWh
  - - Output: 620 MW COD: Q2, 2004
- Gas fired plant in Hermiston, OR
  - Heat Rate: 6,900 Btu/kWh Output: 630 MW COD: Q2, 2002
- Gas fired plant in Goldendale, WA
  - Heat Rate: 7,100 Btu/kWh
    - Output: 248 MW
      - COD: Q3, 2002

## Large Merchant Plants (cont.)

### **Duke Energy of North America**

– Satsop

POD. 600 MW plant in Grays Harbor County, WA Heat Rate: 7,160 Btu/kWh Output: 600 MW COD: Q3, 2003

## Large Merchant Plants (cont.)

#### Engage Energy

- Frederickson Power 1:
- POD: BPA 230 kV system, S. Tacoma main grid
  - Heat Rate: 7,100 Btu/kWh (guaranteed)
- Output: 249 MW (base; 270 MW w/duct firing and steam augmentation
  - COD: 7-1-2002 (estimated)
- Frederickson Power 2:
- POD: BPA 230 kV system, S. Tacoma main grid
  - Heat Rate: 7,100 Btu/kWh (average)
- Output: 250 MW (base); 290 MW w/duct firing and steam augmentation
  - COD: Q3/Q4, 2003 (estimated)

## Large Merchant Plants (cont.)

#### Mirant

- Gas fired plant in Longview, WA
- Heat Rate: 6,800 Btu/kWhOutput: 290 MWCOD: Q3, 2003
- Gas fired plant in Boardman, WA (Coyote Springs II)
- Heat Rate: 6,800 Btu/kWh
  - Output: 270 MW COD: Q3, 2002

### Page 36 of 219

## Large Merchant Plants (cont.)

### Reliant Energy

- Proposed gas-fired power plant in north central Oregon.
- POD: BPA, close to three 500 kV lines, near Grizzley
- Heat Rate: 7,100 Btu/kWh (average)
  - Output: 500 MW
- COD: Q1, 2005 (estimated)

### **Westward Power Project**

- Proposed gas-fired power plant in Clatskanie, OR.
- POD: BPA system near Clatskanie Heat Rate: 6,693 Btu/kWh
  - Output: 520 MW
    - COD: Q2, 2004

### Renewable Resources

Zilkha

→ Wind

King County

Methane Gas

Cedar Hills Landfill in Maple Valley, WA. Private company to build a plant. The County accepted proposals in January, 2002.

POD: PSE or BPA

Output: 22-26 MW

COD: Q1, 2004

# Renewable Resources (cont.)

- Various
- Methane Gas (Farmatic)POD: Whatcom/Skagit CountiesOutput: 400 kW

### **APPENDIX**

**Customer Sales Forecast Resources Summaries** 

Resources
Contract Abstracts

**Selected Transmission Studies** 

Frederickson – 270 MW

Frederickson - 50/100/150 MW

Frederickson - 25 MW

Fredonia – 110 MW

March Point - 50 MW

**Sumas II - 720 MW** 

Ex		(WAG-4)
Page 4	0  of '	219

### PUGET SOUND ENERGY CUSTOMER AND SALES FORECASTS (F2001) 2002-2009

### SALES FORECAST SUMMARY

### Electric

- Electric sales from fixed rate schedules is expected to slightly decline by -0.4% in 2002 (-82 GWHs) including ISPs (-0.6% or -108 GWHs without ISPs), while customers are expected to increase by 1.5% or 14,341 customers over 2000.
- In F2000, sales was projected to increase by 5.9% (1,313 GWHs, including ISPs), while customers was expected to increase by 12,416 over 2001.
- 8 year forecast is 1.9% average annual sales growth with ISPs (1.7% without ISPs) versus 2.6% in F2000.

### Gas

- Gas sales is expected to increase by 1.5% (14,781 Mtherms) in 2002 and customers are expected to rise by 18,410 (including sales and marketing goals) over 2001.
- F2000 sales forecast for 2002 was 0.5% growth (5,253 Mtherms) and customer addition of 19,243 over 2001.
- 8 year forecast of growth is 2.5% average annual versus 1.1% in F2000.

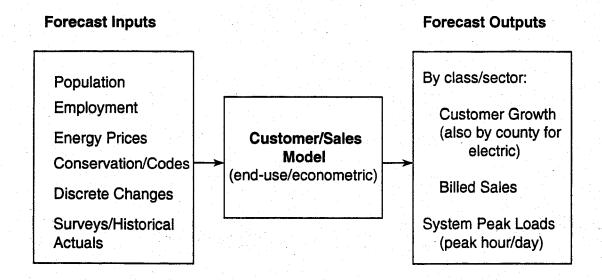
Ex	(WAG-4)
Page 4	

### KEY DRIVERS TO THE FORECAST

- F2001 is different from F2000 forecast due to the removal of schedule 48 (except for 3 small customers), special contract and Seatac from the projected loads, following the settlement agreement. A separate forecast for retail wheeling customers (schedule 449: all Boeing, Air Liquides, Air Products, Intel, Seatac and other small customers) is developed however.
- Forecast of further slowing in Puget Sound population and employment slightly declining in 2002 but slightly increasing in 2003. Adjustments were made for the negative impacts of the terrorist attacks on the national economy and the Boeing layoff on the Puget Sound regional economy.
- Projection of retail electric rates increasing in the near term and gas prices declining in real terms; for electric, rates were adjusted for the BPA credit on the residential and projected rate increases due to the emergency rate relief (18%) and a general rate case after that (22.5%); for gas, rates are projected to decline given the PGA adjustment plus a forecast of declining spot gas prices, even after increasing the margin by 5.1% after the general rate case.
- Downward adjustment in the forecast of ISP loads (for 2002, F2001 forecast of ISP load is 51 GWHs versus 1,418 GWHs for F2000 and 184 GWHs in F2000R).
- Inclusion of the estimated effects of PEM/Conservation on the electric forecast. Based on GPI analysis, PEM/Conservation effects start at about 3% reduction in January 2001 and declining to zero by June 2003 spread over residential and commercial classes using monthly sales are relative weights. Time of use rates are assumed to affect load shifting only.
- Reductions in loads due to savings from conservation programs adjusted for average measure life and price overlap effects. New savings for 2001 is assumed to be 8.1 aMW and 5.5 aMW annually for 2002 and beyond.
- Additions to gas customers due to marketing programs. Marketing goal for 2002 is to add 2,050 customers over forecasted customer additions.

Ex. (WAG-4) Page 42 of 219

### FORECAST MODEL OVERVIEW



- F2000 models utilized combination of end-use and econometric models using quarterly or annual data at the 2 digit SIC level.
- F2001 models used econometric approach using monthly revenue class data. The basic structure of the equations are:

Use per Customer = f(Weather, Prices, Economic/Demographic Variables)

Customer Counts = f(Prices, Economic/Demographic Variables)

Where prices or economic/demographic variables could enter as polynomial distributed lag variables

Estimated Price Elasticities:

Electric: Residential = -.18; Commercial = -.33; Industrial = -.46 Gas Core Sales: Residential = -.21; Commercial = -.26; Industrial = -.27

Other Model Revisions: Updated for new normal weather variables using the last 30 years up through first quarter of 2001 (F2000-4851, F2001-4847, HDD65); Streamlined the model runs and processing of model outputs.

Ex. \_\_\_\_ (WAG-4) Page 43 of 219

### POPULATION AND EMPLOYMENT PROJECTIONS

Comparison of Population and Employment Forecasts, F2000 vs. F2001 (Revised)

			E	lectric Se	rvice Area	1							Gas Serv	ice Area			
		Popul	ation			Employ	loyment Population						ion Employment				
	Forecasts(000) Growth Rates		n Rates	Forecasts(000) Gro		Grow	Growth Rates Forecast		ts(000) Growth Rates		n Rates	Forecasts(000)		Growt	n Rates		
Year	F00	F01	<u>F00</u>	<u>F01</u>	F00	FOI	B	<u>F01</u>	ſ	<u>F00</u>	FO	F00	<u>F01</u>	<u>F00</u>	FŌ	F00	F01
2000	3239.2	3229.6	1.28%	1.01%	1720.7	1740.2	23%	3.3%	ı	3210.9	3208.3	1.27%	1.28%	1725.9	1734.5	20%	23%
2001	3280.2	3269.4	1.27%	1.23%	1753.5	1767.6	1.9%	1.6%	1	3251.0	3248.9	1.25%	1.26%	1758.6	1763.3	1.9%	1.7%
2002	3320.3	3279.1	1.22%	0.29%	1787.9	1762.0	20%	-0.3%	١	3290.0	3259.4	1,20%	0.32%	1793.6	1757.2	20%	-0.3%
2003	3359.2	3322.2	1.17%	1.31%	1818.5	1780.2	1.7%	1.0%	1	3327.9	3303.2	1.15%	1.34%	1825.9	1775.4	1.8%	1.0%
2004	3400.7	3365.4	1.24%	1.30%	1855.3	18184	20%	21%	ŀ	3368.3	3347.2	1.22%	1.33%	1865.0	1813.4	21%	21%
2005	3446.2	3407.2	1.34%	1.24%	1894.4	1854.4	21%	20%		34128	3389.8	1.32%	1.27%	1907.5	1850.8	23%	21%
2006	3494.2	3449.6	1.39%	1.24%	1932.5	1889.6	20%	1.9%		3459.6	3433.0	1.37%	1.27%	1948.3	1887.3	21%	20%
2007	3542.5	3493.0	1.38%	1.26%	1969.9	1921.9	1.9%	1.7%	1	3506.7	3477.3	1.36%	1.29%	1987.1	1920.5	20%	1.8%
2008	3590.1	3535.3	1.35%	1.21%	2005.4	1949.1	1.8%	1.4%	l	35532	3520.4	1.33%	1.24%	20234	1948.1	1.8%	1.4%
2009	3637.0	3576.5	1.31%	1.17%	2036.8	1985.1	1.6%	1.8%	ı	3598.9	3562.6	129%	1.20%	2054.9	1984.5	1.6%	1.9%

- Macroeconomic forecasts are based on DRI-WEFA's First Quarter 2001 Long Term Projections which before the terrorist attacks, assumed no recession but a slower GDP growth in 2001 (1.8%) and a faster growth in 2002 (3.1%).
- Also before the terrorist attacks and despite of the February earthquake, the Boeing shuffle, energy price spikes, dot com meltdown, and the burst in stock market bubble, the Puget Sound regional economy was expected to grow 1.7% in employment in 2002 with the help of steady Boeing and Microsoft employment and assuming that the national economy avoids recession.
- With the terrorist attacks, recession is now projected for the national economy, with the US economy declining in the last two quarters of 2001 and recovering immediately after that. Boeing has also recently announced layoffs of about 30,000 jobs given the decline in air travel. Given these, service area employment is now expected to decline by .3% in 2002 but increases by 1.0% in 2003. The implication is that the full effects of Boeing's layoff will be spread over two years. Population is expected to be close to flat and income growth will be zero.

Ex. \_\_\_\_ (WAG-4) Page 44 of 219

### RETAIL ELECTRIC AND GAS PRICES

Comparison of Forecasts of Retail Rates (nominal)

Electric Rates	cents/kwh	2001	2002	2003	2004	2005	2006	2007	2008	2009	aarg
Residential	F2000	6.35	6.35	6.43	6.50	6.59	6.69	6.81	6.94	7.08	1.4%
	F2001	6.47	7.09	7.07	7.07	7.07	7.07	7.07	7.07	7.07	1.1%
Commercial	F2000	6.49	6.48	6.54	6.60	6.69	6.80	6.92	7.05	7.19	1.3%
	F2001	6.62	7.63	7.88	7.88	7.88	7.88	7.88	7.88	7.88	2.2%
Industrial*	F2000	7.27	6.35	5.94	5.53	5.60	5.69	5.79	5.90	6.02	-2.3%
	F2001	6.09	7.03	7.25	7.25	7.25	7.25	7.25	7.25	7.25	22%
aarg - aver and	rual rate of grow	th * Industri	al includes :	Sch 48 in F	2000, but no	t in F2001					

Gas Rates,\$/ti	nerm	2001	2002	2003	2004	2005	2006	2007	2008	2009	aarg
Residential	F2000	0.97	0.95	0.96	0.99	1.00	1.01	1.03	1.05	1.07	1.3%
	F2001	0.96	0.92	0.84	0.83	0.83	0.83	0.83	0.85	0.86	-1.3%
Commercial	F2000	0.91	0.89	0.89	0.93	0.94	0.94	0.96	0.98	1.00	1.2%
	F2001	0.89	0.86	0.77	0.75	0.76	0.75	0.75	0.77	0.78	-1.7%
Industrial	F2000	0.86	0.82	0.82	0.87	0.87	0.88	0.90	0.91	0.94	1.1%
	F2001	0.68	0.67	0.59	0.58	0.58	0.58	0.58	0.59	0.60	-1.5%

- Retail electric rates are expected to rise due to the emergency rate relief (18% over current rates from Nov. 2001 to October 2002) and then due to the general rate case (22.5% over current rates starting November 2002), even after the residential BPA credit. They are assumed to be flat beyond 2003.
- Gas retail rates account for the most recent PGA filing reducing rates by 11%, then following DRI-WEFA's projection of retail rates for 2003 and beyond. The decline is mitigated by the expected rate increase (5.1%) due to the general rate case effective November 2002. DRI-WEFA expects gas retail rates to decline in the next 2-3 years. In F2000, gas retail rates were expected to increase over time.

Ex. \_\_\_\_ (WAG-4) Page 45 of 219

### HISTORICAL GROWTH AND SHARES

Electric Sales and Customers											
	5 Yr A	vg Growth	200	O Shares							
Class	Sales	Customer	Sales	Customer							
Residential	0.9%	1.9%	45%	88.6%							
Commercial	29%	25%	36%	10.8%							
industrial	1.1%	1.0%	18%	0.4%							
St Lights/Resale	1.5%	28%	1%	0.2%							
Total	1.6%	1.9%	100%	100.0%							

Gas	Gas Sales and Customers											
	5 Yr A	wg Growth	199	9 Shares								
Class	Sales	Customer	Sales	Customer								
Residential	23%	4.4%	46%	91.68%								
Commercial	1.9%	29%	19%	7.68%								
Industrial	3.2%	0.6%	4%	0.48%								
Total Core	23%	4.3%	69%	99.84%								
Interruptibles	-1.0%	-1.8%	11%	0.14%								
Transportation	6.1%	3.7%	20%	0.02%								
Total NonCore	0.0%	-1.3%	31%	0.16%								
Total	1.5%	4.3%	100%	100.00%								

The tables above show a summary of the five year (1976-2000) average growth rate by class and load shares in 2000.

- Electric sales have grown an average of 1.6% per year in the last five years with growth coming mostly from non-residential sector.
- Residential electric customers account for 45% of sales and about 90% of total number of customers.
- Gas sales have grown about 1.5% per year in the last five years with growth accounted for mostly by core sales sector.
- Again, residential gas customers account for 46% of sales and 92% of total customers. Non-core customers (interruptibles and transports) account for 30% of gas sales but less .2% of total customers.

Ex. \_\_\_\_ (WAG-4) Page 46 of 219

### **ELECTRIC CUSTOMER AND SALES FORECASTS**

### **F2001 Electric Forecasts**

			For	ecast of Cust	omers (year	end)				
	2001	2002	2003	2004	2005	2006	2007	2008	2009	aarg*
Total - Fixed Sched	939,665	954,006	968,890	985,752	1,003,497	1,020,970	1,038,659	1,056,682	1,074,403	1.7%
Additions	16,055	14,341	14,883	16,863	17,745	17,473	17,689	18,023	17,721	
% Change	1.7%	1.5%	1.6%	1.7%	1.8%	1.7%	1.7%	1.7%	1.7%	
Residential	831,400	843,904	856,155	870,422	885,634	900,572	915,738	931,250	946,464	1.6%
Commercial	102,408	104,206	106,744	109,182	111,583	113,984	116,371	118,741	121,087	2.1%
Industrial	4,038	4,003	4,012	4,077	4,105	4,122	4,129	4,124	4,120	0.3%
Street Lights	1,810	1,886	1,970	2,063	2,167	2,283	2,414	2,560	2,725	5.3%
Resale	8	8	8	8	8	8	8	8	8	0.0%
Retail Whing Svcs**	12	12	12	12	12	12	12	. 12	12	0.0%

<sup>\*</sup>aver annual rate of growth from 2002 to 2009 \*\* Not icluded in Total Fixed Sched

			Forecast	of Billed Sale	s with ISPs (	GWHs)		,		
	2001	2002	2003	2004	2005	2006	2007	2008	2009	aarg*
Total - Fixed Sched	19,117	19,035	19,309	19,636	20,173	20,591	20,980	21,377	21,800	1.7%
% Change	0.4%	-0.4%	1.4%	1.7%	2.7%	2.1%	1.9%	1.9%	2.0%	
Residential	9,476	9,593	9,748	9,846	10,015	10,179	10,342	10,510	10,681	1.5%
Commercial	8,010	8,018	8,170	8,346	8,545	8.760	8.974	9,190	9,430	2.1%
Industrial	1,434	1,276	1,204	1,209	1,231	1,241	1,249	1,256	1,264	-1.5%
Street Lights	85	88	93	96	100	104	108	113	118	4.2%
Resale	87	9	9	9	10	10	10	10	10	-9.7%
ISPs	25	51	.84	129	273	297	297	297	297	42.5%
Retail Whing Svcs**	376	1,034	1,047	1.072	1.096	1.115	1,120	1,119	1,110	22.8%

\*aver annual rate of growth from 2002 to 2009 \*\* Not icluded in Total Fixed Sched

			F20	01 and F2000	Comparison	ns				
	2001	2002	2003	2004	2005	2006	2007	2008	2009	aarg
Customer Additions	(year end)						:			
F2000	14,912	12,416	12,416	12,775	13,134	13,328	13,620	13,714	13,368	
% Change	1.6%	1.3%	1.3%	1.3%	1.3%	1.3%	1.4%	1.3%	1.3%	1.3%
F2001	16,055	14,341	14,883	16,863	17,745	17,473	17,689	18,023	17,721	
% Change	1.7%	1.5%	1.6%	1.7%	1.8%	1.7%	1.7%	1.7%	1.7%	1.7%
Sales in GWHs					· · <u>-</u>					
F2000 with ISP	22,238	23,551	24,470	24,918	25,388	25,866	26,329	26,855	27,371	1.
% Change	3.4%	5.9%	3.9%	1.8%	1.9%	1.9%	1.8%	2.0%	1.9%	2.6%
F2000 no ISP	21,759	22,133	22,574	23,021	23,492	23,969	24,432	24,959	25,474	
% Change	1.4%	1.7%	2.0%	2.0%	2.0%	2.0%	1.9%	2.2%	2.1%	2.0%
F2000R with ISP	20,294	19,605	20,672	21,489	22,258	22,880	23,305	23,798	24,286	
% Change	-5.5%	-3.4%	5.4%	3.9%	3.6%	2.8%	1.9%	2.1%	2.1%	2.3%
F2000R no ISP	20,254	19,421	20,165	20,614	21.031	21,456	21.881	22.374	22,863	
% Change	-5.7%	-4.1%	3.8%	2.2%	2.0%	2.0%	2.0%	2.3%	2.2%	1.6%
F2001 with ISP	19,117	19,035	19,309	19,636	20,173	20,591	20,980	21,377	21,800	
% Change	0.4%	-0.4%	1.4%	1.7%	2.7%	2.1%	1.9%	1.9%	2.0%	1.7%
F2001 no ISP	19,092	18,984	19,225	19,507	19,900	20,294	20,683	21,080	21,503	
% Change	0.3%	-0.6%	1.3%	1.5%	2.0%	2.0%	1.9%	1.9%	2.0%	1.5%

\*aver annual rate of growth from 2002 to 2009 \*\* Not icluded in Total Fixed Sched F2000R - Revised F2000 forecast for Sched 48, PEM and ISPs in March 2001.

- Average sales growth in the next 8 years is about 1.7%/yr, but growth pattern follows forecast of the economy and assumptions about rates, PEM and ISPs. Customer growth also follows growth pattern in economy.
- Main source of growth continues to be the commercial sector, although residential and the remaining industrial are expected to grow slightly.
- Load levels, even without ISPS, in 2001 are lower in F2001 vs F2000 by about 12% due to lower use per customer and the exclusion of schedule 48, special contracts and Seatac in F2001.

Ex. (WAG-4) Page 47 of 219

### GAS CUSTOMER AND SALES FORECASTS

### F2001 Gas Forecasts

Forecast of Customers (year end)

	( or country ( ) can call ( )											
	2001	2002	2003	2004	2005	2006	2007	2008	2009	aarq*		
Total	607,991	626,401	644,690	663,238	681,406	699,247	716,832	734,031	750.642	27%		
Additions	19,081	18,410	18,289	18,548	18,168	17,841	17,585	17,199	16.612			
% Change	3.2%	3.0%	2.9%	2.9%	27%	26%	25%	24%	2.3%			
Residential	558,443	576,383	594,303	612,308	629,860	647,051	664,014	680.637	696,654	2.8%		
Commercial	45,978	46,529	46,797	47,220	47,791	48,423	49.005	49,559	50,136	1.1%		
Industrial	2,615	2,545	2,638	2,745	2,769	2,769	2,788	2.789	2.782	0.8%		
Comi Interrupt	796	784	789	803	823	841	861	. 880	903	1.6%		
Ind interrupt	47	47	49	49	50	. 51	52	53	54	1.8%		
Comi Transpo	20	20	21	21	21	21	21	21	21	0.6%		
Ind Transpo	92	93	93	92	92	92	92	92	92	0.0%		

\*aver annual rate of growth from 2002 to 2009

Forecast of Billed Sales (Mtherms)

	2001	2002	2003	2004	2005	2006	2007	2008	2009	aarg*
Total	1,002,278	1,017,059	1,056,147	1,096,481	1.125.767	1,155,726	1,183,010	1,203,572	1,224,500	2.5%
% Change	-5.2%	1.5%	3.8%	3.8%	27%	27%	24%	1.7%	1.7%	
Residential	473,873	488,444	505,644	524,230	537,865	550,973	563,474	574.075	584,233	27%
Commercial	202,288	207,165	215,393	219,815	223,225	227,686	231,614	234,353	237.290	20%
Industrial	41,561	39,166	41,234	43,980	45,601	46,333	47,016	47,111	46.785	1.5%
Comi Interrupt	89,193	86,880	92,389	98,738	105,536	113,615	121.846	129,308	137.544	5.6%
Ind interrupt	16,569	14,935	15,185	16,269	17,128	17,885	18,454	18,732	18.893	1.7%
Comi Transpo	22,638	25,636	27,467	28,336	28.858	29,401	29,798	30.067	30,384	3.7%
Ind Transpo	156,156	154,834	158,835	165,113	167,554	169,833	170,808	169,926	169.370	1.0%

\*aver annual rate of growth from 2002 to 2009

			F2001	and F2000	Comparison	s				
	2001	2002	2003	2004	2005	2006	2007	2008	2009	aarg*
Customer Additions	(year end)									
F2000	20,061	19,243	17,442	18,190	18,053	18,912	19.281	17,331	17.373	
% Change	3.4%	3.1%	2.8%	2.8%	27%	2.8%		24%	2.5%	27%
F2001	19,081	18,410	18,289	18,548	18,168	17,841	17,585	17,199	16.612	
% Change	3.2%	3.0%	29%	2.9%	27%	2.6%		24%	23%	27%
Sales in Mitherms										
F2000	1,091,375	1,096,628	1,105,376	1,122,808	1,133,909	1.149.865	1,166,609	1.181.629	1,195,199	
%Change	0.8%	0.5%	0.8%	1.6%	1.0%	1.4%		1.3%	1.1%	1.1%
F2001	1,002,278	1,017,059	1,056,147	1,096,481	1,125,767	1,155,726	1.183.010		1,224,500	
%Change	-5.2%	1 5%	3.80/	2 90/	270/	2.79/	0.49/	4.70/	4.70/	0.50/

\*aver annual rate of growth from 2002 to 2009

- Average growth in gas sales is 2.5%/yr in the next 8 years, higher than last 5 year history due to expected decline in gas rates. Near term growth pattern in sales and customers is influenced by assumptions about rates, marketing goals, and economic factors.
- There is a decline in load levels from in 2000 to 2001 because of fuel switching in transport/interruptibles and lower residential use per customer.
- F2000 and F2001 differences are due to different forecast of rates, economy and marketing goals.

Ex. \_\_\_\_ (WAG-4) Page 48 of 219

The next two tables compare F2001 forecasts vs. normalized actuals, and 2001 forecasts vs. 2000 actuals for each class and by month and year, hence, shows monthly shapes and model calibration effects.

Comparison (GWHs)			-								4.5			
• •	Jan	Feb	Mar	Apr	May	Jun	<u>Jul</u>	Aug	Seo	<u>Oct</u>	Nov	Dec	JulYTD	Total
Total														
2000 Actuals	1956.4	1898.9	1840.3	15326	1405.8	1395.7	1329.0	1439.0	1409.1	1475.6	1553.7	1798.6	11358.7	19034.8
2000-F01	1967.8	1902.9	1800.2	1544.6	1453.3	1395.1	1338.1	1419.9	1395.6	1411.1	1572.6	1799.4	11402.0	19000.7
%Dif,ActvF01	-0.58%	-0.21%	2.22%	-0.78%	-3.27%	0.05%	-0.68%	1.35%	0.97%	4.57%	-1.20%	-0.05%	-0.38%	0.18%
2001 Actuals	1999.2	1969.5	1707.8	1655.7	1505.1	1408.0	1366.2	0.0	0.0	0.0	. 0.0	0.0	11611.4	
2001-F01	1996.3	1955.8	1714.4	1623.6	1479.1	1430.8	1393.6	1328.3	1385.2	1379.5	1578.7	1852.1	11593.6	19117.3
%Dif,ActvF01	0.15%	0.70%	-0.38%	1.98%	1.76%	-1.60%	-1.97%	-100.00%	-100.00%	-100.00%	-100.00%	-100.00%	0.15%	
Residential						. ,?								
2000 Actuals	1132.8	1061.8	987.4	822.1	705.8	653.3	609.0	600.4	601.6	639.5	7929	1022.5	5972.2	9629.0
2000-F01	1140.5	1047.8	982.6	836.2	721.1	651.5	607.4	580.8	601.5	644.3	799.1	1021.8	5987.2	9634.5
%Dif,ActVF01	-0.68%	1.34%	0.49%	-1.68%	-2.12%	0.27%	0.26%	3.38%	0.02%	-0.74%	-0.78%	0.07%	-0.25%	-0.06%
2001 Actuals	1152.5	1040.6	920.8	834.7	742.5	634.4	591.6	0.0	0.0278	0.0	0.0	0.0	5917.2	-0.0070
2001-F01	1138.5	1041.1	9123	820.6	717.6	654.9	6122	568.2	588.8	630.9	797.2	993.8	5897.2	9476.0
%Dif.ActvF01	1.23%	-0.05%					100							94/0.0
70LII,ALIVEUI	ه/بحدا	-0.05%	0.94%	1.73%	3.47%	-3.13%	-3.36%	-100.00%	-100.00%	-100.00%	-100.00%	-100.00%	0.34%	
Commercial(net														
2000 Actuals	675.9	672.2	694.7	564.7	551.6	591.0	580.3	679.7	640.8	6728	608.9	<b>63</b> 0.4	4330.4	7563.0
2000-F01	6823	693.4	663.0	565.8	587.0	595.3	. 593.9	683.6	631.0	607.1	624.6	<b>63</b> 5.9	4380.8	7563.0
%Dif,ActvF01	-0.94%	-3.05%	4.78%	-0.21%	-6.04%	-0.71%	-2.29%	-0.56%	1.55%	10.82%	-2.51%	-0.86%	-1.15%	0.00%
2001 Actuals	701.9	7724	653.2	683.3	624.4	635.0	633.4	0.0	0.0	0.0	0.0	0.0	4703.6	
2001-F01	7129	758.0	667.4	665.2	624.0	636.9	640.2	628.2	659.0	624.4	653.9	740.3	4704.5	8010.3
%Dif,ActvF01	-1.54%	1.91%	-2.12%	272%	0.06%	-0.29%	-1.07%	-100.00%	-100.00%	-100.00%	-100.00%	-100.00%	-0.02%	
ndustrial					÷									
2000 Actuals	129.1	146.4	140.4	127.1	130.4	134.0	121.7	140.6	147.7	144.8	133.6	125.3	929.1	1621.1
2000-F01	126.1	143.0	137.1	124.2	127.4	130.8	118.8	137.3	144.3	141.4	130.4	122.4	907.4	1583.3
%Dif,ActvF01	2.39%	2.39%	2.39%	2.39%	2.39%	2.39%	2.39%	239%	239%	2.39%	2.39%	239%	2.39%	2.39%
2001 Actuals	124.5	136.2	114.9	117.4	117.3	118.8	120.7	0.0	0.0	0.0	2.35%	0.0	849.7	238/0
2001-F01	124.4	136.1	115.0											1404.0
				117.0	117.0	118.5	120.0	121.9	127.6	114.2	116.3	106.3	847.9	1434.2
%Dif,ActvF01	0.05%	0.04%	<b>-</b> 0. <b>06</b> %	0.31%	0.30%	0.21%	0.56%	-100.00%	-100.00%	-100.00%	-100.00%	-100.00%	0.20%	
Street Lights														
2000 Actuals	6.4	6.1	6.7	6.6	6.5	6.2	6.1	6.2	6.4	6.5	6.6	7.0	44.6	77.4
2000-F01	6.7	6.5	6.5	6.4	6.3	6.3	6.2	6.2	6.3	6.3	6.7	7.1	44.8	77.4
%Dif,ActvF01	-4.57%	-5.71%	3.60%	2.82%	2.54%	-1.45%	-0.51%	-0.19%	2.08%	3.13%	-0.90%	-0.54%	-0.50%	-0.01%
2001 Actuals	6.7	6.6	6.2	6.1	7.3	6.3	6.4	0.0	0.0	0.0	0.0	0.0	45.4	
2001-F01	7.3	7.1	7.0	7.0	6.9	6.8	6.8	6.8	6.9	7.0	7.4	7.8	48.9	84.7
%Dif,ActvF01	-7.76%	<b>-</b> 7. <b>28</b> %	-12.38%	-12.53%	5.25%	-8.37%	-6.01%	-100.00%	-100.00%	-100.00%	-100.00%		-7.04%	
Resale							4. j							
2000 Actuals	12.3	124	11.2	12.1	11.4	11.3	11.9	12.2	12.6	44.0	11.8	120	82.6	142.0
2000-F01	123	123								11.9				143.0
			11.1	12.0	11.4	11.2	11.8	12.1	12.5	11.8	11.7	11.9	81.9	141.9
%Dif,ActvF01	0.79%	0.79%	0.79%	0.79%	0.79%	0.79%	0.79%	0.79%	0.79%	0.79%	0.79%	0.79%	0.79%	0.79%
2001 Actuals	126	12.6	11.4	12.3	11.6	11.4	120	0.0	0.0	0.0	0.0	0.0	83.9	
2001-F01	12.5	12.5	11.3	12.2	11.5	11.3	12.0	0.6	0.5	0.3	1.2	0.9	83.3	<b>8</b> 6.8
%Dif,ActvF01	0.79%	0.79%	0.79%	0.79%	0.79%	0.79%	0.79%	-100.00%	-100.00%	-100.00%	-100.00%	-100.00%	0.79%	
ISPs														
2000 Actuals	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	0.0	1.3
2000-F01	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		02	0.4	0.0	0.7
%Dif.ActvF01	#DIV/O	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/O	#DIV/0!	-100.00%			#DIV/0!	83.16%
2001 Actuals	1.0	1.2	1.3	1.9	2.0	21	#DIVIO:	0.0	0.0				11.6	03.1076
2001-F01	0.8	1.0	1.4	1.9	21	23	25	26	26		27	29		ne 4
	36.32%												11.8	25.4
%Dif,ActVF01	JD.JZ/6	17.41%	-8.74%	12.53%	-4.42%	-10.39%	-13.95%	-100.00%	-100.00%	-100.00%	-100.00%	-100.00%	-1.63%	

Ex. \_\_\_\_(WAG-4) Page 49 of 219

### Comparison of F2001 Gas Sales Forecasts versus Weather Adjusted Actuals (Mtherms) Jan Feb Mar JulYTD Apr May <u>Jun</u> Jui Aug Sep Oct Nov Dec -**Total Total** 148.775 141,261 119,745 101,570 2000 Actuals 74.416 59.432 45.770 41.332 44,381 59,960 92,103 126,727 690,969 1,055,472 2000-F01 142,606 136,399 121,408 97,650 76,655 61,742 46,389 42,925 48,327 55,751 96,580 130,958 682,848 1,057,388 %Dif.ActvF01 4.33% 3.56% -1.37% 4.01% -2.92% -3.74% -1.33% -3.71% 7.55% -8.16% -4.64% -3.23% 1.19% 2001 Actuals 138,879 136,089 109,346 97,528 75.577 55,330 43.066 0 ٥ ٥ ٥ 655,816 2001-F01 133,364 142,550 118,379 96,567 70,468 53,307 40,407 35,607 39,240 52,134 89,474 130,781 655.042 1.002.278 %Dif.ActvF01 4.14% -4.53% -7.63% 1.00% 7.25% 3.80% 6.58% 100.00% -100.00% -100.00% -100.00% -100.00% 0.12% Residential 2000 Actuals 79.432 72,791 59.580 46,160 30,268 19.954 13.647 10.880 12.263 23.028 44.066 68.753 321.833 480.822 2000-F01 77.249 68,506 62.749 43.904 31,703 21,792 13,344 9,803 13,741 19,953 46,537 69,761 319,247 479,042 %Dif.ActvF01 2.83% 6.26% -5.05% 5.14% -4.53% -8.44% 2.27% 10.99% -5.31% -10.76% 15.41% -1.44% 0.81% 0.37% 2001 Actuals 77,735 74,906 57,691 46,299 31,138 20.064 12.530 0 0 0 0 0 320,363 2001-F01 71,954 77,259 61,389 46.063 29,947 19,514 11,888 7.919 10,135 19.662 44.340 73.804 318,013 473,873 %Dif,ActvF01 8.04% -3.05% -6.02% 0.51% 3.98% 2.82% 5.41% -100.00% -100.00% -100.00% -100.00% -100.00% 0.74% Commercial 2000 Actuals 29,672 27,597 23,997 19.980 13,735 10.610 8.918 203,626 8.042 8.582 10.568 17,227 24.698 134,509 2000-F01 28,061 26,458 24,423 18.334 7.838 9,145 17.383 14,368 8.826 11.226 10.319 25,684 131,696 202.064 %Dif,ActvF01 5.74% 4.31% -1.74% 8.98% -4.40% -5.49% 1.04% 2.60% -6.15% 2.41% -0.90% -3.84% 2.14% 0.77% 28,949 2001 Actuals 27.976 23.813 20,204 15,034 10,872 8,098 'n 134,945 0 n 0 0 2001-F01 28.854 29.896 25,912 18,982 13,477 9.777 7,618 6,661 7.692 10,117 17,190 26,112 134.516 202,288 %Dif.ActvF01 0.33% -6.42% -8.10% 6.43% 11.55% 11.20% 6.29% -100.00% -100.00% -100.00% -100.00% -100.00% 0.32% Industrial 2000 Actuals 5,708 5,065 4,754 4.083 3,368 2,840 2.633 2.501 2.472 2.775 3.703 4.580 28.452 44,483 2000-F01 5,399 5,140 4,933 4.123 3.001 2.712 3.484 2.484 3.836 28,791 2.692 2 824 4.564 45.192 %Dif,ActvF01 5.73% -1.46% -3.61% -0.97% -3.34% -5.35% -2.90% 0.67% -8.17% -1.76% -3.46% 0.36% -1.18% -1.57% 2001 Actuals 5.211 4.965 3.609 3,725 3,812 2,753 2,742 ٥ ٥ 0 0 0 26,817 2001-F01 5.427 5.280 3.977 3,936 3,117 2,582 2,391 2,175 2,333 2,574 3,382 4,388 26,709 41.561 %Dif.ActvF01 -1.31% -8.51% -9.24% -5.36% 22.30% 6.64% 14.67% -100.00% -100.00% -100.00% -100.00% -100.00% 0.40% Coml Interr/LV 2000 Actuals 11,806 13,313 10,542 10,092 7.641 6,456 4,864 4,299 4,191 5.792 7,588 10,254 64,713 96.838 2000-F01 11.379 15,272 10,418 9,206 8,097 7.298 5.267 6.527 10.694 4.768 5.542 8.736 66.939 103,206 %Dif.ActvF01 3.75% -12.83% 1.18% 9.62% -5.63% 11.53% -7.65% -34.13% -12.11% 4.52% -13.15% -4.12% -3.32% -6.17% 2001 Actuals 11,147 10.583 7.934 9.716 7.743 5.853 4.958 n 0 n n 0 57,933 2001-F01 10.963 11.540 10,064 8.816 7,272 5,811 4,364 4,617 4,200 4,952 7,069 9,525 58,830 89,193 %Dif.ActvF01 1.68% -8.29% -21.17% 10.21% 6.47% 0.72% 13.62% -100.00% -100.00% -100.00% -100.00% -100.00% -1.52% Indust Interr/LV 2000 Actuals 1,980 2,283 1,949 2,151 1,943 1,755 1,665 1,330 1.664 1.431 1.587 1.384 13.726 21,122 2000-F01 1,755 1,837 1,694 1,801 1,631 1,628 1,493 1,466 1,489 1,599 1.782 1,727 11.840 19.904 %Dif,ActvF01 12.82% 24.28% 15.03% 19.42% 19.10% 11.55% -3.94% 7.78% -9.32% -6.60% -0.74% -19.88% 15.93% 6.12% 2001 Actuals 1,250 1.298 1.340 1,499 1.767 1.483 1,208 n n ٥ ٥ n 9.845 2001-F01 1,533 1,601 1.415 1.458 1.510 1,308 1.290 1,228 1.194 1.209 1,316 1.505 9,928 16.569 %Dif,ActvF01 -18.44% -18.91% -B.11% -0.70% 35.04% 14.94% -1.66% -100.00% -100.00% -100.00% -100.00% -100.00% -0.84% Comi Transport 2000 Actuals 1,778 1,867 1,636 1,650 1,626 1,524 1,394 1,360 1,380 1,361 1,578 1,905 11,476 19,059 2000-F01 1.541 1,748 1.566 2,045 1,338 1.629 1.399 1,341 1,365 1,418 2,154 2,905 11,265 20.448 %Dif.ActvF01 15.38% 6.85% 4.50% -19.31% -0.13% 8.92% 4.17% 1.40% 1.10% -3.99% -26.76% -34.44% 1.87% -6.79% 2001 Actuals 1,625 1,806 1,676 1.990 2.151 1.581 1,450 ٥ · 0 n n ٥ 12,279 2001-F01 2.217 2.283 2.067 2.213 1.924 1.669 1.583 1.565 1,536 1,472 1,909 2,200 13,957 22,638 %Dif.ActvF01 -26.72% -20.90% -18.95% -10.08% -8.39% -100.00% 11.80% -5.22% -100.00% -100.00% -100.00% -100.00% -12.02% Indust Transport 2000 Actuals 18.399 17,286 18,343 17,455 15,834 16,293 12,649 12,921 13,830 15,006 16,354 15,153 116,259 189,523 2000-F01 17,221 17,437 15.625 18,237 15,742 15,397 13,409 13,465 14,834 14,206 16.335 15.623 113,070 187.533 %Dif,ActvF01 6.84% 5.19% 10.63% -4.29% 5.82% -4.04% -6.77% 5.63% 0.58% -5.67% 0.12% -3.01% 2.82% 1.06% 2001 Actuals 12.962 14.555 13.284 14.096 13.933 12,724 12.081 ٥ Λ 93,633 n n n 2001-F01 12.563 14,545 13.513 15.047 13,423 12,664 11,335 11,477 12,134 12,040 14,169 13,246 93.089 156,156 %Dif.ActvF01 3.17% 0.07% -1.69% -6.32% 3.80% 0.47% 6.58% -100.00% -100.00% -100.00% -100.00% -100.00% 0.58%

### RESOURCES

Ex. \_\_\_\_(WAG-4) Page 50 of 219

			Nameplate/	Capacity	Average Energy	Average Average Average Energy Energy Energy	Average Energy	Heat	Power Purchase	Emissions	<b>J</b> O <b>*</b>	¥	Received/	
	Location	Fuel	Capacity	Degrad	(,01)	(1066.)	Price	Rate	Contract Term	Restrictions	Units	Units Ownership Peaking	Peaking	
PSE OWNED GENERATION							UMM/S							
Baseload:			(ALLA CILL)				l	r						L
Colstrip Units 1&2	Colstrip	coal	330.00	295.00	267.2	256.9	\$10.08	E			ľ	¥.	50 hasaload	ļ
Colstrip Units 3&4	Colstrip	coat	370.00	370.00	307.8	293.5	\$9.61	10.6			Î	0	25 hasaload	1
Encogen (acq. 11/99)	Bellingham ga	jas/oil	160.00	160.00	162.8	114.7	\$56.02	8.7		8760 permitted	1		100 reaking	1
Upper Baker River (1959)		hydro	103.00	103.00							ſ		100 baseload	╀
Lower Baker River (1960)	•	hydro	71.40	71.40				l				2	100 haseload	ļ
Electron (1929)	Electron hy	ydro	26.40	21.00				Ī				9	100 baseload	$\downarrow$
Snoqualmie Falls (1910/1957)	lie I	ydro	44.00	42.00								2 5	100 haseload	$\downarrow$
White River (1911/1924)	Dieringer	ydro	63.40	63.40			-				ľ	9	100 bassload	$\downarrow$
Subtotal Hydro:					125.6	153.7	\$7.97					2	Dasgroad	$\downarrow$
Subtotal Baseload:			1168.20	1125.80	863.4	818.8		T						1
								<u> </u>						ļ
Peaking:								t						1
Whitehorn 2	Femdale ga	as/oll	74.00	66.40				11.7		8750 narmittad	•		100 peabling	8
Whitehorn 3	Femdale ga	as/oil	74.00	00.89	88.4	52.7		41.7		8780 permitted			TO POSICIO	
Frederickson 1	Spanaway ga	jas/oil		70.00				11.7					Riman	
Frederickson 2	Ť	as/oil	144.00	71.00	65.7	35.9		11.7		NOX restrictions	-	Ē	100 peaking	1
Fredonia 1	٦	as/oil	104.00	101.40				11.5		Unit 1 restricted		10	100 peaking	L
Fredonia 2		jas/oil	104.00	100.70	108.8	108.8		11.5		Unit 2 unrestricted	-	ğ	Deaking	L
Fredonia 3 & 4 (Oct-Dec)	3	as/oil	108.00	108.00	12.8			10.4		Unit 3 unrestricted	Ī	Ē	100 peaking	leas
Crystal Mountain	Ť		2.75	2.75	1.1	0.4		_		Unit 4 unrestricted	-	Č	100 peaking	L
Plerce Power	Fredrickson ga	as/olf	154.00	154.00										
Subtotal Peaking:			764.75	742.25	256.8	197.8		H						

Power Supply Resources - 2002

Total PSE Owned Generation:

1932.95 1868.05

Power Supply Resources - 2002 (m. resources that terminate over next 9 years)

			Nameplate/	Capacity	Average A Energy E		Average Energy I	Heat	Power Purchase	Emissions	Jo #	×	Resolved/	Fyniretion
	Location	Fuel	Capacity	1		(1066.)		Rate	Contract Term	Restrictions	Units	0		Date
PURCHASED POWER CONTRACTS						L	$\mid$	T						
Mid C receipt:								T						
	Douglas PUD	hydro	263.00		86.7	132.6	\$11.50	6	9/18/63-8/31/2018		9	313	pasaload	8/31/2018
	Chelan PUD	hydro	505.00		171.2	254.2	\$17.87	-	11/14/57-11/1/2011		Ξ		baseload	11/1/2011
	Chelan PUD	hydro	124.00		11.9	4	\$30.57	٦	12/20/1995-6/7/2012		2			6/7/2012
nd II	Chelan PUD	hydro	333.00		144.6	234.8	\$22.40	٦	12/20/1995-6/7/2012		•			6/7/2012
	Grant PUD	hydro	96		38.4	52.7	\$11.60	Ø	6/22/59-10/31/2009		9		10.8 baseload	10/31/2039
st Rapids	Grant PUD	hydro	72		31.1	41.1	\$7.26	2	5/21/56-10/31/2005		9		8 haseload	10/31/2035
Subtotal MId-C:			1395.00		483.9	719.4								2004
						Н	H						,	
System Delivery Receipt;														
Avista		thermal	33,00		50.2	288	\$23.40	7	1/1/1988-12/31/2002				hasalnad	12/31/2002
BPA-Baker Replacement		hydro	7		8.0	-		G.	9/30/2000-9/30/2006				Seasonal	9/30/3006
BPA-Snohomish Conservation		hydro	21		8.2	6.7	\$37.42	6	3/1/90-2/28/2010				haceload	2/28/2010
BPA-CSPE		hydro	59		12.7	18.5	\$0.00	4	4/1/68-3/31/2003				haselned	8/31/2003
BPA-Supplemental Capacity		hydro	8		0.5	80	\$18.13	4	4/1/88-3/31/2003				pasking	201000
BPA-WNP3 BPA Exchange(LCP)		thermat	82		44.4	54.1	\$27.70	ð	9/30/2000-6/30/2017				Poologd Poologd	6/20/2047
Canadian Entitlements (Mid-C) Exist		hydro	Q.		8		2111	5	OULTOO GOOKEDII				Daseload	0/30/2017
Canadian Entitlements (Mid-C)Ext		hydro	41		2 6	-		1	4/4/4000 0/4E/0004				mnei	3/31/2003
1000	Colebdo	init con	40		0.0	2 04	2000	7	1/1930-9/10/2024			a service of the serv	unie.	9/15/2024
Darillo Dower & I Inhi (Darill Corn	Constitute	the collin	600	ĺ	0.10		80078		W1/1989-12/31/2010				baseload	12/29/2010
DOSE Curhomas Mari Cabi		I POLICIOI	202		9781	118.7	246.02		11/1/1988-10/31/03				baseload	10/31/2003
roac exchange (nov-1 eb)		(nermai:	000			9		1	1/1/1992thru				exchange	12/31/2006
TODGITS		gipku	7		2.5	2.3	\$27.80	=	10/01/2001-9/30/2004				baseload	9/30/2004
	The Dalles	hydro	2		5.1	4.5	\$63.79	//	7/1/91-12/31/2012				baseload	12/31/2012
Subtotal System Delivery:			735.00		300	353.4								
(														
Jens:														
	Anacortes	gas	8		81.7		\$53.69	8.5 10	10/1/1991-12/31/2011		2		baseload	12/31/2011
Point Phase II	Anacortes	gas/stean	9		53.6		\$60.48	8.5 11	11/1/91-12/31/2011		~		baseload	12/31/2011
	Bellingham	gas	123		125.9		\$72.85	8.24/	4/16/1993-12/31/2012		2		baseload	12/31/2012
	Bellingham	gas/oil	245		220.7		\$67.90	8.73	3/20/1991-12/31/2011		က		baseload	12/31/2011
Subtotal Cogens:			508		481.9	429.3								
OF Contracts - Blomace & Hodro.				$\dagger$	+	+		$\dagger$						
	Privallin	Harmal	6		C	9			Merenna are mana		-			
	Spokane	thermal	200		15.6		20 20		#10/1685-#10/cos				paseload	4715/2009
	Rellingham	hidm	9.0		200	-	200.70		11930-3/1/2011		0.0000	Company Charles	baseload	11/1/2011
	Coorcete	27.4	19.7		300	ź	27.00		1000 to 000 to 0		4		Daseload	9/30/2004
1 Dense	Ophin and Property	2007	7.00		0.0	4.6	974.00	-	121/1990-12/31/203/				baseload	12/31/2037
	DUBSIMO I TIO	mysio	0.5.0		0.2	3	\$23.67	7	1/1/99-12/31/03				baseload	12/31/2003
gy-Sygitowicz	Whatcom	hydro	0.4	-	0	0	\$47.80	2	2/22/95-2/2/2014		-		baseload	2/2/2014
huk	Centrailia	hydro	0.98		0	0	\$16.00	//	7/1/1993 -				T	ongoing
	Snoqualmie	hydro	R		6.2	6.4	\$75.00	3	3/8/1990-3/2025				baseload	3/8/2025
	Snoqualmie	hydro	4.6		1.2	1.4	\$75.00	112	12/1/1987- 12/31/2022				baseload	12/21/2022
Subtotal Biomass/Hydro:			68.855		28.9	ļ,		-			T			
													1	

2706.86

Total Purchased Power:

### CONTRACT ABSTRACTS

### **CONTRACT ABSTRACTS:**

**Avista** 

Description: Thermal

Delivery Point: Mid-C between Wells and Priest Rapids hydroelectric projects and any other

point where WWP has available transmission

Firm Capacity = Contract Demand = 100MW (1988-2000); 67MW (2001); 33MW (2002)

Energy = Contract Demand x.75 x # of hours in contract year

75% annual load factor; 75% weekly load factor; PSE may schedule energy at a delivery

rate of not < 30% of Contract Demand and must maintain weekly load factor;

Contingency for delivery interruption due to uncontrollable events: Seller shall make available the difference above 10%.

Scheduling: Preschedule by 12:00pm

Fifteen Year Agreement for Purchase & Sale of Firm Capacity and Energy dated 10/16/95

Price: \$32.11/MWh Average /Power Cost for 1995-2002

Term: 1/1/1988-12/31/2002 **Expiration: 12/31/2002** 

**Baker River Replacement Power** 

Description: Hydro, Upper Baker flood control extension, PSE compensated for storage space provided in excess of 16,000 (11/1-3/1), + an additional 58,000 acre feet between 11/15-3/1).

Compensation provided in the form of replacement energy (capacity + losses).

Point of Delivery: Sedro Woolley

Capacity: Not to exceed 7MW hourly rate, unless agreed to by PSE and BPA

Energy:

Scheduling: November-February, 1750 total MWhr/month

(7000 total MWhrs for the term 11/1-3/1)

Memorandum of Agreement between the Corps of Engineers, Department of the Army acting by and through the Division Engineer, Northwestern Division and PSE for Upper Baker Additional Flood Control dated 10/31/2000

(Agreement Between the Corps of Engineers and BPA for Replacement Power for Upper Baker Flood Control date 10/27/2000)

Price:

Capacity: Corps pays BPA for the firm capacity scheduled to PSE pursuant to BPA's wholesale firm capacity tariff

Energy: Corps pays BPA for non-firm energy at the higher of: 1)avg of the 16 highest days of the DJ Mid –C Index for HLH firm power or 2) avg of the 16 highest days average of hours 7-22 of the Cal PX Day Ahead Unconstrained Market Clearing Prices.

Term: 9/30/2000-9/1/2003; may be extended on an annual basis until 9/30/2006 to coincide with the issuance of a new FERC license.

Expiration: 9/1/2003 or 2006

Columbia Storage Power Exchange (CSPE)

Description: Hydro, entity was incorporated in 1964 with objective of purchasing for a term of years Canada's rights (one-half) of the downstream power benefits under the Columbia River Treaty (signed by the US 1/17/61) and incurring indebtedness to finance such purchase. CSPE assigns to Participants the Canadian Entitlement based on Participant's percentage. Participants pay BPA for use of BPA's transmission. The treaty and the notes exchanged provided pursuant to the Treaty provide for the construction, maintenance and operation by Canada of storage dams and reservoirs in B.C. on the Columbia River at Mica Creek, Arrow Lakes and near Duncan Lake. The benefits of the Treaty are created in the US due to the construction of the Projects ability to improve usability of water out of Canada.

Delivery Point: PSE's system or Rocky Reach Project

Capacity: approximately 20MW (2001-2002); 30MW (2002-2003)

Ex	(WAG-4)
Page 53	of 219

Energy: approx. 20MW (2001-2002); 16MW (2002-2003)

Losses: Energy 3.5%; Peak 5.5%

Transmission: BPA to deliver energy and capacity less losses to the point of delivery. BPA

capacity charge: \$0.125/month x kilowatts of capacity

Term: 4/1/68 - 3/31/03

### Agreements:

1. Canadian Entitlement Purchase Agreement between CSPE and BC Hydro dated 8/13/64 for purchase of Canada's entitlement benefit for a specified number of years (through 3/31/2003)

2. Canadian Entitlement Allocation Agreement - to implement the Treaty it is necessary for the Administrator to make available to the District certain amounts of capacity as stated in this agreement in order to return one-half of the dependable capacity resulting from the construction

of the Canadian storage projects and to realize the benefits of such construction

Canadian Entitlement Exchange Agreements between BPA and CSPE dated 8/13/64 - provide for payments by the Participants to BPA for the use of the Government's transmission, transformation and related facilities in making capacity and energy available, also contains provisions describing the character of service and the scheduling arrangements for capacity and energy to be supplied by BPA and provisions whereby the participants and BPA may effect exchanges

Price:

Term: 8/13/64-3/31/03 Expiration: 3/31/03

### **CSPE - Supplemental and Entitlement Capacity**

Description: BPA to provide additional capacity rather than install additional units for capacity.

Allows for shaping capability.

Capacity: approx.10MW (2001-2002); 9MW (2002-2003)

Energy: PSE returns 10MW on LLH and receives 9 MW on HLH - net transfer "0" at month end

Losses: Energy 3%; Capacity 5.5%

Transmission: BPA to deliver energy and capacity less losses to the point of delivery; \$1.50/kw/month; transmission charge, \$4.50/kw/month of supplemental capacity charge.

Term: 4/1/68 – 3/31/03 Expiration: 3/31/03

### **Delivery of the Canadian Entitlement**

Description: Treaty terms: U.S. and Canada each entitled to receive one-half of the average annual usable energy and one-half of the dependable hydroelectric capacity for the next 60 years. (Canada sold its half for first 30 years to CSPE 4/1/68-4/1/98). BPA to deliver Canada's half from US projects.

Capacity: 2001-41MW; 2002-38MW 2003-68MW 2004-68MW 2005-66MW 2006-61MW

Energy: approx. 40aMW

Points of Delivery: Nelway, Waneta, Blaine 1, Blaine 2

Scheduling: Daily preschedule basis; B.C. Hydro to provide a weekly and a mid-week estimate. Weekly provided by 10am Friday thru following Friday. Avg. annual energy prorated based on number of days. Total deliveries in any hour will not exceed Canadian Entitlement capacity

Term: 4/1/98-9/15/2024 Expiration: 9/15/2024

### Conservation Credit with Snohomish PUD

Description: Hydro, conservation transfer pilot program with certain utilities and BPA. The amount of power purchased will roughly match the conservation savings during the first 5 years. Beginning March 2001, Snohomish will sell supplemental power to PSE.

Delivery Point: BPA to deliver to Monroe/Sammish and Sedro Woolley (Murray/Bellingham) thru 2001; Beverly Park 2001-

Capacity/Energy: 12 MW during HLH (0600-2200) and 8 MW during LLH

Contract	Energy	Supple-	Total
Year	in MWh	mental	
3/01-2/02	52,563	27,921	80,484
3/02-2/03	52,563	20,288	72,851
3/03-2/04	52,747	40,429	93,176
3/04-2/05	52,563	40,288	92,851
3/05-2/06	52,563	40,288	92,851
3/06-2/07	52,563	40,288	92,851
3/07-2/08	52,747	40,429	93,176
3/08-2/09	52,563	40,288	92,851
3/09-2/10	52,563	40,288	92,851

Conservation Power Sales Agreement dated 12/11/89

Amendment No.2 to the Conservation power Sales Agreement dated 12/28/2001 – establishes new price methodology

Price: Base Rate-\$32.00 + Adder

### \$/MWH

2002	\$40.50
2003	\$40.80
2004	\$41.10
2005	\$41.40
2006	\$41.70

Term: 3/1/90-2/28/2010 **Expiration: 2/28/2010** 

### Montana Power Company

Description: 10 year contract; Montana has 30% share (210MW) in Colstrip 4 (700MW), not

dedicated to serve Montana's jurisdictional load

Delivery Point: Montana Power has the obligation to provide firm contractual rights to

transmission paths from Garrison to the Point of Delivery. PSE has IR Agreement with

BPA which satisfies this obligation thru the Term.

Displacement: Yes

Contract Capacity: 97MW (Amendment 7/13/98 increasing capacity from 94 to 97MW). No additional fixed monthly charge for additional 3MW upon a one time payment of the lessor a) one-half of the capital cost of such replacement or b) \$900,000

Energy: Amount scheduled shall be a) contract capacity or b) contract capacity x net

generating /nominal rating. Supplemental energy up to 120MW

Scheduling: PSE submits hourly preschedule

### Power Sales Agreement dated 10/1/89

Settlement Agreement dated 2/21/97 - monthly fixed charges reduced by \$6500/mo.

Amendment No.1 to Power Sales Agreement - increases capacity

Price: Energy: Based on the Existing Coal Agreements or any modifications thereto

Monthly Fixed Charge Rate:

2002 - \$24,935

2003 - \$26,358

2004 - \$27,692

2005 - \$29,078

2006 - \$30,434

2007 - \$31,750

2008 - \$33,040

2009 - \$34,321

2010 - \$35,574

Term: 10/1/89-12/29/2010 Expiration: 12/29/2010

**PacifiCorp** 

Description: 15 year term

Delivery Point: Mid-C and additional points which PacifiCorp has available transmission rights or

facilities

Contract Capacity: 200MW (8/1/91-10/31/03); 100 (12/1/88-7/31/91) Energy: Monthly load factor of 70%, weekly load factor of 75%

Scheduling: By Feb 1, PSE shall submit to PacifiCorp a nonbinding monthly estimate for 12 mos. beg. 7/1. Preschedule by 12:00. PSE shall receive energy at a load factor of 60% for

each year (Aug-July).

Fifteen Year Power Sales Agreement dated 10/27/88

Price:

Energy rate- approximately \$18.00/MWh; calculation and data submitted by PacifiCorp. based on the Centralia production expense and Bridger production expense on

PacifiCorp's FERC Form 1

Capacity rate-

2002 capacity rate = \$15.08/kw/mo. 2003 capacity rate = \$16.13/kw/mo.

Term: 11/1/88-10/31/03 **Expiration: 10/31/2003** 

### PG&E Seasonal Exchange Agreement

Description: Seasonal exchange of power, no monetary exchange

Delivery Point: BPA/Southern Intertie (COB or NOB), PSE holds transmission contract (network

transmission) Puget/Bonneville Intertie & Network Transmission Agreement

Capacity: 300MW

Energy: PSE receives 413,000 MWh of energy Nov-Feb.

PSE delivers 413,000 MWh of energy to PG&E June-Sep

Scheduling:

PG&E delivers to PSE November-February PSE delivers to PG&E June –September

Most of the energy is delivered during HLH. Hourly energy schedule submitted for Monday-Sunday. Not to exceed 300 MW for any hour, nor more than 2 changes during any day (best efforts), and not less than 25% of the highest rate

of delivery scheduled for any hour delivered for such day

Capacity and Energy Exchange Agreement dated 10/4/91

Puget/BPA Intertie Network Transmission Agreement dated 10/4/91

Mitigation Agreement between BPA and PG&E dated 10/4/91

Price: n/a

Term: 10/4/91-12/31/2006. PSE has given PG&E notice of termination as of 12/01

Expiration: 12/31/2006

### Point Roberts/BC Hydro/Powerex

Description: power purchase to serve Pt. Roberts load (physically isolated from PSE's system)
Delivery Point: US/Canadian Border, south end of 56<sup>th</sup> Street, B.C. Canada where the electrical

facilities of PSE and BC Hydro are interconnected.

Capacity: 8MW Energy: 3 aMW

Scheduling: Full requirements

Agreement for Power Purchase dated 10/1/2001

Price: \$67.00/MWh Term: 10/1/01-9/30/2004 Expiration: 9/30/2004 WNP3 Settlement Exchange Agreement

Description: Settlement of BPA nuclear project whereby PSE had a 5% ownership and BPA terminated the project. Allows PSE to be in essentially the same power supply situation proportionate to its investment if construction had been completed by 1983.

**BPA Exchange:** PSE receives an equivalent amount of power based on availability factor of 4 surrogate nuclear units Palo Verde, Unit 1, Arkansas Nuclear One- Unit 2, Waterford Unit 3, and San Onofre 3. The minimum amount of replacement energy PSE is entitled to receive is 5.833,333MWh.

Delivery Point: Maple Valley or Satsop

Scheduling: BPA delivers to PSE November-April. Rate of delivery Nov-Feb shall not exceed 82MW during HLH. During March and April HLH shall not exceed 41MW. Preschedule

to BPA by 11:00am. Final preschedule by 2:00pm

PSE's price to BPA: Based on formula calculation in contract.

Transmission: 32,220 kw, transmission charge \$0.375/kw/mo.; BPA's rate schedule FPT-02.1

**PSE Exchange**: BPA has a call on PSE's CTs except in the months of May, July and August and pursuant to resource availability.

BPA's price: all incremental generating costs including gas cost, pipeline transport, taxes, O&M Scheduling: BPA submit preschedule by 9:00am, PSE shall respond by 11:00 am. Final

preschedule by 2:00pm. Maximum rate of delivery 117MW

Settlement Exchange Agreement dated 1985

Term: 9/30/2000-6/30/2017

Expiration: estimated to be 6/30/2017

### WASCO

Description: hydro

Generating Capacity: 5MW, 1 unit

Licensing: FERC license issued 12/31/87 (#7076-002)

Location: The Dalles Dam

Outages/Maintenance: May-July (coordinated with PSE), notice provided on or before Jan. 1 of each year for 18 month maintenance schedule

Point of Delivery: Where the project is interconnected with BPA (Klickitat switching station

directly connected to BPA's Spearfish sub)

Transmission: from POD to PSE's system, wheeled by BPA under a separate wheeling contract

Agreement for Firm Power Purchase dated 10/24/88 - entire net electrical output. Operation of the project is limited by governmental agencies having jurisdiction over the project (i.e.Corps of Engineers)

Transmission Agreement between Klickitat and WASCO dated 7/25/89 Price: \$.0077/kwh x escalation quotient + Exhibit C (below) x amount

WASCO reimburses PSE for losses plus any costs or expenses for wheeling

Exhibit C

 Winter
 Summer

 2001-2012
 \$68.76
 \$33.23

Term: 7/1/91 - 12/31/2012; 21 year contract

Expiration: 12/31/2012

### **QUALIFYING FACILITIES (QF's)**

### **Cogens**

March Point Phase I

Description: 20 year contract, cogeneration, 2 GE Frame 6 units each 35-45MW

Displacement: Yes. Prior to each delivery month Seller shall provide PSE with written notice of its incremental generation rate for such month. PSE shall displace Seller if it determines that replacement power may be less than the incremental generation rate and that such displacement shall not interfere with the operations of the Sellers facility

Generating Capacity: 80MW

Heat Rate: 8400-8500 full capacity; 11,200-11,700 under displacement conditions

Location: Anacortes, WA

Outages/Maintenance: May-July, scheduled 18 mos. in advance; notice provided 1/1 each year

Scheduling: Flat, around the clock

Point of Delivery: Where the project is interconnected with PSE's electrical system

Agreement for Firm Power Purchase dated 6/29/89 - entire net electrical output Summer (April-Aug) = quotient index x base rate of 7.70 mills+ Exhibit B rate

Winter (Sept-Mar) = quotient index x base rate of 7.70 mills + Exhibit B rate

### \$/MWhr (Estimated)

2001	60.72	43.32
2002	61.03	43.63
2003	61.35	43.95
2004	61.67	44.27
2005	62.01	44.61
2006	62.35	44.95
2007	62.71	45.31
2008	63.07	45.67
2009	63.45	46.05
2010	63.84	46.44
2011	64.24	46.84

Term: 10/1/91-12-31/2011 Expiration: 12/31/2011

### **March Point Phase II**

Description: 20 year contract, cogeneration, 1 GE Frame6 turbine 40MW, 1 steam turbine 20MW Displacement: Yes. Prior to each delivery month Seller shall provide PSE with written notice of its incremental generation rate for such month. PSE shall displace Seller if it determines that replacement power may be less than the incremental generation rate and that such displacement shall not interfere with the operations of the Sellers facility

Excess Energy Sales Agreement - Yes

Generating Capacity: 60MW

Heat Rate: 8400-8500 full capacity; 11,200-11,700 under displacement conditions

Location: Anacortes, WA

Outages/Maintenance: May-July, scheduled 18 mos. submitted Jan1

Scheduling: Flat, around the clock

Point of Delivery: Where the project is interconnected with PSE's electrical system

Agreement for Firm Power Purchase dated 12/27/1990 - entire net electrical output Price: Summer (April-Aug) = quotient index x base rate of 8.0 mills+ Exhibit B rate Winter (Sept-Mar) = quotient index x base rate of 8.0 mills + Exhibit B rate

\$/MWhr (Estimated)

2001	63.52	52.92
2002	65.24	54.24
2003	66.97	55.57
2004	67.91	57.21
2005	68.65	58.25
2006	70.51	59.51
2007	71.48	61.48
2008	72.36	63.46
2009	73.45	65.35
2010	74.46	67.16
2011	76.57	69.27

Term: 11/1/91-12-31/2011 **Expiration: 12/31/2011** 

Sumas

Description: 20 year contract, cogeneration, 1 gas turbine, 1 steam turbine

Displacement: Yes

Generating Capacity: 125MW; cannot exceed 135MW

Heat Rate: 8208 @ 125MW full capacity;

Location: Anacortes, WA

Outages/Maintenance: May-July, scheduled 18 mos. submitted Jan1

Scheduling: Flat, around the clock

Point of Delivery: Where the project is interconnected with PSE's electrical system

Agreement for Firm Power Purchase dated 2/24/1989 - entire net electrical output

Amendment to Agreement for Firm Power Purchase dated 9/30/91: operating period shall be 20

years after date of commercial operation.

Price: Summer (April-Aug) = quotient index x base rate of 7.70 mills+ Exhibit B rate

Winter (Sept-Mar) = quotient index x base rate of 7.70 mills + Exhibit B rate

\$/MWhr (Estimated)

WILLIAM!	ii (LSuinat	eu)
2001	82.10	59.00
2002	81.22	58.32
2003	82.74	59.54
2004	84.28	60.88
2005	85.93	62.23
2006	87.59	63.6
2007	74.96	49.86
2008	76.34	50.94
2009	77.73	51.93
2010	79.23	53.03
2011	80.64	54.24
2012	81.07	54.67
2013	81.51	55.11

Term: 4/16/93 -12/31/2012 Expiration: 12/31/2012 Tenaska/PSE

Description: Qualifying Facility (QF), 2 combustion turbines, 1 steam turbine. 1998-Contract

restructuring, PSE supplies natural gas (approx. 50,000 MMBtu)

Capacity: 245MW; Maximum of 280MW

Delivery Point: Where the project is interconnected with PSE's electrical system

Displacement: Yes Energy: 117 aMW

Heat Rate: 8.7 full capacity; 11.4 for excess energy

Location: Ferndale, WA

Maintenance: May and June unless otherwise agreed to

Scheduling: Prescheduling by 9:00am, Tenaska shall notify PSE of hourly estimates of

project generation for next 7 succeeding days.

Agreement for Firm Power Purchase dated 3/20/91 – entire net electrical output

Gas Purchase Agreement between PSE and Tenaska Washington Partners, L.P. dated 1/1/98

DCQ = 50,000 MMBtu; terminates 12/31/2011; coincident with Power Purchase; delivery point: 1) NWPL-Sumas; 2) NWPL/Cascade at Bellingham; 3) Westcoast/Cascade at

Sumas; price is Gas Daily index for NWPL-Sumas + \$.06/MMBtu

Amendment No. 2 to the Firm Power Purchase dated 1/1/98 – establishes new contract rate

Amendment No.3 to the Firm Power Purchase dated 12/1/99 – Displacement formula

Amended and Restated Excess Energy Sales Agreement dated 8/1/2001 – price = Excess Energy Generation Cost + (Market Price – EEGC)/2

Excess Sales Agreement 6/1/2001 – When not displaced then (a) if 1 gas turbine and 1 steam turbine on line then excess is quantities over 140MW (b) if 2 gas and 0 steam on line then excess is quantities over 164MW; (c) if 1 gas on line then excess is quantities over 85MW

Price/Contract Rate= rate+ (heat rate x fuel costs)/1000

Year	Rate/\$/MW	HeatRate
2001	31.30	8303
2002	32.20	8340
2003	31.70	8377
2004	33.50	8414
2005	33.90	8450
2006	35.60	8266
2007	33.90	8303
2008	32.70	8340
2009	31.20	8377
2010	29.10	8414
2011	26.80	8450

Term: 4/1994-12/31/2011 Expiration: **12/31/2011** 

Ex.	(WAG-4	1)
Page 6	0 of 219	

### **QUALIFYING FACITILITIES (CONT.)**

### Small Hydro/Biomass

### Kingdom Energy Products - Sygitowicz Creek

Description: small hydro, 1 generating unit

Generating Capacity: 400 kw

Licensing: 7/14/82; transferred to Kingdom (5069-001) Order Granting Exemption from licensing

requirements under the Federal Power Act Location: Van Zandt, Whatcom County

Outages/Maintenance: May-July or as otherwise requested by PSE; written notice of 12 month

outage schedule

Point of Delivery: Where energy from Project is to be delivered to PSE's electrical system

Scheduling: N/A; Energy supply does not schedule volumes less than 1 MW

Agreement for Firm Power Purchase dated 1/1/95 – entire electrical output of the Project (less any energy used in connection with the operation of the Project)

Purchase Price:

2001 - \$47.90 2002 - \$49.60

2003 - \$51.50

2004 - \$53.50

2005 - \$56.07

2006 - \$58.76

2007 - \$61.58 2008 - \$64.54

2009 - \$67.63

2010 - \$70.88 2011 - \$74.28

2012 - \$77.85

2013 - \$81.58

Term: 1/1/1/95-2/2/2014; 19 year agreement; can be extended

Expiration: 2/2/2014

### Koma Kulshan

Description: small hydro, diversion dam Generating Capacity: 13.7 MW nominal rating Licensing: FERC license issued 4/13/87 (#3239)

Location: near Concrete, WA

Outages/Maintenance: May-July or as otherwise requested

Point of Delivery: where the Project is interconnected with PSE's system

Agreement for Purchase of power dated 2/21/85

Price: Capital component of 66.7mills/kwh + any additional capital costs + O&M (based on GDP implicit price deflator)+ taxes and insurance. Price is generally in a range of \$74-\$79/MWhr)

Term: 12/1/90 – expiration of FERC license 50 years

**Expiration: 12/1/2037** 

Description: 3 units, 925 kw each (3516 Caterpillar uprated landfill gas engines)

Generating Capacity: not less than 2,775kw Location: Puyallup, WA, Hidden Valley Landfill

Outages/Maintenance: May and June; submitted to PSE 60 days prior to the next calendar year Point of Delivery: Interconnected to PSE, retail purchasers Land Recovery, Inc. and Puyallup Sand & Gravel, Inc.

Agreement for Firm Power Purchase - entire electrical output less energy used for project Energy Price: Dow Jones on/off peak and 24 hour firm pricing, weighted average of the 3

Ex	(WAG-4)
Page 61	

Capacity Payment: \$3.00/kw/month multiplied by the sum of the capacity of all the Units Option Price: \$5,000/monthly; \$49,950.00 as an advance payment of part of the price for

capacity for the first six calendar months of the Operating Period Right of First Refusal: \$15,000/month during Operating Period

Provision for Green Power

Term: 4/15/99-4/15/2009, 10 year contract

Expiration: 4/15/2009

### Port Townsend Paper Corporation

Qualifying Facility (QF) status Description: small hydro, 1 unit

Generating Capacity: 375 kw nominal rating

Licensing: Project is exempt from licensing requirements under the Federal Power Act

Location: Port Townsend, WA

Outages/Maintenance:

Point of Delivery: where the project is interconnected with PSE's electrical system Scheduling: N/A; Energy supply does not schedule volumes less than 1 MW

Agreement for Firm Power Purchase dated 1/1/99- for entire net electrical output generated

Price: electrical output x long term avoided cost rate

### \$/MWh

	2001	2002	2003	
Jan	30.7	32.4	33.6	
Feb	28.1	30.7	31.9	
Mar	22.8	24	25.4	
Apr	20.1	20.9	21.9	
May	17.6	19.2	20	
Jun	18	19.3	21.4	
July	24.5	26	27.3	
Aug	26.1	27.6	31.4	
Sept	28.3	31	34.6	
Oct	26.5	28	29.6	
Nov	28.5	29.6	30.9	
Dec	30.3	31.7	34.1	

Should PSE extend the contract beyond 2004, which is likely, Port Townsend Paper will be moved to Schedule 91 which prices the resource according to the lesser of (a) market (Mid-C firm for on peak/off peak) or (b) Sumas gas index for applicable month x heat rate proxy of 10.2

Term: 1/1/99 - 12/31/2003 **Expiration: 12/31/2003** 

### STS Hydropower Ltd. -Hutchison Creek

Qualifying Facility (QF) status

Description: small hydro, 4 generators, 225 kw each, diversion dam, uses Nooksack River

Generating Capacity: Approx. 900 kw Licensing: FERC exemption from licensing

Location: Bellingham, WA Outages/Maintenance:

Point of Delivery: Where the project is interconnected with PSE's electrical system Scheduling: N/A; Energy supply does not schedule volumes less than 1 MW

Power Sales Agreement dated 9/20/84
Price: Winter (October-March) - \$0.045/kw

Summer (April-September) - \$0.027/kw

Penalty provision if Seller does not deliver as much energy during the second half of the Term as during the first half. Seller shall pay PSE \$0.01 for each kilowatt hour undelivered. Should PSE extend the contract beyond 2004, STS will be moved to Schedule 91 which prices the resource according to the lesser of (a) market (Mid-C firm for on peak/off peak) or (b) Sumas gas index for applicable month x heat rate proxy of 10.2

Term: 10/1/84 - 9/30/2004; 20 year contract

**Expiration: 9/30/2004** 

### Spokane Project

Qualifying Facility (QF) status; 21 year contract

Description: thermal, regional solid waste refuse combustion project

Generating Capacity: 22.9MW Location: Spokane County, WA

Outages/Maintenance: Written notice shall be provided on or before Jan 1 of each year for all

outages for next 18 months

Point of Delivery: interconnection with WWP's system

Scheduling: Hourly Preschedule submitted by PSE to BPA by 12:00pm Transmission: Wheeled from project by BPA to Kitsap Substation

PSE incurs energy losses at a rate of 1.6% of the amount of all energy delivered to PSE by BPA under the Transmission Agreement, Spokane reimburses PSE for wheeling costs.

Agreement for Firm Power Purchase dated 1/4/88- purchase of entire net electrical output less plant use

Transmission Agreement by BPA, WWP,PSE and City of Spokane dated 7/28/88 Price: \$0.0074/kwhr x escalation quotient (GDP/1987 base year) + Exhibit C (below)

### Exhibit C

-	ATIIDIL G		
		Winter (Sep-Mar)	Summer (Apr- Aug)
	2001-2008	\$96.40	\$52.80

Term: 3/1/90-2/28/2011 Expiration: 2/28/2011

### Twin Falls

Description: hydro, 2 units, run of the river (Snoqualmie)

Generating Capacity: 20MW

Licensing: FERC license issued 9/22/86 (#4885-003)

Location: South Fork Snoqualmie River, King County, WA (5 miles east of North Bend)

Outages/Maintenance: May—September, generally August and September Point of Delivery: where the project is interconnected to PSE's system

Agreement for the Purchase of Power dated 10/29/84 – for the entire net electrical output

Price: \$75.00/MW

Term: 3/8/1990-3/8/2025, 35 year contract

**Expiration: 3/8/2025** 

### Weeks Falls

Description: hydro

Generating Capacity: 4.6MW

Licensing: FERC license issued 4/24/85 (#7563)

Location: South Fork Snoqualmie River, King County, WA

Outages/Maintenance: May-September, generally August and September with notice on or

before January 1 of each year

Ex	(V	VAG-	-4)
Page 63	of 219		

Point of Delivery: Where the project is interconnected to PSE's system

Agreement for Purchase of Power dated 10/29/84 - entire net electrical output
Amendment No.1 to the Agreement for the Purchase of Power from the Weeks Falls Hydro
Electric Project dated 12/12/85 increasing capacity, updating one line and delivery voltage

Price: \$75.00/MW

Term: 12/1/87 (COD) - 12/31/2022; 35 year contract

Expiration: 12/31/2022

### **CONTRACTS TO NOTE:**

**BPA Residential Exchange** 

Description: NW Power Act establishes a Residential Exchange Program to provide benefits to residential and small farm consumers through the Residential Purchase and Sale Agreement. Pursuant to this Amended Settlement Agreement (Agreement), instead of delivering firm power to PSE, BPA will make cash payments to PSE during the period July 1, 2001- September 30, 2006. The Agreement also extends the term from 10/1/2006 thru 9/30/2011 on the same terms and conditions in the Residential Exchange Settlement Agreements and Firm Power Block Sales Agreements (monetary benefits and firm power). Unless notification is given to BPA by October 2005. BPA will use the power not sold to PSE to meet its firm load obligations in the PNW

10/1/2001-9/30/2006: Monetary Benefit

10/1/2001-9/30/2002 – Monthly Cash payment by BPA to PSE = \$14,142,786 10/1/2002-9/30/2006 – Monthly Cash payment by BPA to PSE = \$14,628,966

10/1/2006 - 9/30/2011: Firm Power and Monetary Benefits

BPA shall provide to PSE Firm Power or Monetary Benefit payments, or both. PSE must notify BPA by October 2005

Total of Firm Power and Monetary Benefit for Puget = 648 annual aMW

Amended Settlement Agreement executed by BPA and PSE date June 11, 2001

Term: 7/1/01-9/30/2011 Termination: 9/30/2011

Note condition in the Agreement for:

Conservation and Renewables Discount = Total Net Requirements Loads (700aMW) x .5mill/kwh discount rate x 8760 = \$3,066,000 annually = \$255,500/monthly for 5 year term. PSE is required to submit an annual C&R Discount report specifying the amount of expenditures claimed under the program and amount of C&R Discount received to date. First report is due 10/1/2002.

MEGA-Merchant Energy Group of the Americas, Inc.

Description: (7) LM2500 turbine units to be operated by Pierce Power LLC

Capacity: 154MW

Energy: 50% of the Available Capacity

Point of Delivery: 115kv terminals at Fredrickson site Non Winter Supply Period: 3/1/2002-9/30/2002

Scheduling: Not later than 5:30 am PPT on the Prescheduling Day Buyer may notify Seller that Buyer intends to purchase and take delivery of whatever energy is produced during that day in the amount associated with 50% of the available capacity.

Electric Capacity and Energy Confirmation Agreement dated July 31, 2001

Capacity Price -Supply Period: \$1.00/month/turbine (\$7.00)

Energy Price- Supply Period: Seller's actual costs including fuel and transportation

Variable O&M: \$0.71/MWH Term: 7/31/2001-9/30/2002 Termination: **9/30/2002** 

Electric Capacity and Energy Confirmation Agreement dated April 20, 2001

Winter Period: 12/1/2001-2/28/2002 Energy: 100% of the Available Capacity Point of Delivery: Same as above

Market Charge: Dow Jones, Mid-C Index for Firm On-Peak, Firm Off-Peak and Sunday 24 Hour

Firm for the period in which such hour occurs.

Outage Strike Price: \$/mWh (payment for outages)

Variable O&M: \$0.71/MWH

Ex	(WAG	i-4)
Page 65	of 219	,

Capacity Price-Winter Period: \$419,931.00/month /turbine for each month of the winter period.

This amount shall be reduced prorata, MW for MW, day for day, if unable to generate

normal rated output

Energy Price-Winter Period:

Seller's actual costs including fuel and transportation

Scheduling: Same as above Term: 5/2/01 – 11/30/2002 Termination: 11/30/2002

### **Black Creek Hydroelectric**

Description: Storage and Transmission. Letter Agreement between WWP and PSE dated 7/14/98 in which PSE shall store the power generated by Black Creek during the year (July-June period) and return all power to WWP during the month of August of each year. The Agreement for Power Sale is between WWP and Black Creek Hydro (HEDC, Hydroelectric Development

Corporation, an affiliate of PSE)
Capacity: 3.7MW, 1 generating unit

Storage charge: PSE bills WWP \$6.00/MWr

Scheduling: product is shaped when delivered to WWP

Term: 7/14/98-6/30/04 Termination: 6/30/2004

### Skookumchuck

Description: Thermal. Part of the Centrailia Steam Electric project, 2 year letter agreement with

PacifiCorp expired on 10/31/95

Capacity: 980 kw Location: Centralia, WA Price: \$16.00/MWhr Transmission:

Agreement for Firm Power Purchase dated

Term: 7/1/93-10/31/95 or until a long term agreement can be agreed upon

Termination: Upon notice?

# Selected Transmission Studies

Paris Comment

The second second

SI STERNAL ISS STREET ES LE

The following files represent a 2000 heavy winter case with north to south flows on the BC to Pacific Northwest intertie and north to south flows on the Pacific AC Intertie.

- HSNS4I Compressed input and output file for a 2000 heavy summer case, North to South flows
  - HSNS4O Compressed input and output file for a 2000 heavy summer case, North to South flows
- HWNS21 Compressed input and output files for a 2000 heavy winter case, North to South flows
- HWNS2O Compressed input and output files for a 2000 heavy winter case, North to South flows

The following files represent a study for generation integration at PSEI's Frederickson substation.

- FREDERICKSONI Word
  - FREDERICKSONI Excel
- FREDERICKSONII Word
- FREDERICKSONII Excel

The following file represent a study for generation integration at PSEI's Sumas substation.

SumasII - Transmission Contraints Scoping Study

The following file represent a study for transmission service from March Point Co-generation to the Mid-Columbia bus.

MPCC Point-to-Point Service Request, System Impact Study

The following PTI Must output files represent a preliminary assessment of PSEI's Whatcom/Skagit counties' transmission system for the summer 2001. This assessment is preliminary:

Summer 2001, existing generation, SINGLECM Word file

12/21/200

Construction of the last

SCHOOL STORY SICHES LINE

Summer 2001, existing generation, former loads, SINGLECM\_FCITC Word file

Summer 2001, new Fredonia 100MW, IndAdj, PTIfixes, SINGLECM Word file

Summer 2001, new Fredonia 100MW, IndAdj, PTIfixes, SINGLECM\_FCITC Word file

Summer 2001, new MPCC 50MW, new Fredonia 100MW, IndAdj, PTIfixes, SINGLECM\_FCITC Word file Summer 2001, new MPCC 50MW, new Fredonia 100MW, IndAdj, PTIfixes, SINGLECM Word file

generation integration near PSEI's Frederickson substation. The zip contains one Word document and three post-script power The following zip file represents a study conducted as part of Electricity Captial, LCC's request for transmission service and flow drawing files.

Electricity Capital Study

The following zip file contains a study conducted as part of Puget Sound Energy's merchant function's request for additional generation integration at Fredonia substation. The zip contains one Word document

Fredonia 100MW Study

Back to PSEI's Documents

# Frederickson - 270 MW

# FREDERICKSON 270 MW

Ex	<u> </u>	(WA	.G-4)
Page 6	8 of 219	)	

## SYSTEM IMPACT STUDY OASIS Reference No. 17855 270 MW GENERATION ADDITION TO FREDERICKSON 115 kV BUS

September 29, 2000 PSE Electric Transmission

#### INTRODUCTION

This study is in response to OASIS Reference No. 117855 and the System Impact Study Agreement executed by PSE's merchant function on May 17, 2000 requesting, among other things, 270 MW of Firm Point-to-Point Transmission Service for proposed new combined-cycle generation located at PSE's 115 kV Frederickson Substation located in Pierce County, Washington. This study summarizes the results of analyses done to develop reliable transmission alternatives that integrate the proposed generation at Frederickson. The generation studied includes six levels of generation: (1) 0 MW; (2) 149 MW of existing Frederickson generation; and (3) 200 MW; (4) 250 MW; (5) 270 MW; and (6) 300 MW from the proposed generators, with levels (3) – (6) all including 149 MW of existing Frederickson generation.

#### CONCLUSION

With certain transmission improvements, the proposed generation at a 270 MW level can be reliably integrated into the transmission system through a 115 kV connection at PSE's Frederickson Substation. A single 115 kV line would be constructed between the proposed generator substation bus and the Frederickson Substation bus, with substation breakers at both ends of the line.

Two alternative transmission improvement plans have been identified. The preferred plan is: (a) construct a line from Frederickson Substation to Woodland Substation (north of Frederickson); (b) convert the Fern Hill-St. Clair 55 kV line to 115 kV; (c) install substation breakers for the lines; and (d) upgrade several other lines to higher ratings.

The alternative plan is: (a) reconductor the Frederickson-St. Clair 115 kV line; (b) reconductor the 4/0 copper portions of the Electron Heights-Blumaer line; and (c) upgrade several lines to higher ratings. The preferred plan is less expensive, can avoid the need to trip generation for most transmission outages, and can support generation output under a greater number of planned and unplanned transmission outages.

For the condition of highest flow across the Raver-Paul path, generator tripping is not required for a West Side Northern Intertie (WSNI) import up to 2850 MW. With pre-existing line outage conditions, the proposed generation may need to be tripped by an electronic signal supplied by BPA for high West Side Northern Intertie imports.

An estimate of the cost for transmission interconnection facilities and transmission improvements is \$16,500,000 for the preferred plan, and \$19,300,000 for the alternative plan. The major difference between the two plans is that the preferred plan provides a second transmission circuit west to St. Clair, and north to White River and Alderton. Therefore, the system will be able to sustain transmission system outages and continue to support generation output from the proposed generators much better under the preferred plan, than with the alternative plan.

#### **STUDY ASSUMPTIONS**

Summer and winter seasons were studied with high Raver-Paul loading and high north to south flows on lines going through Pierce County. Flow conditions with high south to north flows to Canada were also checked for the summer. The summer season included heavy and light load conditions for both north to south and south to north. The winter season studies were with heavy loading. The existing two combustion turbines were included as generating 74.4 MW each in most of the simulations. The proposed 270 MW generation is in addition to the existing 149 MW from Frederickson.

The lines that cross Pierce County toward Thurston and Lewis Counties in the south are:

Raver-Paul 500 kV line White River-Cowlitz-Olympia 230 kV line Covington-Cowlitz-Chehalis 230 kV line Frederickson-St. Clair 115 kV line Electron Heights-Blumaer 115 kV line White River-Fern Hill 57.5 kV line

The time frame used for simulations was 2002 with the following improvements assumed to be completed:

Chief Joe-Monroe #4 line re-converted to 345 kV operation.

Bothell-Snoking #2 and Snoking-Maple Valley #2 230 kV lines energized.

Schultz-Raver #2 500 kV line rerouted from Raver to Echo Lake.

Bothell #2 and #3 230-115 kV transformers replaced with 300 MVA transformers.

Novelty 115 kV substation bus.

Shelton-South Bremerton 230 kV line, South Bremerton 230-115 kV transformer.

Reactive power margin and voltage stability were not determined. It is anticipated that the addition of the proposed generation with full reactive capability will improve voltage regulation in the area. This can be confirmed with reactive margin studies. Transient stability was not confirmed, and would be done when stability models, and machine specific parameters are provided.

#### **OUTAGE ASSUMPTIONS**

Outages taken included single contingency (N-1) outages and common mode outages. The single contingency outages are taken automatically, and include all lines in southern King, Pierce and Thurston Counties. The common mode outages are:

White River north 230 bus, south 230 bus, north115 bus, and south 115 bus Alderton 115 bus, Frederickson 115 bus, Woodland 115 bus Krain Corner 115 bus, Electron Heights 115 bus, Saint Clair 115 bus Blumaer 115 bus, West Olympia 115 bus, Plum Street 57.5 bus PSE Olympia north 115 bus, and south 115 bus, Tono 115 phase shifter BPA Olympia east 230 bus, west 230 bus, and 115 bus All 115 kV double circuit outages in Pierce County.

The following use governor load-flow following WSCC guidelines.

Raver-Paul 500 line; Trip BC Hydro, FDG/WHG
Raver-Paul 500 line; Trip BC Hydro, FDG/WHG, PG
Raver-Paul-Centralia G2 500 BKF; Trip BC Hydro, FDG/WHG
Raver-Paul-Centralia G2 500 BKF; Trip BC Hydro, FDG/WHG, PG
Raver-Paul-Centralia G2 500 BKF & Centralia G1: Trip BC Hydro, FDG/WHG

Raver-Paul-Centralia G2 500 BKF & Centralia G1; Trip BC Hydro, FDG/WHG, PG

Ex		_(WAG-4	.)
Page	70 of 2	19	

Paul-Allston 1&2 500 lines on common right-of-way; Trip BC Hydro

The formula for tripping BC Hydro generation is:

Trip generation = 1.3 x (West Side NI north-to-south – 1450 MW) FDG/WHG stands for tripping Fredonia and Whitehorn combustion turbines. PG stands for tripping the proposed generation. BKF stands for breaker failure.

#### **FINDINGS**

The Frederickson Substation 115 kV bus is currently interconnected to the local transmission system through three 115 kV lines. They are: Alderton - Frederickson, Electron Heights -Boeing Puyallup - Frederickson, and Frederickson - St. Clair. The usual flow on these lines is from the northeast to the southwest, corresponding to the flow pattern on the 230 and 500 kV lines across the same area. With the addition of 270 MW of generation connected at Frederickson, these three lines can become overloaded above their thermal capabilities, especially during conditions when other facilities are out-of-service. Out-of-service conditions may be those that are planned for maintenance needs, or those that are unplanned, such as due to wind or lightening.

To operate the system reliably, reliability criteria are used by WSCC member utilities that specify, among other things, single element outages, and common element outages that should be accommodated when planning transmission facilities. Operator actions and remedial action schemes (RAS) may be used to adjust the system to operate it in a reliable condition. One RAS used on this path is to automatically trip selected generators to the north, if the BPA Raver-Paul 500 kV line is lost from service during a period of high north to south flow on the Raver-Paul line. By tripping generation to the north, the flow that shifts from the 500 kV line to the underlying 230 and 115 kV line is reduced.

Two alternative transmission improvement plans were developed that will support the interconnection of the proposed generation to the Frederickson substation 115 kV bus. The preferred plan is: (a) construct a line from Frederickson Substation to Woodland Substation (north of Frederickson); (b) convert the Fern Hill-St. Clair 55 kV line to 115 kV; (c) install substation breakers for the lines; and (d) upgrade several lines to higher ratings. The alternative plan is: (a) reconductor the Frederickson-St. Clair 115 kV line to a much larger conductor; (b) reconductor the 4/0 copper portions of the Electron Heights-Blumaer line; and (c) upgrade several lines to higher ratings.

The preferred plan results in two paths from Frederickson to St. Clair, and from Frederickson to Alderton, whereas the other alternative plan results in single paths from Frederickson to St. Clair, and to Alderton. As a consequence, the preferred plan can support generation output under many planned and unplanned outages that the alternative plan cannot. The preferred plan can avoid generator RAS tripping for most transmission outages, and is less expensive. Line item details of both plans are given in the COSTS section that follows.

#### **Simulation Results**

The pre-outage flows on lines can be seen in Table 1, which shows MW flows before outages are taken for the preferred and alternative plans. Heavy and light summer cases are represented with WSNI in the north-to-south (at 2850 MW) and south-to-north (and 1500 MW) directions. In the winter cases the WSNI is 1450 MW north-to-south. Line flows on the Raver-Paul 500 kV line, as an example are about 1800 in the heavy summer north-to-south case, and 2000 MW in the light summer north-to-south case.

Ex.		(WAG-4)
Page	71	of 219

Raver-Paul 500 kV line in the winter case is goes down to about 1200 MW. When the winter import OTC rises above 1450 MW, then transmission through-flows will increase and loading on the Raver-Paul line will increase.

During the summer season the loading on lines in the Raver-Paul path is generally closer to their ratings than during other seasons. This is because the transmission through-flow is higher, and because the line ratings are often significantly lower in the summer, especially on lines having low conductor temperature ratings. The summer season then presented the worst case conditions and became the focus for developing alternative improvements.

The difference in distribution of MW loading on the transmission lines between the two plans can be seen by comparing the numbers separated by a slash "/" in Table 1. For example, in the heavy summer, north-to-south case with the proposed generation at 270 MW, the loading on the Frederickson-St. Clair 115 kV line (labeled FREDRICK – TILCM TP 115) is 135 / 184. Flow on this line under the preferred plan is 135 MW, and on the alternative plan, it is 184 MW.

The sensitivity of line loading to Raver-Paul flow levels can be determined from this table. For example, in the heavy summer north-to-south case, with the proposed generation at 270 MW, loading on the proposed Woodland-Fern Hill line is 109 MW, when loading on the Raver-Paul line is 1822 MW. In the heavy summer south-to-north case, loading on the Woodland-Fern Hill line is 49 MW, when loading on the Raver-Paul line is 723 MW. A 60% reduction of flow on the Raver-Paul line is accompanied by a 55% reduction of flow on the Woodland-Fern Hill line.

The results of outage simulations are given in Table 2, for single contingency outages (N-1), and common mode outages, except that the Raver-Paul 500 kV outage results for summer are given in Tables 3-6, and are discussed later. The outage results for other than the Raver-Paul 500 kV show that line loadings remain within their ratings up to an addition of 270 MW of generation. An exception is the double line loss of the Alderton-Frederickson and Frederickson-St. Clair 115 kV lines for the alternative plan. This outage is an N-1 outage only if one of the other two lines to Frederickson is already out for some reason. Because of the severity, a RAS should be installed to trip the proposed generation if the alternative plan is implemented and this outage occurs.

Other overloads in Table 2 are the Covington-Tacoma A 230 kV line and the White River-Tacoma B 230 kV line. These lines are actually both parts of separate three-comer lines. They are the Covington-Cowlitz-Chehalis (Tacoma A) and the White River-Cowlitz-Olympia (Tacoma B) 230 kV lines. These overloads would only occur in the event that either of the line breakers at Cowlitz Substation were to open without its entire three-corner line tripping. By installing relays to open the appropriate Covington or White River breaker or the appropriate Olympia or Chehalis 230 kV breaker when its Cowlitz breaker opens, these overloads would not occur. As indicated in the table, these overloads are insensitive to the existing Frederickson and proposed generation levels.

#### Raver-Paul 500 kV Outage

The most severe outage is the Raver-Paul 500 kV outage, and combination outages, in which the Raver-Paul 500 kV line is included. The combination outages studied are a breaker failure at Paul that trips both the Raver-Paul line and the Centralia #1 generator, and the same breaker failure when the Centralia #2 generator is also out-of-service. Results are given in Tables 3-6, and include heavy and light summer load with the preferred plan (Tables 3 & 4), and heavy and light summer load with the alternative plan

Ex.			(W	AG-4)
Page	72 o	f 21	9	

(Tables 5 & 6). The tables show when lines overload both without, and with tripping the proposed generators.

BPA arms a generator tripping RAS when there are high north to south flows on the Raver-Paul 500 kV line. The RAS sends trip signals to selected generators north of this line when the RAS detects that the line is lost from service. The generators that are armed are determined according to the flow level on the Raver-Paul line, and other factors, as described in BPA Dispatcher Standing Order (DSO) 307. In the power system simulations, for high flow levels on the Raver-Paul line, the generators that were tripped included Whitehorn, Fredonia, 1024 MW at Chief Joseph, and units in Canada following the formula:

#### MWtoTrip = 1.3(IngledowCusterflow - 1450MW)

The results indicate that for heavy or light summer loads, with the existing Frederickson CT's on, and with the proposed generators at 270 MW, the preferred plan will support a WSNI level that is 100 to 140 MW higher than the alternative plan. For the Raver-Paul single line outage, and Raver-Paul and Centralia Unit 2 breaker failure outage, tripping the proposed generators is not required with the preferred plan, and is probably not required with the alternative plan.

When the Centralia Unit 1 is out-of-service, the Raver-Paul pre-outage flow modeled is above 2000 MW. In practice, BPA would reduce the flow on the Raver-Paul 500 kV line, following DSO 307 for Level 4, so that the overloads would not happen if the outage were to occur. But running the outage at this high level illustrates the need for a Raver-Paul flow threshold that results in significant overloads if violated. From Table 3, with Centralia Unit 1 down, and following the breaker failure outage, loading on the Tacoma A-Centralia 230 kV line is at 104.8% of its rating when Frederickson CT's are on, but with the proposed generation at zero. When the proposed generators are at 270 MW, for the outage, loading on the Tacoma A-Centralia 230 kV line is at 107.5% of its rating. By tripping the full 270 MW, loading on this line reduces to 105.3%. In practice, when the Centralia Unit 1 is out-of-service, the flow level on the Raver-Paul would be reduced before any outages.

The percents of overload for the light summer cases are higher than the heavy summer cases. However, the increase is only 3 to 4%. During light load conditions, ambient temperatures are lower, and line ratings increase. For the lines that overload, a reduction in ambient air temperature from 35C to 20C results in a 10% increase in rating. During winter conditions the line loading on the Raver-Paul is relatively much lower.

The White River-Fem Hill 57.5 kV line overloads for the alternative plan with outages of the Raver-Paul line. A relay is installed at White River to detect when the line is being overloaded and the relay will sent a signal to automatically trip the line breaker at White River. All the power system simulations on the alternative plan were done with either the White River-Fem Hill line open, or with the relay modeled to open the line up if the flow level on the line is above its seasonal rating.

#### <u>Winter</u>

Some common mode outages do not achieve a solution for winter loading conditions. The Olympia 230 kV bus is divided between east and west segments with both 230-115 kV transformers on one bus segment, the east bus. Loss of the Olympia 230 east bus results in no solution. Loss of the Olympia 230 west bus results in depressed voltages and severe overloads. The depressed voltages may be remedied by inserting capacitors

that are not in the case. The combination outage of the breaker failure loss of the Paul-Raver line and Centralia unit #2, when Centralia unit #1 is out-of-service fails to solve in the winter case. The voltage collapse is too severe to get a power flow solution. The conclusion is that during winter heavy loads, Centralia unit #1 must be running.

#### **COSTS**

Transmission costs for improvements to connect the proposed 270 MW of generation at Frederickson for the preferred and alternative plans include the following. This does not include the cost of 115 kV breakers at the proposed generator bus, or generator step-up transformers.

Preferred Plan	(\$	x1000)
Cut over Fern Hill-St. Clair 55 kV line to 115 kV		,
Woodland-Fern Hill, rebuild 55 line to 115 with Bittern	2,200	
Fern Hill-South Gate Tap, uprate Bittern to 100C	20	
South Gate Tap-Gravelly Lake Drive, reconductor 2 miles to	20	
Bittem, and uprate existing Tern to 100C	700	
Gravelly Lake Drive-Holden Tap, reconductor 2.5 miles to Bitten	n 900	
Holden Tap-Dupont-St. Clair, uprate Bittern and Tern to 100C	70	
Woodland Substation, construct 115 kV bus with 3 breakers	1.600	
St. Clair Substation, install a 115 kV breaker	400	
Gravelly Lake Substation, install two 115 kV breakers	700	
Fern Hill & South Gate, construct distribution facilities	1,000	
	1,000	7,590
Construct Woodland-Frederickson 115 kV line		7,000
Construct 0.5 and 1 mile sections of double circuit Bittern	700	
Reconductor 2 miles of Tem to Bittem	260	
Construct 4.7 miles of Bittern	1410	
Breakers at Woodland and Frederickson	800	
Additional right-of-way costs	150	
	.00	3,320
Frederickson-Proposed Generator 115 kV bus		0,020
Frederickson-Proposed Gen., construct 115 kV Lapwing ¼ mile	90	
Frederickson Substation, install 115 kV breaker	450	
		540
Up-Rate several 115 kV lines to higher conductor temperature		
Electron Heights-Boeing Puyallup-Frederickson, 17 miles to 100	C 340	
Frederickson-Hemlock-Alderton, 12 miles Term to 150C	360	
White River-Gardella-Alderton, 7.4 miles, Tern to 100C	150	
White River-Sumner-Pioneer, 4.7 miles, Tern to 100C	100	
Alderton-Stewart, reconductor 0.5 mile 4/0 to Bittern	120	
St. Clair-Johnson Hill, 5.7 miles, Tern to 100C	120	
St. Clair-Patterson, 2.7 miles, Tern to 100C	60	
		1250
Total for preferred plan	\$ 1	2,700.
Total for preferred plan with 30% contingency buffer	-	6,500.
	_ •	-,

Ex. \_\_\_\_(WAG-4) Page 74 of 219

Alternative Plan	(\$	x1000)
Frederickson-St. Clair 115 kV line Reconductor 29.7 miles to Lapwing (may require switch replace Electron Heights-Blumaer 115 kV line Reconductor 4/0 copper is 23.5 miles to Tem Up-rate Merlin conductor, 15.9 miles, to 125C  Frederickson-Proposed Generation 115 kV bus Frederickson-Proposed Gen., construct 115 kV Lapwing ¼ miles Frederickson Substation, install 115 kV breaker  Up-Rate several 115 kV lines to higher conductor temperature Electron Heights-Boeing Puyallup-Frederickson, 17 miles to 106 Frederickson-Hemlock-Alderton, 12 miles Tem to 150C Alderton-Stewart, reconductor 0.5 mile 4/0 to Bittern	ment)	7,430
Reconductor 4/0 copper is 23.5 miles to Tem	5860	
Up-rate Merlin conductor, 15.9 miles, to 125C	320	6,180
Frederickson-Proposed Generation 115 kV bus		
Frederickson-Proposed Gen., construct 115 kV Lapwing ¼ mile	90 450	
1 1000 House of Cabouatory House 110 KV Diocitor	430	540
Up-Rate several 115 kV lines to higher conductor temperature Electron Heights-Boeing Puyallup-Frederickson, 17 miles to 100	C 340	
Frederickson-Hemlock-Alderton, 12 miles Tern to 150C	360	
Alderton-Stewart, reconductor 0.5 mile 4/0 to Bittern	120	820
Total for second alternative	\$ 1	4,970.
Total for second alternative with 30% contingency buffer		9,460.

Table 1. Line flows on both Plans with Incremental levels of Proposed Generation

Page 1/2 Proposed Generation MW Level & Frederickson CT MW Level												
Seasonal case	0 & 0	0 & 149	200 & 149	250 & 149	270 & 149	300 & 149						
ELEMENT OR PATH	Lin	e loading in N	/w ( Preferred	Plan Cc / Al	ternative Plar	n Ec)						
2002 Heavy Summer, West S	ide NI North	to South										
West Side NI, Ingledow-Custer 1&2	2851 / 2850	2851 / 2850	2852 / 2851	2851 / 2851	2851 / 2850	2851 / 2851						
RAVER - PAUL 500	1787 / 1807	1800 / 1816	1816 / 1829	1820 / 1833	1822 / 1834	1825 / 1836						
OLYMPIA - TACOMA B 230	308 / 317	312 / 319	316 / 322	317 / 323	318 / 324	319 / 324						
TACOMA A - CENTR SS 230	292 / 296	297 / 300	303 / 306	305 / 307	306 / 308	307 / 309						
FREDRICK - BOE_PUY 115	3/ -1	27 / 34	60 / 82	68 / 94	71 / 99	76 / 106						
FREDRICK - SW28TIE 115	-39 / -81	1/-8	56 / 93	70 / 118	75 / 128	83 / 143						
FREDRICK - TILCM TP 115	64 / 77	90 / 116	124 / 167	132 / 179	135 / 184	140 / 192						
FREDRICK - WOODLND 115	-34	24	102	122	130	141						
WOODLND-FERNHILL 115	79	90	105	108	109	111						
WOODLND-PIONEER 115	<b>-9</b> 6	-61	-13	-1	4	11						
WOODLND-FRUITLAND 115	-23	-12	4	8	9	11						
2002 Light Summer. West Sid	e Ni North to	South										
West Side NI, Ingledow-Custer 1&2	2851 / 2850	2851 / 2851	2851 / 2851	2851 / 2850	2851 / 2851	2850 / 2850						
RAVER - PAUL 500	1997 / 2019	2008 / 2026	2017 / 2034	2021 / 2035	2022 / 2036	2024 / 2038						
OLYMPIA - TACOMA B 230	334 / 344	338 / 346	343 / 350	345 / 351	345 / 351	346 / 352						
TACOMA A - CENTR SS 230	310 / 314	315 / 318	322 / 324	323 / 326	324 / 327	325 / 327						
FREDRICK - BOE_PUY 115	0/-4	24 / 32	57 / 79	65 / 91	68 / 96	73 / 103						
FREDRICK - SW28TIE 115	-42 / -87	-1 / -13	54 / 88	67 / 113	73 / 123	81 / 139						
FREDRICK - TILCM TP 115	73 / 88	99 / 126	132 / 177	140 / 189	143 / 194	148 / 201						
FREDRICK - WOODLND 115	-34	23	102	121	129	141						
WOODLND-FERNHILL 115	88	99	113	116	118	120						
WOODLND-PIONEER 115	<b>-93</b>	-58	-9	3	8	15						
WOODLND-FRUITLAND 115	-34	-22	-7	-3	-1	1						
Dec. 2002 Heavy Winter, Wes	t Side NI Nor	th to South										
West Side NI, Ingledow-Custer 1&2	1450 / 1450	1451 / 1450	1450 / 1450	1451 / 1451	1451 / 1450	1451 / 1451						
RAVER - PAUL 500	1148 / 1161	1159 / 1170	1173 / 1180	1177 / 1183	1179 / 1184	1181 / 1186						
OLYMPIA - TACOMA B 230	185 / 191	189 / 193	193 / 196	194 / 197	195 / 197	195 / 198						
TACOMA A - CENTR SS 230	77 / 79	82 / 84	89 / 90	90 / 92	91 / 92	92 / 93						
FREDRICK - BOE_PUY 115	10/5	37 / 44	69 / 91	77 / 103	80 / 108	85 / 115						
FREDRICK - SW28TIE 115	-29 / -66	15/ 16	70/ 117	84 / 143	89 / 153	97 / 168						
FREDRICK - TILCM TP 115	45 / 50	72/ 92	105 / 142	114 / 155	117 / 160	122 / 167						
FREDRICK - WOODLND 115	-37	27	106	126	134	145						
WOODLND-FERNHILL 115	53	65	79	83	84	86						
WOODLND-PIONEER 115	-105	-66	-17	-5	0	7						
WOODLND-FRUITLAND 115	-1	12	28	31	33	35						

Table 1. Line flows on both Plans with Incremental levels of Proposed Generation

Page 2 / 2	0	anad Ganara	tion MW I eve	al & Fractarick	son CT MW I	evel
rayo e / e	Prop					
Seasonal case	0 & 0	0 & 149	200 & 149	250 & 149	270 & 149	300 & 149
		. looding in 14	hu / Droformad	Pion Co / AH	ernative Plan	Ec)
ELEMENT OR PATH			M ( Preferred	Plati GC/All	ellialive r iai	
2002 Heavy Summer, West Si	de NI South I	o North				
West Side NI, Custer-Ingledow 1&2	1506 / 1506	1500 / 1500	1501 / 1501	1501 / 1501	1502 / 1501	1501 / 1501
RAVER - PAUL 500	704 / 705	705 / 706	719 / 716	722/ 718	723 / 719	726 / 721
OLYMPIA - TACOMA B 230	89 / 90	<b>89 / 90</b>	93 / 92	94 / 93	95 / 93	95 / 93
TACOMA A - CENTR SS 230	86 / 86	86 / 86	92 / 92	94 / 93	94 / 93	95 / 94
FREDRICK - BOE_PUY 115	27 / 36	27 / 36	59 / 84	67 / 96	71 / 101	75 / 108
FREDRICK - SW28TIE 115	30 / 52	30 / 52	85 / 153	99 / 178	104 / 188	112/ 203
FREDRICK - TILCM TP 115	39 / 54	39 / 54	72 / 105	80 / 118	83 / 123	88 / 130
FREDRICK - WOODLND 115	47	47	125	145	153	165
WOODLND-FERNHILL 115	30	30	44	47	49	51
WOODLND-PIONEER 115	-9	-9	40	52	57	64
WOODLND-FRUITLAND 115	19	19	35	39	40	43
2002 Light Summer, West Side	e NI South to	North				
West Side NI, Custer-Ingledow 1&2	1501 / 1501	1501 / 1501	1501 / 1501	1502 / 1501	1501 / 1501	1501 / 1501
RAVER - PAUL 500	686 / 690	676 / 677	690 / 687	693 / 690	695 / 691	697 / 693
OLYMPIA - TACOMA B 230	87 / 89	87 / 88	91 / 90	92 / 91	92 / 91	93 / 91
TACOMA A - CENTR SS 230	94 / 95	95 / 95	101 / 101	103 / 102	103 / 103	104 / 103
FREDRICK - BOE_PUY 115	-1/ -2	23 / 33	55 / 80	63 / 92	66 / 97	71 / 104
FREDRICK - SW28TIE 115	-9 / -20	32 / 56	87 / 157	101 / 183	106 / 193	114/ 208
FREDRICK - TILCM TP 115	16/ 19	39 / 56	72 / 106	80/ 118	84 / 123	89 / 131
FREDRICK - WOODLND 115	-9	50	129	149	157	168
WOODLND-FERNHILL 115	20	30	43	47	48	50
WOODLND-PIONEER 115	-34	3	52	64	69	76
WOODLND-FRUITLAND 115	1	13	29	33	35	37

#### Table 2. Outages with Incremental levels of Proposed Generation and Frederickson Generation

Propose	d Generation	MW Level	& Frederickson	CT MW Level
---------	--------------	----------	----------------	-------------

Outage

0 & 0

0 & 149

200 & 149 250 & 149 270 & 149

300 & 149

Element at % of rating

Facility loading in % of rating

#### Preferred Plan (Convert Fern Hill-St. Clair 55 kV line)

BUS WHITE RIVER SOUTH 230, 2002 Light Summer, North-to-South

**COWLITZ - TACOMA B 230** 

111.6/2100 112.1/2070 113.3/2000 113.6/1980

113.7 / 1980 113.8 / 1970

WHITE RV - TACOMA B 230, 2002 Light Summer, North-to-South

COWLITZ - TACOMA B 230

111.6/2090 112.3/2060 113.7/1970 114.0/1960

114.1/1950 114.2/1940

COVINGTN - TACOMA A 230, 2002 Light Summer, North-to-South

COWLITZ - TACOMA A 230

107.5 / 2360

109.2 / 2250 111.7 / 2100 112.3 / 2060

112.6 / 2050 112.9 / 2030

#### Alternative Plan (Reconductor Frederickson-St. Clair 115 kV line)

2 LINE FREDRICK-SW28TI	E & FREDRICK	<b>(-TILCM TP 1</b>	15, 2002 Ligi	nt Summer. N	orth-to-Souti	1
BLUMAER - OLY VAIL 115			96.8	107.9	112.3	119.1
ELECTHTS - FRED TAP 115			160.1	185.2	195.4	210.9
ELECTHTS - ORTING 115			143.8	173.3	185.3	203.6
WHITE RV - BONNEYLK 115			95.7	119.9	129.8	144.8
FRED TAP - BOE_PUY 115			121.4	140.5	148.2	159.9
FREDRICK - BOE_PUY 115			126	145.1	152.9	164.7
WR-KCTAP - BONNEYLK 115			100.8	125	134.9	150
WR-KCTAP - RHODESLK 115			126.6	155.6	167.4	185.3
ELECTHTS - WILKNSON57.5			101.4	117.7	124.4	134.5
KAPOWSIN - YELM 115			111.5	122.7	127.2	134
LONGMR T - OLY VAIL 115			97.8	108.7	113.1	119.9
LONGMRT-YELM 115			104.4	115.5	120	126.8
ORTING - RHODESLK 115 1			135.7	164.6	176.4	194.3
<b>BUS WHITE RIVER SOUTH</b>	1 230. 2002 Lig	ht Summer. N	orth-to-South	L		
COWLITZ - TACOMA B 230	114.7 / 1930	114.9 / 1920	115.6 / 1880	116.0 / 1870	116.0 / 1860	116.1 / 1860
WHITE RV - TACOMA B 230	0. 2002 Light S	ummer. North	1-to-South			
COWLITZ - TACOMA B 230	116.0 / 1850	116.2 / 1840	117.0 / 1800	117.4 / 1780	117.5 / 1780	117.5 / 1780
COVINGTN - TACOMA A 23	30. 2002 Light \$	Summer. Nort	h-to-South			
COWLITZ - TACOMA A 230	109.5 / 2240	111.0 / 2150	113.2 / 2020	113.8 / 1980	114.0 / 1970	114.4 / 1950

						S										
Table	3. Ravei	-Paul	500	kV A	elate	d Ou	ntag	es - 2	2002	Hea	vy Sı	ımme	er			
	Preferr	ed Pla	an (C	onve	rt Fe	m Hi	II-St	. Cla	ir 55	kV li	ne)					
	% line	e loadi	na at 2	2850 N	AW No	orther	n Inte	ertie /	Ni at	100%	loadir	na :	Trip	큠	킁.	를 를
Page 1 / 2												.9				
	LONGMR T	KAPOWSIN	GRAVELLY	DUPONT -	DUPONT -	FREDRICK	ST CLAIR -	ELECTHTS	BLUMAER	TACOMA A	OLYMPIA -	CHEHALIS	Proposed Generation	Coulee gen 720 MW		BC Hydro gens 1820 MW Whitehorn & Fredonia 34
Proposed  Generation Level	LONGMR T - OLY VAIL 115 LONGMR T - YELM 115	KAPOWSIN - YELM 115	GRAVELLY - TILOM TP 116	DUPONT - QUARRY 115	DUPONT - GRAVELLY 115	FREDRICK - TILCM TP 115	ST CLAIR - QUARRY 115	ELECTHTS - KAPOWSIN 115	BLUMAER - OLY VAIL 115	TACOMA A - CENTR SS 230	OLYMPIA - TACOMA B 230	CHEHALIS - CENTR SS 230	eration	WW	gens 1100 MW	ns 1820 MW Fredonia 349 MW
Outage	5 15	Ċ	116	5	115	115	5	SIN 115	15	S 230	3 230	S 230			₹	¥ N
Existing Frederickson	(149 MW)	CT's c	off: Rav	ver-Pa	aul 50	0 kV li	ne =	1787	MW	pre-ou	tage					
BKF Raver-Paul & Ctr2											•				*	* *
BKF Raver-Paul & Ctr2				-						103.3	101.5	99.5			*	* *
and Centralia 1 off line		· · · · · · · · · · · · · · · · · · ·				<u> </u>					2830	2870	]			
With Proposed Gener	ation 0 MW	/: Rave	er-Pau	500	kV line	9 = 18	100 N	W pr	e-outs	<u>ige</u>		×.	,			
BKF Raver-Paul & Ctr2															*	* *
BKF Raver-Paul & Ctr2									2+	104.8	102.3	101.0			*	* *
and Centralia 1 off line	<u> </u>									2620	2820	2800				
With Proposed Gener	ation 200 N	W: Ra	ver-P	<u>aul 50</u>	O KV	ine =	1816	MW	pre-o	utage	٠, .		1			
BKF Raver-Paul & Ctr2			, .					1.		97.0					* ; ·	* *
BKF Raver-Paul & Ctr2	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			.:						95.3			*		*	* *
BKF Raver-Paul & Ctr2	100.3 98.1	95.6						99.1	96.6	106.8	103.8	103.0			•	
and Centralia 1 off line	2840 2910							2880		2530	2800	2710			- 1	
BKF Raver-Paul & Ctr2			-							105.1	102.7	,101.3	*		<b>*</b> 1	* *
and Centralia 1 off line										2590	2820	2780		-		

.

											_					
Table :					kV R <u>onve</u>			_					mme	r		
		`	4-					• • •								
	•	% line	loadir	no at 2	2850 N	JW N	orthen	n Inte	rtie / N	li at 1	00% I	oadin	a	<b>ゴ</b> 큐	금 중	킇.
Page 2/2		o mic	,occui	.g c									9			
	5	Ş	₹	Q <del>p</del>	2	2	H	ST	ᄄ	BLU	AT X	5	윺	Proposed Generation	Chief Joseph gens 1100 MW Coulee gen 720 MW	Whitehorn & Fredonia 349 MW
	ONGMR T - YELM 115	ONGMR T - OLY VAIL 115	KAPOWSIN - YELM 115	BRAVELLY - TILCM TP 118	DUPONT - QUARRY 116	DUPONT - GRAVELLY 115	FREDRICK - TILCM TP 115	ST CLAIR - QUARRY 115	ELECTHTS - KAPOWSIN 11	BLUMAER - OLY VAIL 115	TACOMA A - CENTR SS 230	OLYMPIA - TACOMA B 230	CHEHALIS - CENTR SS 230	8. q		9
	R	H T	S	¥	7-0	Г-0	Š	A-(	- S.	55	۶	A -	Ŗ		7 <b>5</b> 8	Ĭ.
Proposed	¥	ဉ	¥	큳	Ę	₽	딑	Ā	₹	던	E C	δ	CE	ratio	≨ §	g
Generation Level	ξ	` €	Ξ	. ₹	Ä	Ē	Σ.	ARY	ğ	≨	Ä	MA	H		8	<u>ω</u>
	ភ		5	7	15	Y ==	- 70	= =	NSN.	Ξ	SS	B N	SS		¥	N O
Outage		하		਼ <b>ਨ</b>		Ö	5		15	Oi .	23	8	8			\$
With Proposed Gener	ation 2	250 M	W: Ra	ver-F	aul 50	00 KV	line =	1820	MW	ore-ou	tage	4			,	
BKF Raver-Paul & Ctr2											97.5				. •	*
								•	1	-	3030					
BKF Raver-Paul & Ctr2			- 1	-							95.4	·		*	*	*
BKF Raver-Paul & Ctr2	103.2	101.2	98.1	95.7			98.0		101.7	99.7	107.3	104.1	103.5			* *
and Centralia 1 off line	2760	2820	2920				2960		2790	2860	2500	2800	2680			
BKF Raver-Paul & Ctr2				-							105.2	102.8	101.4	*	*	*
and Centralla 1 off line											2580	2810	2780			
With Proposed Gener	ation 2	270 M	W: R	ver-F	aul 5	00 kV	line =	1822	MW	ore-ou	tage			ı		
BKF Raver-Paul & Ctr2											97.7	N		٠.	*	*
											3020					
BKF Raver-Paul & Ctr2											95.5			*	*	*
		· .														
BKF Raver-Paul & Ctr2	104.4	102.4	99.1	97.3		95.5	99.6			101.0	107.5	104.3	103.7		.*	*
and Centralia 1 off line	2720	2780	2880	2990			2870	<u> </u>	2760	2820	2490	2790	2670			
BKF Raver-Paul & Ctr2												102.8		*	*	*
and Centralia 1 off line With Proposed Gener	<u> </u>	200.14	W. Ó.	war E	Poul S	00 61/	lino -	1925	MAZ.	~~~~~		2810	2770	l.		
	allon .	300 M	VV. IN	1461-	aul S	OU NY	mie =	1020	IAIAA	<u> </u>				1		
BKF Raver-Paul & Ctr2											98.0				*	*
DKE Davies Bank & ChO			<u></u>			· · · · · · · · · · · · · · · · · · ·		<i>y</i>	7.		95.5	· · · · · · · · · · · · · · · · · · ·				
BKF Raver-Paul & Ctr2							چو ه:				₩.5	•		*		*
BKF Raver-Paul & Ctr2	106 1	104.3	100.6	99 A	96.4	97.9	102.1	95.4	104.1	102.8	107.8	104.4	104.0			
and Centralia 1 off line	1	2730		2860	,	2960	2740					2790				. #
BKF Raver-Paul & Ctr2	1				14.5							102.9		_		
and Centralia 1 off line												2810		*.	•	. 4

Table									. Clai							
Page 1 / 2	9	6 line	loadin	g at 2	2850 N	/W No	orther	n Inte	ertie / N	VI at 1	00%	loadin	)g		ς 2 3 3 3 4 5 3	Trip Wi
Proposed  Generation Level  Outage	LONGMR T - YELM 115	LONGMR T - OLY VAIL 115	KAPOWSIN - YELM 115	GRAVELLY - TILCM TP 115	DUPONT - QUARRY 115	DUPONT - GRAVELLY 115	FREDRICK - TILCM TP 115	ELECTHTS - KAPOWSIN 115	BLUMAER - OLY VAIL 115	TACOMA A - CENTR SS 230	OLYMPIA - TACOMA B 230	COWLITZ - TACOMA B 230	CHEHALIS - CENTR SS 230	Proposed Generation	Chief Joseph gens 1100 MW Coulee gen 720 MW	Whitehorn & Fredonia 349 MW
Existing Frederickson	(149	vw) (	Ts o		ver-Pa	aul 50	0 KV I		1997		re-ou	rtage				
BKF Raver-Paul & Ctr2										95.7		104.4 2640			*	* 1
BKF Raver-Paul & Ctr2 and Centralia 1 off line										101.3 2780	95.7	115.3 2100			*	* 1
With Proposed Gener	ration (	MW:	Rave	r-Pau	ıl 500	kV lin	e = 20	008 N	(W pre		ge					
BKF Raver-Paul & Ctr2										97.2 3010		102.7 2720			*	
BKF Raver-Paul & Ctr2 and Centralia 1 off line										102.7 2700	96.8	113.6 2180			*	* 1
With Proposed Gener	ration 2	00 M	W: R٤	ver-F	aul 50	00 kV	line =	2017	MW	ore-ou	rtage					
BKF Raver-Paul & Ctr2										99.1 2900	1	101.4 2780	96.5		*	*
BKF Raver-Paul & Ctr2										97.5 3000		103.4 2690		*	 *	*
BKF Raver-Paul & Ctr2	101.8		~					95.4	102.5	104.7			102.1		*	*
and Centralia 1 off line BKF Raver-Paul & Ctr2	2740	2640		-					2700	103.0	2980 97.1		2730	*	*	*
and Centralia 1 off line										2680	3050	2150	2830			

No. of Contract of

Table	e 4.	Rave	r-Pa	ul 50	0 kV	Rela	ited (	Outag	jes -	2002	2 Lia	ht Su	ımme	r			
		eferr												•			
		% line	ned a	ina et	2850	MAN N	Jortha	m int	ortio /	NI et	1000/	loadii	2	=	-	=	<b>=</b> =
Page 2/2		/O III IV	load	HIY CL	2000	IATAA I	VOI U IC	311 11 11 11 11 11 11 11 11 11 11 11 11	ei ue /	IVI AL	100%	) IOAUII	ng	į		T P C	Trip o
	LONGMR T - YELM 115	LONGMR T -	KAPOWSIN - YELM 115	GRAVELLY - TILCM TP 115	DUPONT - QUARRY 115	DUPONT - GRAVELLY 115	FREDRICK - TILCM TP 118	ELECTHTS - KAPOWSIN 115	BLUMAER - OLY VAIL 115	TACOMA A - CENTR SS	OLYMPIA - TACOMA B	COWLITZ - TACOMA B 230	CHEHALIS - CENTR SS 230	Proposed Generation	Coulee gen 720 MW	Chief Joseph gens 1100 MW	Whitehom & Fredonia 34
Proposed	- <del>-</del> - ≺	-	Z - Y	-	Ę	9	. ∃		ò	2-0	. <del>,</del>	4	ċ	nera	20	gen.	F 26
Generation Level	Ē	OLY VAIL 115	Ê	2	Ā	AVE.	- ₫	- ₹	Ž	Ä	် နို	8	9	5	₹	8 1	200
	=======================================	<b>≥</b>	- 1	7	¥ ==	Ę	Į,	) WG	≱	TR.	) B	· \$	Ti O	. N 		8	348
Outage		3	<b>.</b>	= = =	Ö	115	=======================================	Ž	15	S 230	23	8	S S			₹	ns 1820 MW Fredonia 349 MW
May December 0				<del></del> -									0				
With Proposed Gene			MW: H	aver-	Paul 5	00 kV	line :	= 2021	MW	pre-o	utage	•	· .	7		21	
BKF Raver-Paul & Ctr2	96.7								96.9	99.6		101.1	97.0			*	* *
845 8		2970					· · · · · · · · · · · · · · · · · · ·			2870	· · · · · · · · · · · · · · · · · · ·	2800	3020				
BKF Raver-Paul & Ctr2						•				97.6		103.5		*		*	* *
PKE Davis David & Ove	1015									2990		2680					
BKF Raver-Paul & Ctr2	1	106.6	95.8					97.9		105.2		111.9	102.6			*	* *
and Centralia 1 off line	2550	2450				· · · · · · · · · · · · · · · · · · ·	<del> </del>	3010	2510				2700	1			
BKF Raver-Paul & Ctr2										103.1	97.2			*		*	* *
and Centralia 1 off line		070 1				00.14				2670	3040		2820	]			
With Proposed Gene			IVV: H	aver-	<u> 28UI 5</u>	<u>00 kv</u>	line =	2022			rtage			1			
BKF Raver-Paul & Ctr2		99.2								99.8		101.0	97.2			*	* *
	2990	2900			····				2960	2860		2800	3010				
BKF Raver-Paul & Ctr2										97.6		103.5		*		*	* *
DICE Day of Day of Day									- '	2990		2680					
BKF Raver-Paul & Ctr2		107.9	96.8				96	98.9	106.8	105.4			102.8			*	* *
and Centralia 1 off line	2480	2380					·	2930	2440	2540	2950		2690				
BKF Raver-Paul & Ctr2				٠								114.5		*		*	* *
and Centralia 1 off line With Proposed Gener	Tation '	200 14	M. D.		oud F	00 141	liaa	. 2004	AMA/			2140	2820				
With Proposed Gener			yy. F18	aver-h	aul 5	vv KV	:Ine =	ZU24	MW								
BKF Raver-Paul & Ctr2	i	101.0	. %									100.8				*	* *
DVE Daves David & OLG	2880	2790		· · · · ·	· ·	<del></del>					2840	2810					
BKF Raver-Paul & Ctr2										97.7		103.6	95	*		*	* *
BVE Dayer Day 4 Av 4	405 5	400 =			,					2980		2670					
BKF Raver-Paul & Ctr2	1	109.7		97.1	95.0	95.9		100.4					103.1			*	* *
and Centralia 1 off line	2370	2270	2980	3150	-	-	3010	2820	2330	2520	2940	2290	2670				
BKF Raver-Paul & Ctr2							•					114.6		*		*	* *
and Centralia 1 off line										2670	3030	2140	2820				

-

#### Table 5. Raver-Paul 500 kV Related Outages - 2002 Heavy Summer Alternative Plan (Reconductor Frederickson-St. Clair 115 kV line)

	9	6 line	loadir	ng at 2	2850 N	W N	orthen	n Inte	rtie / N	vi at	100%	loadir	ng	T np	급	귞	幸	킇
Page 1 / 2  Proposed  Generation Level  Outage	LONGMR T - YELM 115	LONGMR T - OLY VAIL 115	KAPOWSIN - YELM 115	GRAVELLY - TILCM TP 115	DUPONT - QUARRY 115	DUPONT - GRAVELLY 115	FREDRICK - TILCM TP 115	ST CLAIR - QUARRY 115	ELECTHTS - KAPOWSIN 115	BLUMAER - OLY VAIL 115	TACOMA A - CENTR SS 230	OLYMPIA - TACOMA B 230	CHEHALIS - CENTR SS 230	Proposed Generation		Chief Joseph	Whitehom & Fro	BC Hydro gens 1820 MW
Existing Frederickson	(149	v(W)	CT's o	ff: Ra	ver-Pa	aul 50	0 kV li	ne =	•	MW p	re-ou	tage						
BKF Raver-Paul & Ctr2											96.9					*	*	*
BKF Raver-Paul & Ctr2											107.1	106.8	103.4	1		*	*	*
and Centralia 1 off line	<u> </u>	· ·									2520	2760	2700	]				
With Proposed Gener	ration 0	MW	Rave	r-Pau	1 500	kV line	e = 18	16 M	W pre	-outa	<u>ge</u>			<del>-</del> 				
BKF Raver-Paul & Ctr2											98.1			]		*	*	*
				·.							2980							
BKF Raver-Paul & Ctr2											108.4	107.4	104.6			*	*	*
and Centralia 1 off line											2470	2760	2640	]				Ì
With Proposed Gener	ation 2	00 M	W: Ra	ver-P	aul 50	00 KV	line =	1829	MW c	re-ou	<u>rtage</u>		- 1			. :		
BKF Raver-Paul & Ctr2											99.9		96.1			*	*	*
					+ 1						2860							
BKF Raver-Paul & Ctr2											98.5					*	*	*
					· .						2960			]				:
BKF Raver-Paul & Ctr2										1.00	110.1	108.3	106.4			*	*	*
and Centralia 1 off line											2400	2740	2560	1			-	
BKF Raver-Paul & Ctr2											108.7	107.7	104.9	*		· <b>*</b>	*	*
and Centralia 1 off line											2440	2750	2620	/··				

<u>Alte</u>	mativ	e Pla	ın (Ro	<u>econ</u>	<u>duct</u>	or Fr	<u>ederi</u>	<u>CKSO</u>	n-St.	<u>Clai</u>	<u>r 115</u>	<u> </u>	<u>ine)</u>		•	
	9	6 line	loadin	a at 2	2850 N	W N	orthen	n Inte	tie / N	ll at 1	00%	loadin	g	큠	급 등	[ 등
Page 2 / 2				•												
	LONGMR T - YELM 115	LONGMR T - OLY VAIL 115	KAPOWSIN - YELM 115	GRAVELLY - TILCM TP 115	DUPONT - QUARRY 115	DUPONT - GRAVELLY 115	FREDRICK - TILOM TP 115	ST CLAIR - QUARRY 115	ELECTHTS - KAPOWSIN 115	BLUMAER - OLY VAIL 115	TACOMA A - CENTR SS 230	OLYMPIA - TACOMA B 230	CHEHALIS - CENTR SS 230	Proposed Generation	Coulee gen 720 MW	Whitehorn & Fredonia 349 MW
Proposed Generation Level	YELM 11	OLY VAIL	- YELM 11	TILCM TE	UARRY 11	RAVELLY	TILCM TP	UARRY 1	KAPOWS	OLY VAIL	CENTR S	ACOMA B	CENTR S	ation	WW Too M	donia 349
Outage	g	115	Ch .	115	5	115	= = = = = = = = = = = = = = = = = = = =	5	Ž	115	S 230	230	\$ 230		\$	<b>E S</b>
With Proposed Gener	ration S	DEO M	W· Ra	var-P	oul Si	n kV	line –	1833		re-ni						
BKF Raver-Paul & Ctr2		<u></u>			<u>gar o</u> .	<b>JU IV</b>	<i></i>					95.2	96.5		•	* * 1
BKF Raver-Paul & Ctr2											98.6			*	•	. * 1
							1.				2950	<u> </u>				
BKF Raver-Paul & Ctr2			96.7								110.6	108.7	106.8			
and Centralia 1 off line											2380	2740	2540			
BKF Raver-Paul & Ctr2											108.8	107.8	105.1	*		r ** 1
and Centralia 1 off line											2430	2750	2610			
With Proposed Gener	ation 2	70 M	W: Ra	ver-P	aul 50	20 KV	line =	1834	MW p	re-ou	rtage					
BKF Raver-Paul & Ctr2				. * . *		*					100.5 2820	95.3	96.7		•	* * 1
BKF Raver-Paul & Ctr2									. :		98.7					
											2950			•	•	
BKF Raver-Paul & Ctr2			97.8								110.8	108.9	107.0			r - 14 - 1
and Centralia 1 off line			2930								2370	2740	2540			•
BKF Raver-Paul & Ctr2									-		108.9	107.9	105.1	*	•	•
and Centralia 1 off line									-		2430	2750	2610			
With Proposed Gener	ation 3	00 M	W: Ra	ver-P	aul 50	00 KV	line =	1836	MW p	re-ou	rtage	•				
BKF Raver-Paul & Ctr2									* .	: 1	100.7	95.4	97.0			r <b>sk</b> 1
											2800					
BKF Raver-Paul & Ctr2					1.						98.7			*		* *
	1				<u> </u>						2950		-			
BKF Raver-Paul & Ctr2			99.4					, ,			111.0	109.0	107.3			· ·
and Centralia 1 off line			2870								2360	2740	2530			
BKF Raver-Paul & Ctr2											108.9	107.9	105.1			k **
and Centralia 1 off line	,											2750		-	•	-

-

Table <u>Alte</u>	6. R							_						)r		
Proposed Generation Level Outage	LONGMR T - YELM 115	LONGMRT - OLY VAIL 115	KAPOWSIN - YELM 115	GRAVELLY - TILCM TP 116	50 DUPONT - QUARRY 115	DUPONT - GRAVELLY 115	FREDRICK - TILCM TP 115	ELECTHTS - KAPOWSIN 115	BLUMAER - OLY VAIL 115	TACOMA A - CENTR SS 230	OLYMPIA - TACOMA B 230	COWLITZ - TACOMA B 230	CHEHALIS - CENTR SS 230	Inp Proposed Generation		
Existing Frederickson  BKF Raver-Paul & Ctr2  BKF Raver-Paul & Ctr2	(149	MW) (	CTso	ff: Ra	ver-Pa	aul 500	O KV I	ine = ;	2019	99 2900		108.6 2450				* * *
and Centralia 1 off line  With Proposed General	ation 0	MW:	Rave	r-Pau	1 500	kV line	a = 20	26 M		2580	2800	119.9 1930				* *
BKF Raver-Paul & Ctr2								v 111)	<u> piQ</u>	100.2 2840		107.1 2520	97.6 2980		si.	* * *
BKF Raver-Paul & Ctr2 and Centralia 1 off line										2520	2770	118.4 2000			*	* *
With Proposed General BKF Raver-Paul & Ctr2	ation 2	00 M	W: Ra	ver-P	aul 50	<u>10 kV I</u>	<u>ine = </u>	2034		102 2740	ıtage	105.4	99.4 2890		*	* *
BKF Raver-Paul & Ctr2										100.6 2820		107.6 2500		*	*	* *
BKF Raver-Paul & Ctr2 and Centralia 1 off line			1							2430	2710		2570		*	* *
BKF Raver-Paul & Ctr2 and Centralia 1 off line										106.4 2500		118.9 1980		*	*	* *

	6. Rave						-			_			r				
Alter	mative Pl	an (Re	econ	ducto	or Fr	<u>ederi</u>	ckso	n-St.	Clai	ir 11:	5 kV	<u>line)</u>					
	9/ lin/	e loadin	a at S	90EN A	MA/ NI	orther	n Inte	rtia / l	VII at 1	1000/	loodir	· · · · · · · · · · · · · · · · · · ·	=	· =	ا ا	=	=
Page 2/2	70 til te	Oauli	y at z	203U N	100 14	OI U ICI	11 11110	ue / i	NI QL	100%	IOauli	ıy	Trip Pr		공		Trip BC
	LONGMR T - OLY VAIL	KAPOWSIN - YELM 115	GRAVELL	DUPONT - QUARRY 115	DUPONT .	FREDRIC	ELECTHT	BLUMAER	TACOMA	OLYMPIA	COWLITZ	CHEHALIS	Proposed Generation	Coulee gen 720 MW	Chief Joseph gens 1100 MW	hitehom &	BC Hydro gens 1820 MW
Proposed	T-0	Z - Y	Υ-1	ě	GP.	^- <u>-</u> ⊒	ω-Σ	<u>6</u>	Α.Ω	- TAC	-TA(	္ရင္ထ	nerat	20 M	gens	Fredo	75 18:
Generation Level Outage	LONGMR T - OLY VAIL 115 LONGMR T - YELM 115	ELM 115	GRAVELLY - TILCM TP 115	NRY 116	DUPONT - GRAVELLY 115	FREDRICK - TILCM TP 115	ELECTHTS - KAPOWSIN 115	BLUMAER - OLY VAIL 115	TACOMA A - CENTR SS 230	OLYMPIA - TACOMA B 230	COWLITZ - TACOMA B 230	CHEHALIS - CENTR SS 230	3	*	1100 MW	Whitehom & Fredonia 349 MW	20 MW
							•		. •	Ŭ		8				~	
With Proposed Gener	ation 250 N	/W: Ra	ver-P	<u>aul 50</u>	0 kV	line =	2035	MW		ntage			1				
BKF Raver-Paul & Ctr2									102.4		105.0				*	*	*
BKF Raver-Paul & Ctr2			<del></del>		<u> </u>	<del></del>		<u></u>	2720		2620	2860					
DNF naver-raul & Cu2		•							100.7 2810		107.8 2490	98.0 2960	*		*	*	*
BKF Raver-Paul & Ctr2			·		<del></del>	<del></del>	<del></del>	-		102.6	116.3		1				
and Centralia 1 off line									2400		2110				*	*	*
BKF Raver-Paul & Ctr2							· ·		106.5		119.1						
and Centralia 1 off line									2500	2730	1970	2640	•		-	-	-
With Proposed General	ation 270 M	W: Rav	ver-P	aul 50	0 kV	line =	2036	MW s	ore-ou	rtage						-	
BKF Raver-Paul & Ctr2					-:-				102.6		104.9	100.0			*	*	*
									2710		2630	2850					
BKF Raver-Paul & Ctr2									100.7		107.9	98.1			*	*	*
									2810		2490	2960					
BKF Raver-Paul & Ctr2		95.5							108.5	102.7	116.1	105.8			*	*	*
and Centralia 1 off line			<del></del>						2390	2680	2110	2530					
BKF Raver-Paul & Ctr2											119.2		, *		*	*	*
and Centralia 1 off line	-4 600 1	NA4- 50-			0.1371		0000	MA!			1970	2640					
With Proposed General	ation 300 M	w: Hav	rer-P	aui 50	U KV	ine =	2038	MW r			· .		1				
BKF Raver-Paul & Ctr2	*,*								95.1		104.7				*	*	*
				<del></del>						2690	2640			ď.			
BKF Raver-Paul & Ctr2	r <sub>e</sub> st								100.8		107.9		*		*	*	*
BVE Davies David & Obe		OT 4				-			2810	405.5	2480						٠.
BKF Raver-Paul & Ctr2		97.1									115.9				*	*	*
and Centralia 1 off line		3060									2130	<del></del>					
BKF Raver-Paul & Ctr2											119.3		*		*	*	*
and Centralia 1 off line							· ·		2490	2730	1960	2630	<u> </u>				

# FREDERICKSON 50/100/150 MW

Frederickson - 50/190/150 MW



July 17, 2000

Puget Sound Energy, Inc. 411 108th NE Bellevue, WA 98004-5515 Attn: Douglas K. Faulkner, Manager Energy Contracts

Re: Requests for Transmission Service – Frederickson OASIS Assignment Reference No. 117855
Preliminary Study Results

Dear Doug:

This is in response to your letter to me dated June 16, 2000 in which you requested an additional study pursuant to your OASIS Request No. 117855. Specifically, you asked us to first study the effects of adding 50 MW, 100 MW, and 150 MW at the Frederickson site, before studying the remainder of your request. The preliminary study is enclosed.

For the System Impact Study Agreement for the Frederickson OASIS Assignment Reference No. 117855, please see the attached preliminary study, "Frederickson Steam Generator Addition." This study explores the transmission capacity that would be needed to reliably interconnect a steam turbine at the PSE Frederickson Generation Station. Steam turbine sizes studied included 50, 100, 150, and 200 MW.

The results of studies showed that with minor improvements the existing Pierce and Thurston County transmission system can reliably interconnect a steam turbine with up to 150 MW output on the Frederickson Substation 115 kV bus. Above that level, several lines exceed their limits, and costs to increase ratings and build additional lines would be high. If this project is chosen additional studies will be needed using data that must be obtained specifically for the generator selected. Because generator tripping is required for a BPA outage, BPA must also be involved, and agree to it being added to their trip scheme.

Before finalizing the study, we would like to meet with you at your earliest convenience. In the meantime, we will proceed with studying the remainder of your request for 270 MW or 600 MW at Frederickson, and lastly 50 MW at Tenaska.

Sincerely,

Puget Søund Energy, Inc.

George Marshall

Its: Manager Transmission Contracts and OASIS Trading

#### FREDERICKSON STEAM GENERATOR ADDITION

Scoping Study
PSE Electric Transmission

#### INTRODUCTION

PSE Electric Transmission has been asked to assess the affect to the transmission system of additional generation at the existing Frederickson combustion turbine site in Pierce County. This report is a scoping document that summarizes studies done to find threshold levels where new generation could be added with large impacts to the existing transmission system. The added generation would be a steam unit with possible sizes being 50, 100, or 150 MW (200 MW was included to explore sensitivities).

#### CONCLUSION

If a new generator is installed at Frederickson Generating Station and connected to the existing 115 kV bus, and if the size is 150 MW or smaller, then impacts to the existing transmission system are expected to be minimal. A requirement for this addition is that during conditions of high north to south flow on the Raver-Paul 500 kV line, an equivalent amount of generation at Frederickson should be tripped automatically if an outage of the Raver-Paul 500 kV line were to occur. The generation could be tripped by an electronic signal supplied by BPA, but BPA must agree to this. The only line requiring conductor temperature upgrade is the Electron Heights-Boeing Puyallup-Frederickson 115 kV line. Also, at the highest generation level, a Remedial Action Scheme should be employed to trip or ramp generation at Frederickson in the event that two of the three 115 kV lines to Frederickson becomes out-of-service. An estimate of the cost for transmission interconnection facilities and improvements is \$800,000.

#### STUDY ASSUMPTIONS

Summer and winter seasons were studied, with a focus on high Raver-Paul loading and high north to south flows on lines going through Pierce County. Load sensitivity was performed for the summer season. The lines through Pierce County are:

Raver-Paul 500 kV line White River-Cowlitz-Olympia 230 kV line Covington-Cowlitz-Chehalis 230 kV line Frederickson-St. Clair 115 kV line Electron Heights-Blumaer 115 kV line White River-Fern Hill 57.5 kV line

The time frame was 2001 with the following improvements assumed to be completed:

Chief Joe-Monroe #4 line re-converted to 345 kV operation.

Bothell-Snoking #2 and Snoking-Maple Valley #2 230 kV lines energized.

Schultz-Raver #2 500 kV line rerouted from Raver to Echo Lake.

Bothell #2 and #3 230-115 kV transformers replaced with 300 MVA transformers.

Reactive power margin and voltage stability was not determined, it is anticipated that addition of generation with full reactive capability at Frederickson will improve voltage regulation in the area. This can be confirmed with reactive margin studies. Transient stability was not confirmed, and would be done when stability models, and machine specific parameters are provided.

Fred steam.doc

Page 1

Preliminary

The proposed Westcoast generator was studied as a sensitivity, to understand the combined impacts of the Frederickson steam turbine generator and the Westcoast generator. The total MW output of the Westcoast generators was modeled as 270 MW.

#### **OUTAGE ASSUMPTIONS**

Outages taken included single contingency (N-1) outages and common mode outages. The single contingency outages are taken automatically, and include all lines in southern King, Pierce and Thurston Counties. The common mode outages are:

White River north 230 bus, south 230 bus, north115 bus, and south 115 bus Krain Corner 115 bus, Alderton 115 bus, Frederickson 115 bus Electron Heights 115 bus, Saint Clair 115bus, Blumaer 115 bus West Olympia 115 bus, Plum Street 57.5 bus PSE Olympia north 115 bus, and south 115 bus, Tono phase shifter BPA Olympia east 230 bus, west 230 bus, and 115 bus

The following use governor load-flow following WSCC guidelines.

Raver-Paul 500 line; Trip BC Hydro

Raver-Paul 500 line; Trip BC Hydro, FGStm, WC

Raver-Paul-Centralia G2 500 BKF; Trip BC Hydro

Raver-Paul-Centralia G2 500 BKF; Trip BC Hydro, FGStm, WC

Raver-Paul-Centralia G2 500 BKF & Centralia G1; Trip BC Hydro

Raver-Paul-Centralia G2 500 BKF & Centralia G1; Trip BC Hydro, FGStm, WC

Paul-Allston 1&2 500 lines on common right-of-way; Trip BC Hydro

The formula for tripping BC Hydro generation is:

Trip generation =  $1.3 \times (Westside NI north-to-south - 1450 MW)$ FGStm stands for tripping the proposed Frederickson steam turbine and gen. WC stands for tripping the proposed Westcoast generator. BKF stands for breaker failure.

#### **FINDINGS**

The transmission through flow can be seen in Table 1, which shows line flows before outages are taken for heavy summer, lighter summer, and heavy winter. Line flows on the Raver-Paul 500 kV line, as an example are 1800 to 1900 MW in the summer, and decrease to 1200 MW in the winter. In these seasons, the West Side Northern Intertie (WSNI) is 2850 MW in the summer cases, and is 1450 MW in the winter cases. If the winter import OTC goes above 1450 MW, then transmission through flow will increase in the winter. Load sensitivity that was performed for the summer season was to reduce the area load by 1000 MW, from 5758 to 4758 MW, an 18% reduction. The results indicated that for lines at or near overload, the overloads increased slightly as loads were scaled down by 1000 MW. This is a favorable result because as loads go down in the summer, ambient air temperatures also cool, as in night-time conditions, and line ratings go up.

#### Summer

During the summer season loading on lines can be closer to line ratings than during other seasons because of transmission through flow, and because the line ratings are significantly lower in the summer on lines having a lower conductor temperature rating.

The results of outage simulations are given in Table 2, for single contingency outages (N-1), and common mode outages, except that the Raver-Paul 500 kV outage results are given in Tables 3-6, and are discussed later. The outage results for other than Raver-Paul 500 kV show that line loadings remain within their ratings up to an addition of

Ex	(WAG-4)
Page 89 of 2	19

150 MW of generation. An exception is the double line loss of the Alderton-Frederickson and Frederickson-St. Clair 115 kV lines. This outage is an N-1 outage if one of the other two lines to Frederickson is already out for some reason. The temperature rating of the Electron Heights-Boeing Puyallup-Frederickson 115 kV line should be raised to significantly increase the threshold levels at which generation can safely generate during conditions such as line maintenance, unplanned outages, and the double line outage. The 1272 kcm Narcissus conductor portions should be uprated to 75C conductor rating, and the 795 kcm Tern portions to 100C conductor rating.

#### Raver-Paul 500 kV Outage

The most severe outage is the Raver-Paul 500 kV outage, and combination outages, which include the Raver-Paul 500 kV line. The combination outages studied are a breaker failure at Paul that trips both the Raver-Paul line and the Centralia #1 generator, and the same breaker failure when the Centralia #2 generator is also out of service. Results are given in Tables 3-6, and include summer heavy load, summer light load, without and with a proposed Westcoast IPP connected to BPA South Tacoma Switch. The tables show when PSE lines will overload without tripping the Frederickson steam generator, or an equivalent amount in MW at Frederickson.

BPA arms a RAS when there are high north to south flows on the Raver-Paul 500 kV line. The RAS sends trip signals to selected generators north of this line when the RAS detects that the line is tripped out of service. The generators that are armed are determined according to the flow level on the Raver-Paul line, and other factors, as described in BPA Dispatcher Standing Order (DSO) 307. In the power system simulations, for high flow levels on the Raver-Paul line, the generators that were tripped included Whitehorn, Fredonia, 1024 MW at Chief Joseph, and units in Canada following the formula:

#### MWtoTrip = 1.3(IngledowCusterflow - 1450MW)

The results indicate that for light summer loads, or for Frederickson steam generator sizes above 100 MW, PSE lines overload for the breaker failure outage of the Raver-Paul 500 kV line and Centralia generator unit 2, unless the Frederickson steam generator is tripped. If the Westcoast generator is installed at about 270 MW, and if it is tripped for the same outage, then the above holds true for Frederickson steam generator sizes above 50 MW. The Frederickson steam generator, or one of the combustion turbine generators will need to be tripped during summer load and temperature conditions when the Raver-Paul 500 kV line loading is high. Tripping will not be needed during winter conditions because the Raver-Paul line loading is low.

The Tables 3-6 show overloads for the breaker failure outage and when the other Centralia generator unit 1 is off line. The Raver-Paul pre-outage flow is above 2000 MW. In practice, BPA would reduce the flow on the Raver-Paul 500 kV line, following DSO 307 for Level 4, so that the overloads would not happen if the outage were to occur. But running the outage at this high level illustrates the need for a Raver-Paul flow threshold that results in significant overloads if violated.

The White River-Fern Hill 57.5 kV line overloads with outages of the Raver-Paul line. A relay is being installed at White River to detect when the line is being overloaded and the relay will sent a signal to automatically trip the line breaker at White River. All the power system simulations were done with either the White River-Fern Hill line open, or with the relay modeled to open the line up if the flow level on the line is above its seasonal rating.

#### Winter

Some common mode outages do not achieve a solution for winter loading conditions. The Olympia 230 kV bus is divided between east and west segments with both 230-115 kV transformers on one bus segment, the east bus. Loss of the Olympia 230 west bus results in no solution.

#### COSTS

Transmission costs to install up to 150 MW of new generation at Frederickson are expected to include the following:

RAS for Frederickson generator tripping for Raver-Paul outage, and for loss of two lines

\$50,000

Breaker and line bay at Frederickson for generator, 115 kV

\$300,000

Conductor temperature upgrade of Electron Heights-Boeing Puyallup-Frederickson 115 kV line

\$400,000

#### **POWER FLOW DRAWINGS**

Schematic type power flow drawings of selected conditions are given following the tables. The drawings provided are a few that represent the thousands of unique combinations of conditions that could be shown. For each season, hundreds of outages were simulated for each level of proposed steam generation at Frederickson, without and with the proposed Westcoast project. The drawings include summer No Outage cases without and with Frederickson steam generator at 150 MW, and without and with the proposed Westcoast project.

They are given in the following order:

Figure	Condition	Season	Frederick-	West-
			son Steam	coast
1	No Outage	HS	0	0
2	No Outage	HS	150	0
3	No Outage	HS	0	270
4	No Outage	HS	150	270
5	No Outage	HW	0	0
6	No Outage	HW	150	0
7	No Outage	HW	0	270
8	No Outage	HW	150	270
9	BPA Olympia 115 kV Bus	HW	0	0
10	BPA Olympia 115 kV Bus	HW	150	0
11	Freder-SW 28 Tie & Freder-Tillicum Tap	HS	150	0
12	White River-Cowlitz-Olympia B 230 kV	HS	0	0
13	Bkf Raver-Paul & Centr G2	HS	0	0
14	White River-Cowlitz-Olympia B 230 kV	HS	150	0
15	Bkf Raver-Paul & Centr G2	HS	150	0
16	Bkf Raver-Paul & Centr G2, trip F.Steam	HS	150	0
17	White River-Cowlitz-Olympia B 230 kV	HS -1000	0	0
18	Bkf Raver-Paul & Centr G2	HS -1000	0	0
19	White River-Cowlitz-Olympia B 230 kV	HS -1000	150	0
20	Bkf Raver-Paul & Centr G2	HS -1000	150	0
21	Bkf Raver-Paul & Centr G2, trip F.Steam	HS -1000	150	0

# Table 1. Line flows with Incremental levels of Frederickson Steam Generation

#### Facility loading in MVA

Seasonal case	Frede	rickson Stean	n Level (witho	out / with Wes	tcoast)
Element or path	0 MW	50 MW	100 MW	150 MW	200 MW
2002 Heavy Summer					
West Side NI, Ingledow-Custer 1&2	2850 / 2850	2850 / 2850	2851 / 2850	2851 / 2851	2851 / 2851
RAVER - PAUL 500	1827 / 1867	1830 / 1871	1833 / 1874	1837 / 1877	1841 / 1882
OLYMPIA - TACOMA B 230	325 / 374	326 / 375	327 / 376	328 / 377	329 / 378
TACOMA A - CENTR SS 230	303 / 321	304 / 322	306 / 324	307 / 325	309 / 327
FREDRICK - BOE_PUY 115	34 / 34	45 / 45	57 / 57	69 / 70	82 / 82
FREDRICK - SW28TIE 115	30 / 30	31 / 29	49 / 46	71 / 68	95 / 92
FREDRICK - TILCM TP 115	117 / 120	130 / 133	142 / 145	155 / 158	167 / 170
2002 Heavy Summer, lighter lo	oad case				
West Side NI, Ingledow-Custer 1&2	2850 / 2851	2849 / 2850	2850 / 2851	2851 / 2852	2851 / 2851
RAVER - PAUL 500	1920 / 1957	1922 / 1960	1924 / 1963	1928 / 1966	1932 / 1970
OLYMPIA - TACOMA B 230	341 / 390	342 / 391	343 / 392	344 / 393	345 / 394
TACOMA A - CENTR SS 230	326 / 344	327 / 346	329 / 347	330 / 349	332 / 350
FREDRICK - BOE_PUY 115	31/32	43 / 43	56 / 56	68 / 68	80 / 80
FREDRICK - SW28TIE 115	29 / 30	28 / 27	45 / 42	68 / 65	92 / 88
FREDRICK - TILCM TP 115	123 / 126	135 / 138	147 / 151	160 / 163	172 / 175
Dec. 2002 Heavy Winter					
West Side NI, Ingledow-Custer 1&2	1450 / 1449	1451 / 1450	1451 / 1451	1451/ 1450	1451 / 1450
RAVER - PAUL 500	1174 / 1210	1177 / 1213	1179 / 1216	1182 / 1219	1185 / 1222
OLYMPIA - TACOMA B 230	198 / 246	198 / 246	199 / 247	200 / 247	200 / 248
TACOMA A - CENTR SS 230	87 104	88 / 106	90 / 107	91 / 108	92 / 110
FREDRICK - BOE_PUY 115	44 / 44	56 / 56	68 / 68	81 / 81	93 / 93
FREDRICK - SW28TIE 115	24 / 20	45 / 42	69 / 66	94 / 91	119/116
FREDRICK - TILCM TP 115	90 / 93	103 / 106	115 / 118	128 / 130	140 / 143

### Table 2. Outages with Incremental levels of Frederickson Steam Generation

		Facility	loading in %	of rating		Notes
<u>Outage</u>	Frede	rickson Stear	n Level (with	out / with Wes	stcoast)	
Element at % of rating	o MW	50 MW	100 MW	150 MW	200 MW	
ST CLAIR - QUARRY 115, 20	02 Heavy S	Summer				
ELECTHTS - FRED TAP 115				96.6 / 97.7	111.5 / 112.6	
same line with lighter summer load					114.4 / 115.5	
FREDRICK - TILCM TP 115, 20	002 Heavy	Summer				
ELECTHTS - FRED TAP 115	i de la companya de l			100.8 / 101.8	115.7 / 116.7	
same line with lighter summer load					117.8 / 118.9	
GRAVELLY - TILCM TP 115, 20	002 Heavy	Summer				
ELECTHTS - FRED TAP 115		ing the second s		99.4 / 100.4	114.3 / 115.3	
same line with lighter summer load					116.6 / 117.7	
FREDRICK - HEMLOCK 115, 2	2002 Heavy	Summer				
ELECTHTS - FRED TAP 115					106.6 / 105.3	
same line with lighter summer load					105.7 / 104.3	
FREDRICK - TILCM TP 115					101.0 / 101.7	
same line with lighter summer load					102.9 / 103.7	
BUS SAINT CLAIR 115, 2002 H	leavy Sumr	ner				
ELECTHTS - FRED TAP 115					105.7 / 106.8	
BUS ALDERTON 115, 2002 He	avy Summe	er .				
ELECTHTS - FRED TAP 115					102.5 / 101.1	
BUS OLYMPIA 230 EAST. 2002	2 Heavy Su	mmer - lighte	er load case			
TACOMA A - CENTR SS 230	/ 96.3	/ 96.6	/ 97.1	/ 97.4	/ 97.9	
FREDRICK - TILCM TP 115				/ 96.0	99.2 / 102.1	
FREDRICK-SW28TIE & FREDR						,
ELECTHTS - FRED TAP 115	115.3	159.2	203.1	247.3	Not Run	
FREDRICK - FRED TAP 115	· . D== 000	130.5	164.4	198.5	• • • • • • • • • • • • • • • • • • •	
WHITE RV 115 - WHITE RV57.5				00 0 / 00 0	96.6 / 97.4	
KRAINCOR 115-57.5 XFMR 1 BUS WHITE RIVER SOUTH 115			99.4 / 100.3	98.0 / 98.8	50.0 / 81.4	
		102.6 / 103.5		98.8 / 99.7	97.0 / 97.9	
STEVNSON - KRAINCOR 57.5,				au.u / aa./	J1.07 J1.0	
			105.1 / 105.0	105.1 / 105.0	105.1 / 105.0	#
CRW PAUL - ALLSTON 500 1&2						
		111.9 / 114.3		112.7 / 115.1	113.1 / 115.5	
					1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	

Notes: # - Line loading is insensitive to proposed generation.

		Teki	. O =	Π-		ا ا	500 <b>'</b>	4( D	_1_4-	<b>-</b>							
		I abl	e 3.a -								tage	s <b>-</b>					
			F	rede	ricks	on S	team	i Ger	nerat	ion							
		% lin	e load	ling at	2850	MW (	North	ern in	tertie /	/ NI st	1009	Load	lina		<b>7</b> =	1 =	[ 큐 등
	C CONGMR T - YELM 118			_											i rip Coulee gen 720 MW	Trip Chief Joseph	Whitehorn & Fredonia 34
	M M	S S	NSI N		Z	2	矣	₽	됐	AEA	×.	₽	ALIS	Ì	gen	sep	S CIC
Frederickson Steam	ı 🕌		- 4	-	5	GP,	Î	و	- 5, - 5	ο	-			9	720 Ste	h ge	Fre
Generation Level		7	Ę	ב ב	ARR	AVE	Ę	AR	APC	<u>'</u>	- CENTA SS 230	TACOMA B	ENT		M	gens 1100 MW	Fredonia 349 MW
	115	\ E	= =	ATP	Y 11	·	뒿	₹	SW(	₽	H S	Æ	R S		<u>.</u>	8	a 34
Outage		115		115	Ch	15	115	5	Ž	115	S 23	230	S 230			N N	. W
NATitle assisting Francis	<b></b>	. 0 OT	1 4.4			_			5		_						₹ .
With existing Frede	ricksor	1201	S. 14	JMW 1	totai;	Haver	-Paul	500 K	V line	= 182	O MV	/ pre-	outage	<u>-</u>	•	٠.	
Raver-Paul 500 outage																*	* *
BKE Davies Bank & Otro						<u> </u>		-	<del></del>					4			
BKF Raver-Paul & Ctr2	.															*	* *
BKF Raver-Paul & Ctr2	102	5 101.6	. 00 2	05.4	<del></del>	<del></del>			461					$\exists$			
and Centralia 1 off line	2760			95.1			97.4						2 105.2 ) 2620	ŗ		*	* *
BKF Raver-Paul & Ctr2	1		<del> i</del>				· · ·		2130	2030	2430	2/30	2620	-			
and Centralia 1 off line															*	*	* *
With Frederickson 50MW	/Steam	unit add	ied 10	OM/\A/ +-	tel· D-	war D-	ul EOO	A/ I:	_ 100 1	A44/				1			
Raver-Paul 500 outage	- OlGain	un aut	, 1 <i>9</i>	SIAI AA [[	<u>nai</u> , Hā	ver-1-8	ui SUU i	v iine	= 1824	MVV pr	e-outa	<del>je</del>		1			
						÷										*	* *
Raver-Paul 500 outage			· · · · · ·	<del></del>										i			
														*		*	* *
BKF Raver-Paul & Ctr2		<del></del>					<del></del>			100	99.1		95.3				
		* .									<del>-</del>					*	* *
BKF Raver-Paul & Ctr2											98.7						
														*		* 1	* *
BKF Raver-Paul & Ctr2	107.5	105.9	101.8	101.4	98.0	<b>9</b> 9.5	103.7	97.0	105.4	104.5	109.4	108.4	105.6				
and Centralia 1 off line	2650	2700	2790	2790			2690		1.		2430					• '	
BKF Raver-Paul & Ctr2	103.0	101.0	98.0	95.0			97.0		102.0	100.0	109.0	108.0	105.0			* 1	, ,
and Centralia 1 off line	2740	2800			· ·	- 1			2780	2840	2440	2740	2610	1			
BKF Raver-Paul & Ctr2					-		.×								*	* 1	* *
and Centralia 1 off line														1			

	7	Γable				aul 5 on St					ages	. <b>-</b>					
	LONGMR T - YELM 115			_		S DUPONT .					100% TACOMA A.	OLYMPIA -		i np Frederickson steam unit	Trip Coulee gen 720 MW	Chief Joseph	Trip BC Hydro gens
Frederickson Steam Generation Level Outage	- YELM 115	LONGMR T - OLY VAIL 115	KAPOWSIN - YELM 115	GRAVELLY - TILCM TP 115	DUPONT - QUARRY 115	DUPONT - GRAVELLY 115	FREDRICK - TILOM TP 115	ST CLAIR - QUARRY 115	ELECTHTS - KAPOWSIN 115	BLUMAER - OLY VAIL 115	- CENTH SS 230	TACOMA B 230	CHEHALIS - CENTR SS 230	steam unit	20 MW	gens 1100 MW	ns 1820 MW Fredonia 349 MW
With Frederickson 100MW	Steam	unit ac	ided, 2	49MW	total; F	laver-P	aul 500	kV line	e = 182	7MW p	re-outa	ge	· · · · · · · · · · · · · · · · · · ·	7			•
Raver-Paul 500 outage																* 1	* *
Raver-Paul 500 outage								-	•					*		* 1	* *
BKF Raver-Paul & Ctr2	96.4			97.5		95.6	99.8		95.8		99.5	95.2	95.7			* 1	
BKF Raver-Paul & Ctr2		<del></del>			•			-	<del></del>	<del></del>	98.8		95	*		* 1	
BKF Raver-Paul & Ctr2	111.5	110.2	105.2	107.7	104.3	105.7	110.0	103.2	108.8	108.8	109.9	108.8	106.1			* *	
and Centralia 1 off line	<del></del>	2600	2690	2520	2670	2600	2420	2710	2580	2630	2410	2740	2580				-
BKF Raver-Paul & Ctr2		101.9	98.5	95.3			97.6		102.1	100.5	109.1	108.3	105.4	*	•	* *	*
and Centralia 1 off line	2730	2790					···		2770	2840	2430	2740	2600				
BKF Raver-Paul & Ctr2														*	* '	* *	*
and Centralia 1 off line	<u> </u>										-	<del> </del>		,			- 1
With Frederickson 150MW	Steam	unit ad	ded, 29	9MW t	otal: R	aver-Pa		kV line	= 1830	MW pr	e-outaç	e		1			1
Raver-Paul 500 outage							96.2								. 1	* *	*
Raver-Paul 500 outage														*	•	* *	*
BKF Raver-Paul & Ctr2	100.3 2840	98.0	95.7			101.8 2740		99.3	99.2	96.9	99.9	95.4	96.2		•	* *	*
BKF Raver-Paul & Ctr2	2010			LULU							98.9		95.1	*	•	* *	*
BKF Raver-Paul & Ctr2	115.5	114.5	108.7	113.9	110.5	112.0	116.2	109.5	112.2	113.1	110.3	109.1	106.5				
and Centralia 1 off line	2440	2490	2580	2260	2400	2340	2160	2450	2470	2520	2390	2740	2560		,		^
BKF Raver-Paul & Ctr2	103.8	102.0	98.6	95.4		<del></del>	97.7		102.2	100.6	109.2	108.4	105.4	*		k *	
and Centralia 1 off line	2720	2790							2760	2830	2430	2740	2600				
BKF Raver-Paul & Ctr2					*********									*	* 1	k *	
and Centralia 1 off line																	

		Table					500 l am, a				7	s <b>-</b>					
Frederickson Steam Generation Level Outage With existing Fredericksor	LONGMR T - YELM 115	% LONGMR T - OLY VAIL 115	KAPOWSIN - YELM 115	GRAVELLY - TILCM TP 115	DUPONT - QUARRY 115	DUPONT - GRAVELLY 115	FREDRICK - TILCM TP 115	ST CLAIR - QUARRY 115	ELECTHTS - KAPOWSIN 115	BLUMAER - OLY VAIL 115	% TACOMA A - CENTR SS 230	a OLYMPIA - TACOMA B 230	CHEHALIS - CENTR SS 230	Trip Frederickson steam unit	Trip Coulee gen 720 MW	Trip Whitehorn & Fredonia 349 MW	Trip BC Hydro gens 1820 MW
Raver-Paul 500 outage		, 173IVI	-	, i idvel	-ı aul c	JU KY	I	OIVIVY P	- Juid	<del>Ac</del>	96.4				*	*	*
BKF Raver-Paul & Ctr2	98.0	97.3			· · · · · · · · · · · · · · · · · · ·	<del></del>	<del> </del>		95.0	96.3			102.8		*	*	*
BKF Raver-Paul & Ctr2	113.1	113.7	105 1	100.1	97.2	98.5	102.0	96.4	108.0	112.4	2460						
and Centralia 1 off line	2520	2530		2860	<i>31</i> .3	<b>30.</b> 3	2780	<i>5</i> 0.4	2620		2150				*	*	*
BKF Raver-Paul & Ctr2 and Centralia 1 off line															* *	*	*
With Frederickson 50MW S	Steam u	mit add	ed. 199	MW to	tal: Ra	ver-Pa	ıl 500 k	V line :	= 1916	/IW/ pre	-outage	•					İ
Raver-Paul 500 outage											96.9				*	*	*
Raver-Paul 500 outage								- ,			96.5			*	*	*	*
BKF Raver-Paul & Ctr2	102.0	101.6	95.5	96.2			98.1		98.4	100.6	107.0	100.4	103.2		*	. *	*
	2790	2810				·				2840	2430		2660				
BKF Raver-Paul & Ctr2	98.1	97.4							95.1	96.4	106.6 2450	100.2 2860	102.9 2680	. *	*	*	*
BKF Raver-Paul & Ctr2	117.1	118.0	108.6	106.4	103.5	104.8	108.3	102.7	111.5	116.7	<del></del>						- 1
and Centralia 1 off line	l	2430											- 1		. *	*	*
BKF Raver-Paul & Ctr2		113.9			<del></del>		102.1									٠.	
and Centralia 1 off line	2490		2690				2750			2530				*	*	# .	~
BKF Raver-Paul & Ctr2									<u> </u>					*	* *		
and Centralia 1 off line																-	

		Tab	le 4.l	b. Ra	aver-	Paul	500	kV R	elate	ed Ou	utage	s -						
			Fr	ederi	ckso	n Ste	eam,	and	Light	Loa	d							
					* .						* - * - * - * - * - * - * - * - * - * -				_	_		<b>-</b> -
				ling at	2850	MW	North	ern Ini	tertie /	NI at	100%	load	ing		TripiF	Tip C		7 <del>6</del> 7
	<u> </u>	2	₹	GR,	Ę	P	FRE	STC	E	BE-0	TAC	5	문		rede	Coutee	hief	≨ 77 77
	୍ଦୁ କୁ	o M∓	8	E E	Š	Š	DA	ST CLAIR -	즲	BLUMAER -	Š	. ×	¥		ricks	e ge	Jose	ydro Horn
5-4	LONGMR T - YELM 115	LONGMR T - OLY VAIL	KAPOWSIN - YELM 115	GRAVELLY - TILCM TP 115	DUPONT - QUARRY 115	DUPONT - GRAVELLY 115	FREDRICK - TILCM TP 115	H-C	ELECTHTS - KAPOWSIN 115	<del>,</del> 50	TACOMA A - CENTR SS 230	OLYMPIA - TACOMA B 230	CHEHALIS - CENTR SS 230		Frederickson steam unit	gen 720	Chief Joseph gens 1100 MW	BC Hydro gens 1820 MW Whitehorn & Fredonia 349 MW
Frederickson Steam	Ĕ	5	Ή	큳	UAR	A V	Ę	QUARRY 115	S	OLY VAIL 115	8	, AC	SE CE		itean	WW O	Jens :	s 18:
Generation Level	_ ₹	Š	Z Z		F	Ē	×	AHY	ŏ	≨	H	MA	TA		5	ξ	110	
	5	L 115	쟑	7	115	Υ 11	70	115	NIS/	Ξ.	SS	D N	SS		=		Ď S	349   ₹
Outage		5		5		Ch	ភ		115	· Oi	230	8	ä				2	ξ.
With Frederickson 100MW	Steam	n unit a	dded. 2	249MW	total: F	Raver-F	aul 500	kV lin	e = 191	9MW p	re-outa	ıge						
Raver-Paul 500 outage											97.3			7			*	* *
												1.1						
Raver-Paul 500 outage								:		-	96.6			7	*		<b>*</b> 1	* *
		1			· ·									]				
BKF Raver-Paul & Ctr2	105.9	105.8	98.9	102.4	99.6	100.8	104.3	98.7	101.8	104.8	107.4	100.6	103.7	·			* 1	k *
	2650	2670	2900	2720	2880	2810	2610	2930	2780	2700	2410	2850	2630	]				
BKF Raver-Paul & Ctr2	98.2	97.6							95.2	96.6	106.7	100.3	102.9		*		* *	*
	<u> </u>		-		<del></del>						2440	2850	2670	1				
BKF Raver-Paul & Ctr2				112.6	109.8	111.0	114.5	108.9	114.9	121.0	117.8	114.3	114.0			٠,	k *	. *
and Centralia 1 off line	2320	2330	2500		2460		2270	2490	2420	2360	2120	2690	2270	1				
BKF Raver-Paul & Ctr2	l	114.0			97.5	98.7	102.2	96.6	108.3		117.1	114.0	113.3		*		* *	*
and Centralia 1 off line  BKF Raver-Paul & Ctr2	2460	2470	2670	2840			2720		2570	2500	2130	2690	2290					
and Centralia 1 off line															*	* *	* . *	*
1						<del></del>				<u> </u>				j				
With Frederickson 150MW		unit ao	ded. 29						= 1922	MW pr		<del>je</del>	•	1				
Raver-Paul 500 outage	95.2			98.7	95.9	97.1	100.7	95.1			97.8						<b>*</b>	*
Raver-Paul 500 outage							2790				00.7							ı
Ravois, autobo outage											96.7				*	•	*	*
BKF Raver-Paul & Ctr2	109.9	110.1	102.3	108.6	105.8	107.0	110.5	104.9	105.2	100 1	107.0	100.9	104.1					
				2360													*	*
BKF Raver-Paul & Ctr2	98.4	97.7						20.0	95.3		106.8							ı
									33.0			2850			*	*	*	*
BKF Raver-Paul & Ctr2	125.1	126.6	115.5	118.9	116.1	117.3	120.8	115.2	118.4	125.3								
and Centralia 1 off line				2090												*	*	*
				100.4				<del></del>		112.9		<del> </del>						
		2430					2650			2470		1.0		· '	*	*	₩	*
3KF Raver-Paul & Ctr2									an j	<del></del> .								
and Centralia 1 off line														. 1	× 1	, <b>स</b>		× 1

		Tab	ie 5.	a. R	aver:	Paul	500	kV F	Relate	ed O	utage	s -							
		F	reder	ickso	on St	eam,	with	Wes	stcoa	st 27	OMV	1							
				21											T.	<b>=</b>	Trip	<u> </u>	3
						_					:100%	_			Trip Frederickson steam uni	Trip Coulee gen 720 MW	δ	ō :	<u> </u>
	. Q		APC	Ä	Ē	Ş	HE 0	C	LEC	Ę	ACC	Σž	並		deri	ulee	ief J	niteh	ĭ
	Ž	Ž	Ž.	Ę	Ž	Ž	ÄΩ	₽	<u> </u>	Ā	Š	PIA	IA Li		ckso	gen	osep	orn ~	iro o
Frederickson Steam	CONGMH I - YELM 115	LONGMR T - OLY VAIL 115	KAPOWSIN - YELM 115	GHAVELLY - TILOM TP 115	DUPONI - QUARRY 115	DUPONT - GRAVELLY 115	FREDRICK - TILCM TP 115	ST CLAIR - QUARRY 115	υ. Σ	BLUMAER - OLY VAIL 115	. A	OLYMPIA - TACOMA B 230	o.		n ste	720	Chief Joseph gens 1100 MW	Fre	BC Hydro gens 1820 MW
Generation Level		3	Ę	Č	AAR	AVE	, LC	IAR	APC	\ \ \	Ä	ိုင္ဆို	ENT		am	×	ns 1	doni	1800
	115	A	115	A TP	Y ==	- 5	Ŧ	₹	SW(	₽	π g	. Ā B	A SS		≦.		8	a 34	ξ
Outage		115	7	115	·	15	115	5	ELECTHTS - KAPOWSIN 11	15	TACOMA A - CENTR SS 230	230	CHEHALIS - CENTR SS 230				€.	Trip Whitehorn & Fredonia 349 MW	
With existing Frederickso	n 2 CT	's 1491	/IW tota	al- Rava	r-Peul	500 KV	line –	1860M	M pro-c	u da ne	J								
Raver-Paul 500 outage		<u> </u>		<u> </u>		300 KV	11110 -	1800141	v pie-c	uage				7			s.•		
																	*	* 1	k
Raver-Paul 500 outage									-								*	* 1	
								:											
BKF Raver-Paul & Ctr2											104.0	103.9	100.2				*	* *	,
	_		<i>5</i>		· .						2640	2800	2840						
BKF Raver-Paul & Ctr2				•										*			*	* *	ŧ
BKF Raver-Paul & Ctr2	107	1 105.5	101 5	07.5		95.6	99.8		105.1	404.4	444.4	447.0	440.0	ł	• *				
and Centralia 1 off line	1	2720				95.6	33.0				114.4 2300						* :	* *	1
BKF Raver-Paul & Ctr2											2000	2040	2440						
and Centralia 1 off line									-					*			* 1	k **	
BKF Raver-Paul & Ctr2											:			*		* :	<b>*</b> 1	* *	١
and Centralia 1 off line																			ł
With Frederickson 50MW 5	Steam	unit add	led. 19	9MW to	tal; Ra	ver-Pa	ul 500 l	«V line	= 18631	MW pre	-outage	•							l
Raver-Paul 500 outage																,	* 1	k *	l
	<u> </u>	••	·			•													ı
Raver-Paul 500 outage	1													*	*	•	k #	* *	
BKF Raver-Paul & Ctr2	<b> </b>		<del></del>					06.1	06.0	05.6	104.4	101.0	100.6						I
ord Travor-1 during Otto								96.1	96.0	95.6	104.4	2790				•	k si	r <b>★</b>	l
BKF Raver-Paul & Ctr2									<del></del>		99.4								l
														*	*			r #r	I
BKF Raver-Paul & Ctr2	111.2	109.8	105.0	103.8	100.4	101.9	106.1	99.4	108.5	108.4	114.8	117.9	111.0				* *	k : #	l
and Centralia 1 off line	2570	2620	2700	2700	2830	2770	2600	2880	2600	2650	2280	2640	2430						l
3KF Raver-Paul & Ctr2	104.3	102.6	99.1	95.7	•		98.0		102.6	101.2	109.7	108.9	105.9	*	*		k y	r <b>*</b>	Ì
and Centralia 1 off line	2730	2780				1		·. ·	2760	2820	2420	2740	2580						
3KF Raver-Paul & Ctr2													.	*	* *	t , #	r, #	, <b>*</b>	
and Centralia 1 off line						•	······································												l

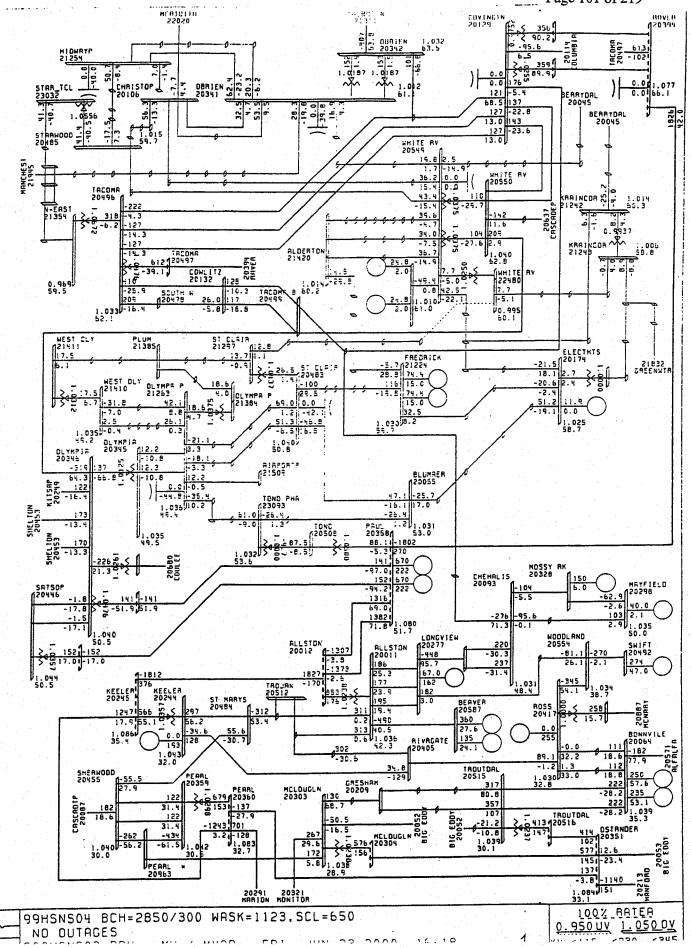
				1 1 X																
			Tab	le 5.t	. Ra	ever-	Paul	500	kV R	elate	d Ou	ıtage	s -							
			Fr	ederi	ickso	n Ste	eam,	with	Wes	tcoas	st 27	OMW	<b>!</b>							
	l makin i						•													
																			_	
			% lin	e load	ling at	2850	MW I	Northe	ern Int	ertie /	NI at	100%	loadi	ng		Trip F	Trip C		Trip	rip E
		ē	Ē		ဋ	2	2	Æ	TS	ב	EL	TAC	5	윤		Frederickson steam unit	Coulee gen 720 MW	Chief Joseph gens 1100 MW	Whitehorn & Fredonia 349 MW	BC Hydro gens 1820 MW
į		LONGMR T - YELM 115	LONGMRT-	KAPOWSIN - YELM 115	GRAVELLY -	DUPONT - QUARRY 115	DUPONT - GRAVELLY 115	FREDRICK - TILCM TP 115	CLAIR - QUARRY 115	ELECTHTS.	BLUMAER - OLY VAIL 115	TACOMA A - CENTR SS 230	ОLYMPIA - ТАСОМА В 230	CHEHALIS - CENTR SS		erick	ee g	Jos	ebor	tydro
		IA T	A T	NIS/	Ę	, <del>,</del>	Ξ.	홋	75	STH	9	-	Ē	R		nos	en 7	ieph	₩.	ger
	Frederickson Steam	-,			=	A UC	GRA	≟	චි	٠ <u>۲</u>	ဥ	Ω	TAC	် က		stea	20 \	gen	Fred	15 1
	Generation Level	Z Z	\ \ \	EE	ξ	AR)	加入	8	ARR	PO		IT	Š	HIN.		ž L	Š	S 11	fonia	B20
		115	OLY VAIL 115	115	TILCM TP 115	= = = = = = = = = = = = = = = = = = = =	٠ <u>٠</u> ٠	Ŧ	Y 11	KAPOWSIN 115	É	R SS	8	SS		킾		8	348	M M
	Outage		115		115	S	115	115	5	- Z	5	23	230	230				Š	¥.	
	With Eradanakaan 100144	/ C+n==	۔ خلصوں	44	ADLES	4-4-1-	· · · · ·				74 41 4 *	Ŭ							<	ĺ
	With Frederickson 100MW Steam unit added, 249MW total; Raver-Paul 500 kV line = 1867MW pre-outage  Raver-Paul 500 outage																			
	maver-raul DOU OUTage										4.57						٠.	*	*	*
	Payer Paul 500 artage	-					<del></del>								-					
ľ	Raver-Paul 500 outage														*	*		*	*	*
	BKF Raver-Paul & Ctr2	100 1	07.0	05.7	100.0	000		400 0	05.5			101.5	1011	104 4	+			r		
ſ	ONF Maver-Faul & CITZ	100.1		95.5	100.0		98.1	102.3	95.5	99.0	96.6			101.1				*	*	*
L	3KE Davier David B Own	2850		,	2850		2960	2720				2590	2790		-					
f	BKF Raver-Paul & Ctr2											<b>99</b> .5	95.4	95.7	*	*		*	*	*
	SKE Davies David & Over	1156	4444	400 1	445 :	400-					4455		445		1					ı
ı	SKF Raver-Paul & Ctr2	1										115.2	12.2					*	*	*
1	and Centralia 1 off line	2470			2450	2580	2520	2350	2620	2500	2550	2270	2640	2410						
ł	3KF Raver-Paul & Ctr2		102.7	99.2	95.8			98.1		102.7		109.8			*	*		*	*	*
1	and Centralia 1 off line	2/10	2770							2750	2810	2410	2740	2580	}					
ı	BKF Raver-Paul & Ctr2														*,	*	*	*	*	*
1	and Centralia 1 off line	<u> </u>													J					
	With Frederickson 150MW	Steam	unit ad	ded. 29		otal; R	aver-Pa		kV line	= 1870	MW pr		е							
r	Raver-Paul 500 outage				96.3			98.6				95.1						*	*	*
		<u> </u>			-															
r	Raver-Paul 500 outage														*	*		*	*	*
						· · · · · · · · · · · · · · · · · · ·		· ·	<del></del>						,					
P	KF Raver-Paul & Ctr2	ł										105.3						*	*	*
l		2710	2790	2900	2500	2690	2610	2370	2750	2750	2820	2570								
В	KF Raver-Paul & Ctr2											99.5	95.5	95.8	*	*		*	*	*
					·													-		
ľ	KF Raver-Paul & Ctr2		102.9	99.3	95.9			98.2				109.9						*	*	*
1	and Centralia 1 off line	2700				- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1						2400								
	KF Raver-Paul & Ctr2				-			-		1		115.7			*	*		*	*	*
a	and Centralia 1 off line	2370	2420	2510	2200	2340	2280	2110	2380	2400	2450	2250	2640	2400						
ı	KF Raver-Paul & Ctr2	. •													*	*	• <b>★</b> ,	*	*	*
a	nd Centralia 1 off line																			
				0.5																

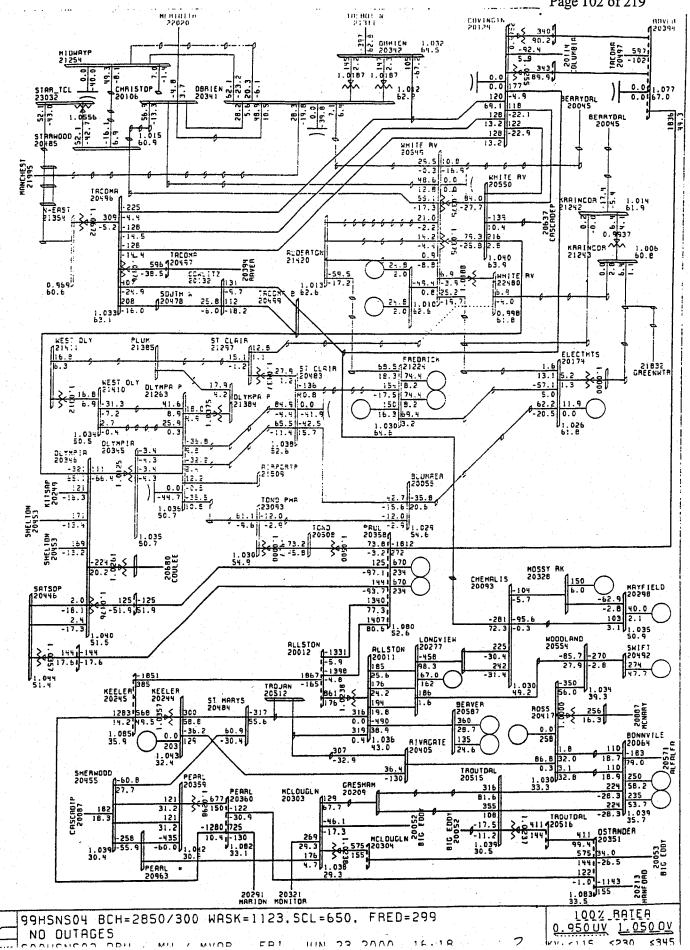
	Table 6.a.	Raver-P	aul 500 l	kV Rela	ated O	utage	s -	
Frede	rickson Ste	am, with	Westcoa	ast 270	MW, a	nd Lig	ght Loa	ad -
	% line loadin	a at 2050 k	MAT Northa		- / <b>h</b> II -	4.000/	1	

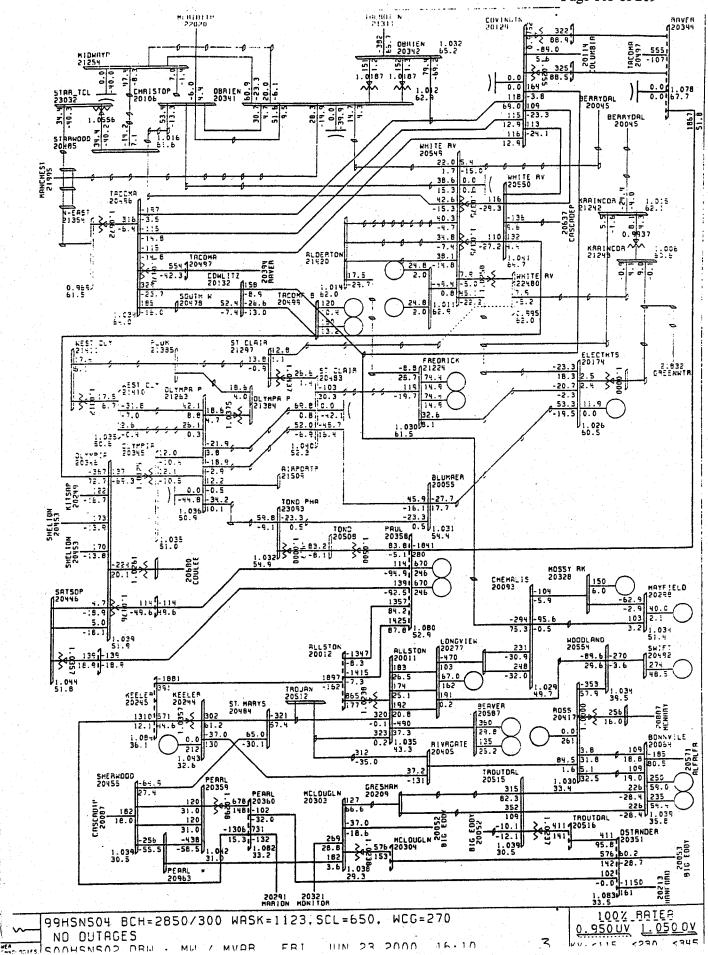
		% lir	ne load	ding a	t 2850	MW C	North	ern In	tertie	/ NI a	100%	6 load	ling		Ę	7 7	Į .	1 7	를 다
	LONGMR T	-					_		_	_		_		)	Frederickson steam unit		Children Too MW	Whitehorn &	BC Hydro gens 1820 MW
	AR T	i i	NSI NSI	E	2	i 2		₹	; <u>;</u>	Ţ	×	PIA	<u> </u>		CKSO	g g	osep	om &	to g
Frederickson Steam					و			غ ز	٠.		-				u Ste	3	n ge	7	ens
Generation Level	- YELM 115	3	<u> </u>	کّ	Ŕ		် ဉ်	ARF	₽	\ - -	Ä	Š	EN T		am	X	. ns	don	1820
	115	OLY VAIL 1	YELM 115	TILCM TP 115	QUARRY 115	GHAVELLY 115	뒥	₹ 2	KAPOWSIN	OLY VAIL 115	CENTR SS	À	CENTR SS		5		00	Fredonia 349	N N
Outage		115		115	· O	115	115	5	Z I	115	S 230	TACOMA B 230	S 230				× ×	WW 6	
With existing Frederickso	n 2 CT	s. 149N	//W tota	∐; Rave	r-Paul	500 kV	line =	1949M\	່ ທ Wore⊷o	utage	J		. •					<	
Raver-Paul 500 outage										3	101.6	3 96.1	98.1	٦.					
							filitation Portugal				2710						*	*	*
Raver-Paul 500 outage								٠			97.2			٦.			_		
		-							٠.			,		"			. *		
BKF Raver-Paul & Ctr2	101.6	101.4	95.4						98.3	100.4	111.9	109.4	108.2	·			*	*	
	2790	2810	)		· · · ·					2840	2260	2730	2440						
BKF Raver-Paul & Ctr2	98.8	98.2			c				95.7	97.2	107.3	100.8	103.5				*	*	
	ļ		<u> </u>					· ·	<u></u>	:	2420	2840	2640						ı
BKF Raver-Paul & Ctr2	- 1		108.4		99.8	101.0	104.5	98.9	111.3	116.5	122.4	123.2	118.6				*	*	
and Centralia 1 off line			2620			2810	2680	2890	2530	2480	2040	2590	2180						-
BKF Raver-Paul & Ctr2	1		105.8			99.1	102.7	97.0	108.8	113.4	117.6	114.4	113.9	*			*	*	*
and Centralia 1 off line	2500			2820	2940		2740	2970	2590	2530	2120	2680	2280						-
BKF Raver-Paul & Ctr2 and Centralia 1 off line	1		100.8	96.7		95.1	98.7		103.8	107.3	110.9	108.6	107.1	*		*	* ,	*	*
		2610	<del></del>						2720	2650			2540	]					1
With Frederickson 50MW S	Steam L	mit add	led. 199	MW to	tal; Ra	ver-Pa	ıl 500 k	V line :	= 1952N	/W pre	-outage		_	1					1
Raver-Paul 500 outage			•								102.2	96.4	98.5				*	*	*
Payor Boyl 500 autors	-							<u> </u>			2680		· · · · · · · · · · · · · · · · · · ·						
Raver-Paul 500 outage							*				97.3		***	*	*		*	* 1	٨
BKF Raver-Paul & Ctr2	105.8	105.7	98.8	007	05.0	07.4	100.6	05.4	404.5										
Distriction and a Ouz	2660	2680	30.0	98.7	95.9	97.1		95.1			112.4						* :	* 1	*
BKF Raver-Paul & Ctr2	99.0	98.4				-	2820		2780		2240								
		-							95.0	97.4	107.4	Α,		* .	*		*	* . 1	*
BKF Raver-Paul & Ctr2	120.9	122.1	111.9	108.9	106.1	107.3	110.8	105.2	114.8	120.8	2410 122 B								
and Centralia 1 off line			2520								2030						*	* 1	1
BKF Raver-Paul & Ctr2			106.0		98.0		102.8				117.7								1
and Centralia 1 off line			2660				2710				2110			*	*		* ;	* *	1
BKF Raver-Paul & Ctr2			100.9			95.3	98.8				110.9								
and Centralia 1 off line	2600										2370		1	*	*	*	* '	* •	
			<del></del>	<del></del>															_

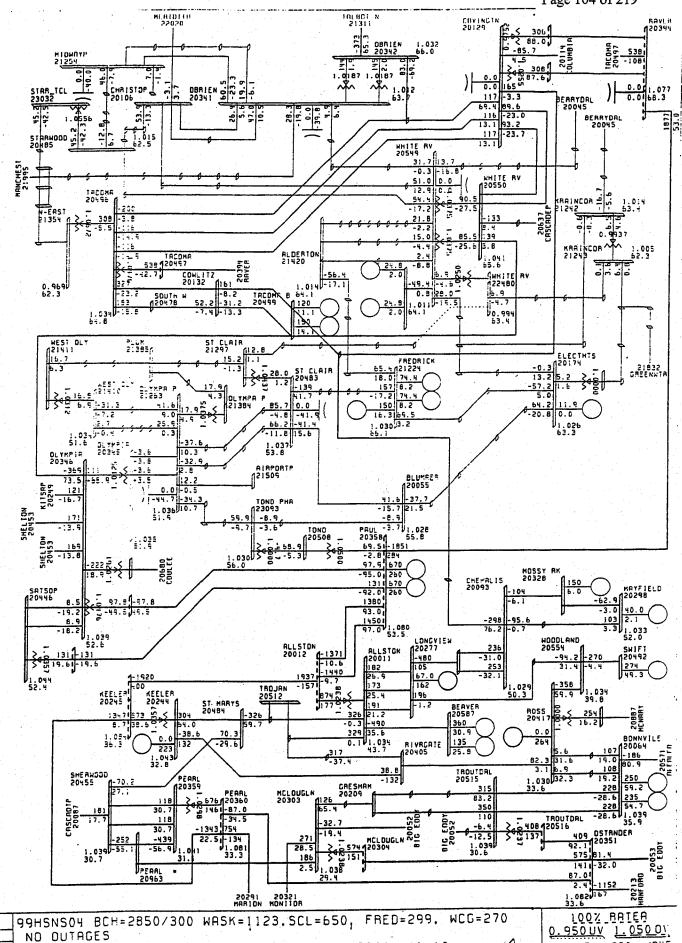
Table 6.b.	Raver-Paul 500 kV Related Outages -
Frederickson Ste	am, with Westcoast 270MW, and Light Load

		% lin	ne load	ding a	2850	MW	North	ern In	tertie .	/ NI at	100%	6 load	ina		- To	1 5	결	를	T Tip
	5	_		_	_	_							-				Chief		ВС
	ONGMR T	ONGMAT	KAPOWSIN	GRAVELLY	DUPONT -	- TNOANC	FREDRICK - TILCM TP 115	5	ELECTHTS	BLUMAER	FACOMA A	OLYMPIA -	CHEHALIS		Frederickson steam unit	ee	발	Whitehorn	BC Hydro gens 1820 MW
	ÎA T	. 5 ⊣	VSIN	Ę	<del>-</del>	Ŧ	Š	CLAIR -	HIS	ÉA	À	×	SIT		ksor	gen	Joseph	Š	90
Frederickson Steam	1		- 7	,	Ş	GA	∃	و		· ·					els t	720			Sug
Generation Level	YELM 115	OLY VAIL 115	- YELM 115	TILCM TP 115	QUARRY 115	GRAVELLY 115	ĽĆ	QUARRY 115	APO	OLY VAIL 115	CENTR SS	TACOMA B	CENTR		am	N N	gens 1100 MW	doni	1820
	115	<u>¥</u>	116	뒫	<b>1</b>	. 4	76	₹	Š	≩	A S	. F	R SS		5		8	Э4	§
Outage		115	Ŭ.	115	, OI	115	115	5	KAPOWSIN 115	15	S 230	230	\$ 230				₹ ¥	Fredonia 349 MW	
Mith Fraderickes 1001 ()	V 04										-							>	ı
With Frederickson 100MV Raver-Paul 500 outage	- 1		idded, 2			Raver-F			e = 19	55MW p				7					
naver-raur 500 outage	95.1			<b>9</b> 5.1			97.0					7 96.7	99.0	۱.			*	*	*
Raver-Paul 500 outage	-					-					2640			4					ı
naver-raul 500 outage	1						. *				97.4			*	*		*	*	*
BKF Raver-Paul & Ctr2	100								<del></del>					-					
DAF Haver-Paul & Cli2	1		102.3								112.9	110.0	109.1				*	*	*
BKF Raver-Paul & Ctr2	2530 99.1			2590	2740	2670	2490	2780			2220	2730	2400	1					
ON Haver-Faul & Cli2	99.1	98.6							96.0	97.5	107.5		103.7	*	.*		*	*	*
BKF Raver-Paul & Ctr2	105.0	100.4	445.0	445.0						<u> </u>	2390			-					
and Centralia 1 off line	125.0		115,3				* -					123.8	119.5				*	*	*
BKF Raver-Paul & Ctr2	<b>—</b>		2430			2330	2200		-		2010	2580	2150						
and Centralia 1 off line	2430		106.1			99.4	102.9		109.0			114.7		*	*		*	*	*
BKF Raver-Paul & Ctr2	108.5			2790	2970	2890	2670	3020	2540	2480	2100	2670							
and Centralia 1 off line	2600		101.1	97.0		95.4	99.0		104.0			108.8		*	*	*	*	*	*
		2610							2710			2590	2530	]					
With Frederickson 150MW	1		lded. 2:						= 1958	BMW pr	e-outaç	je		1.					
Raver-Paul 500 outage	99.0	98.4		101.2	98.4	99.6	103.1	97.5	95.8	97.4	103.2	96.9	<b>9</b> 9.4				*	*	*
Dougs Doul 500 out-on				2750	<u></u>		2590		· ·	-	2610	`							
Raver-Paul 500 outage											97.4			*	*		*	*	*
BKF Raver-Paul & Ctr2	1127	4140	105.7	4444	400.0	100.0	440.0	400 4					<del></del> -						
Diti navel-Faul & Cli2			105.7														*	*	*
BKF Raver-Paul & Ctr2			2640	2270	2410	2350	2160	2460				2720							
DRF haver-raul & Cit2	99.3	98.7							96.1	97.7		101.2		*	*		* 1	*	*
PVE Davier David & CV-C	100.0	400.7	1400									2840							. 2
BKF Raver-Paul & Ctr2			118.8													,	<b>*</b> , 1	<b>*</b> .15	*
and Centralia 1 off line			2330																
			106.2				103.0							*	*	٠. ١	<b>*</b> .1	* 1	*
[		<del></del>	2620		3000			3080				2670							
			101.2	97.1		95.5	99.1					109.0		*.	*	* 1	* 1	<b>*</b> , 1	•
and Centralia 1 off line	2600	2610	2810				·		2710	2640	2370	2580	2530						L









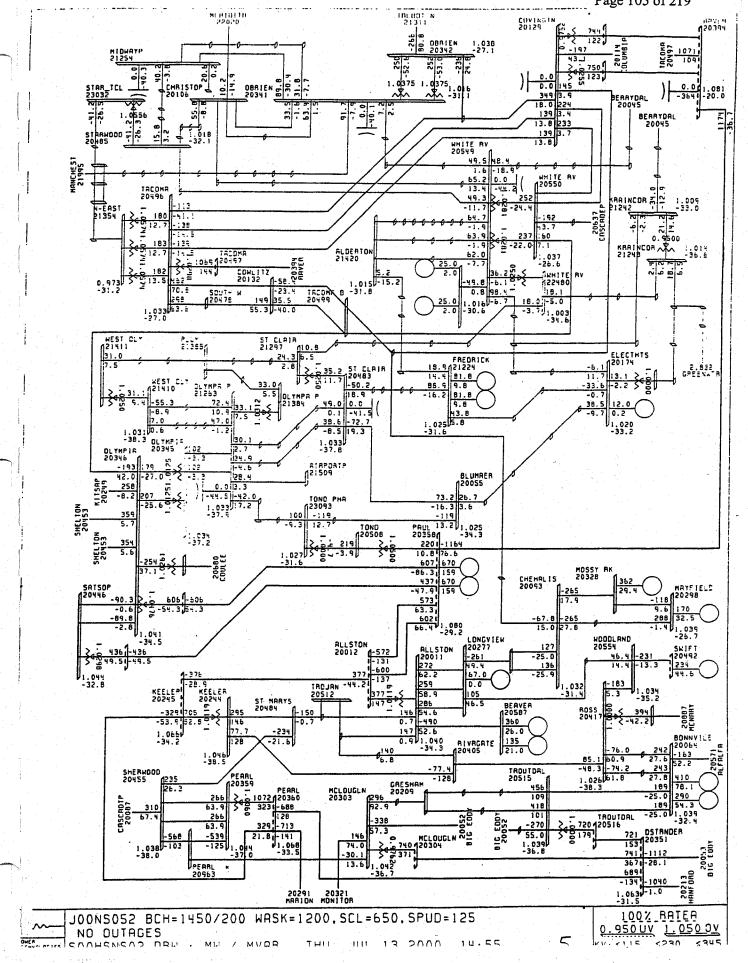
E D 1

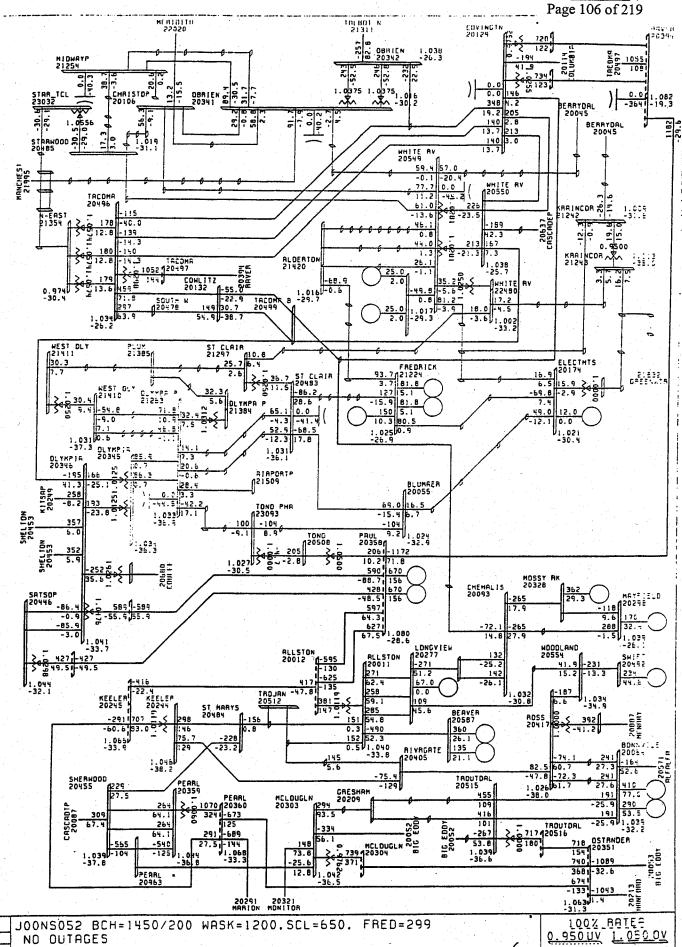
MIJ / MYOP

Jevonerieva DBA

HIN 32 SAVA

1





THU, IIII 13 2000 13:48

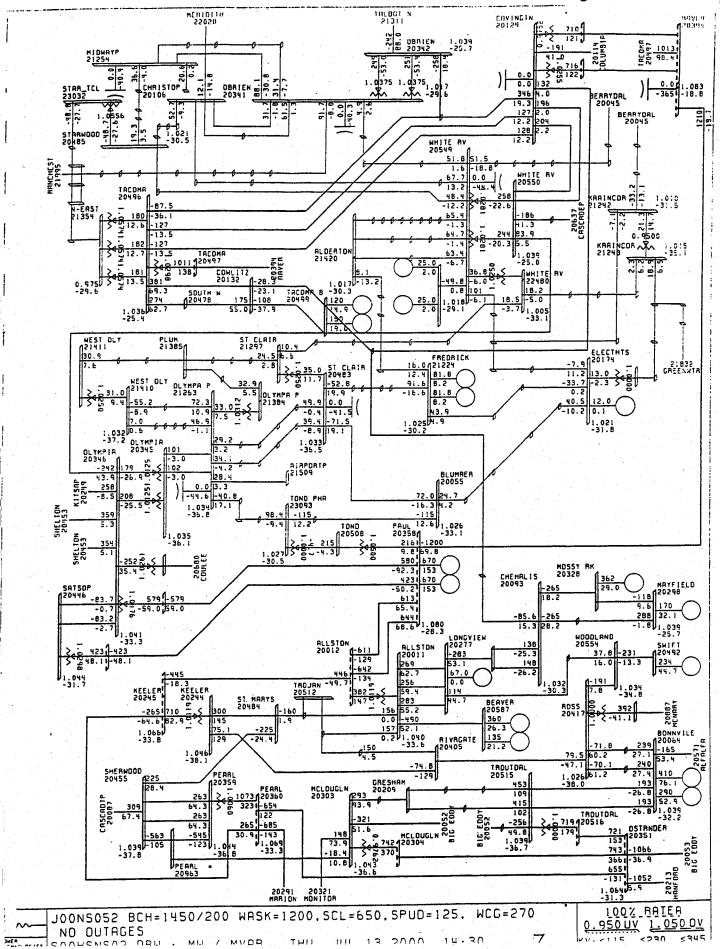
6

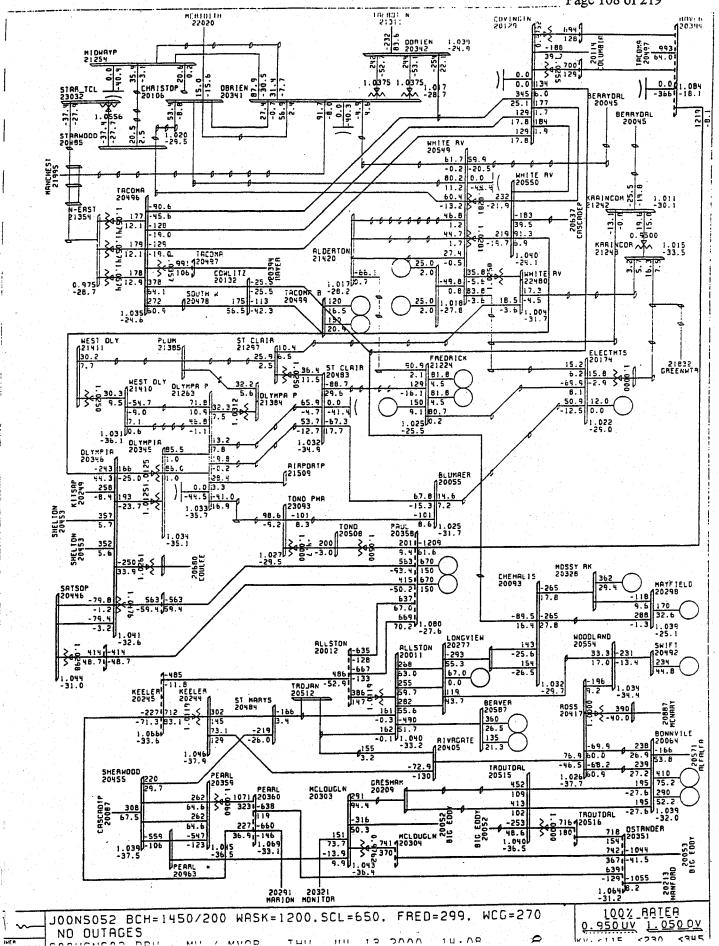
KV - 115

≤**२**45

<230

ENOLIDEES SOOHSNSOZ, DRW : MW / MVAR





16202 16202 20321 MON1TOR 100% RATEA J00NS052 BCH=1450/200 WASK=1200.SCL=650.SPUD=125 0.950UV 1.050 OV BUS OLYMPIA 115 BUS THH: IIII (12 2000) 14.22 9 LOCIES SOOHSNSO2 DRW : MW / MVAR

#FR10110 22020

STOP

ত্রাল

2 8

2.6

\$ 183 \$ 13.5

183 -42.7

- 136

PLUM 21385g

CLYMPR P 21263 69.1

10.6

46.0

) 0.0 3.5

20.000

1-380 HEELERI REELERI 20245 20244

146 77.3

1.046

20963

35.5783. 1.0651 -34.5

234

1 TACOMA 1074 **1**20497

SCUTH W

COWL 172 20132

1.0556 1.0556 2.050 2.05

N-ERST 21354

HEST DLY

0250

OF TWE TE

-158 30.5

276

-57.6

78.31-78.3

SHERHOOD 20455

SHEL TON 20453

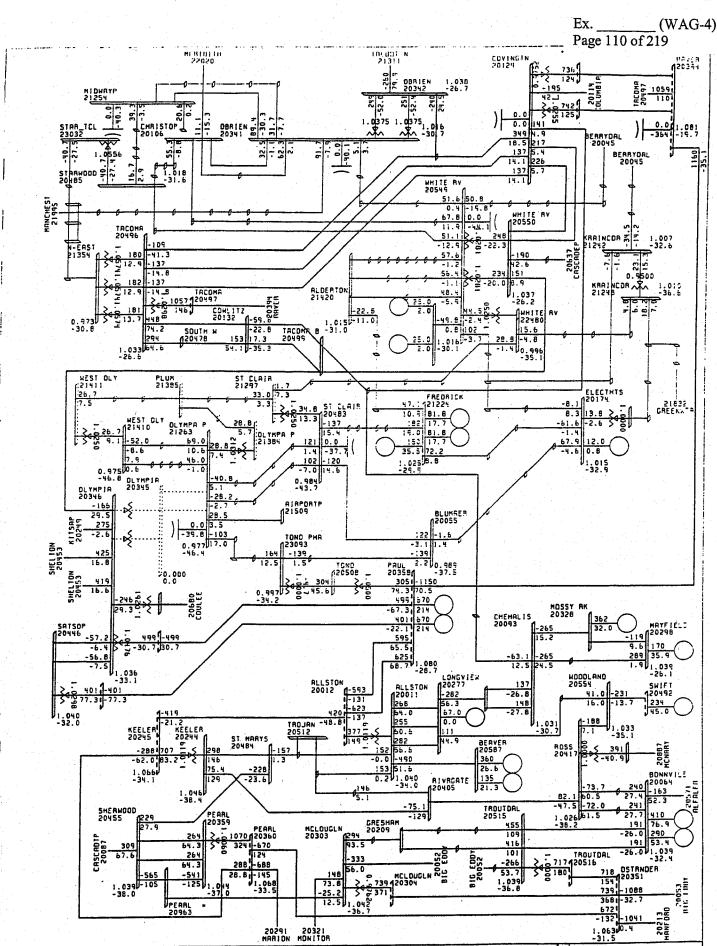
9.11-52.0 -8.6

0.964 0.6 DLYMP!R 20345

30.0

-58.0 501 -501 -6.8 5-28.4 28.4

7.5

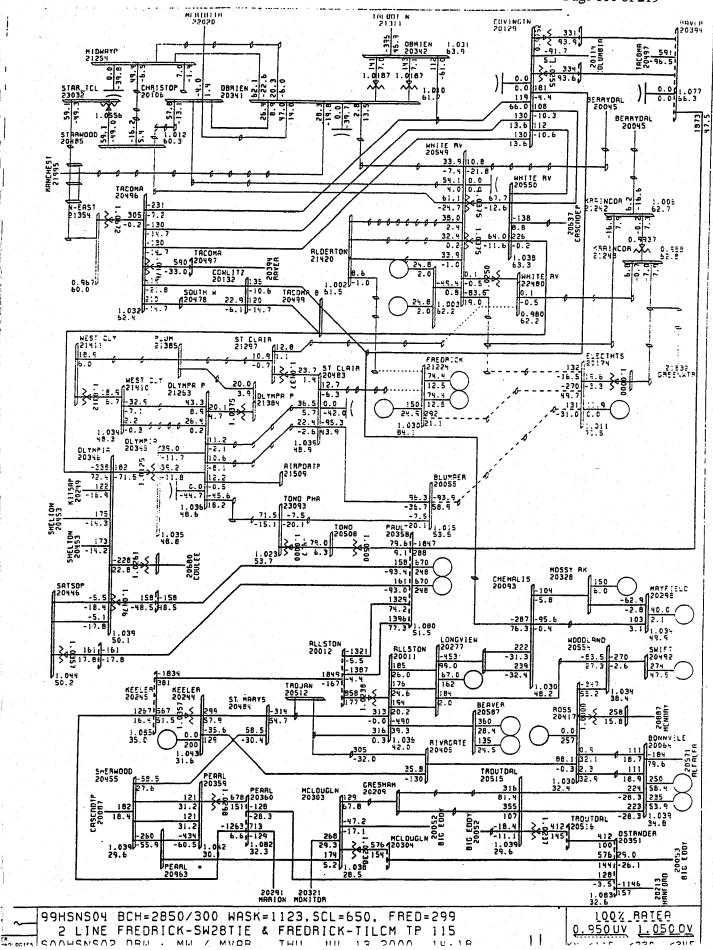


J00NS052 BCH=1450/200 WASK=1200.SCL=650. FRED=299

BUS OLYMPIA 115 BUS

S00HSNS02 DRU - MU / MVDR THU - 12 2000 12.01

100% BAIEA 0.950UV 1.050GV



99HSNS04 BCH=2850/300 WASK=1123.SCL=650 SL WHITE R-COWLITZ-OLYMPIA B 230 TO MILE SOUTHENESS OF THE SAME A MANDE FRI

PERRL

#10HAYP

30 1000 F

N-EAST

0.969

WEST D\_Y 21411 16.9

0LYMP!=

SHEL TON 299 11.5

-35.7

-11.9

SATSOP 120446

1.034J-0.4

9

1-e.5

- ! 6 . 4 125

-15.2

1-5.4

286 -286

1.041

48.4

SHERWOOD 20455

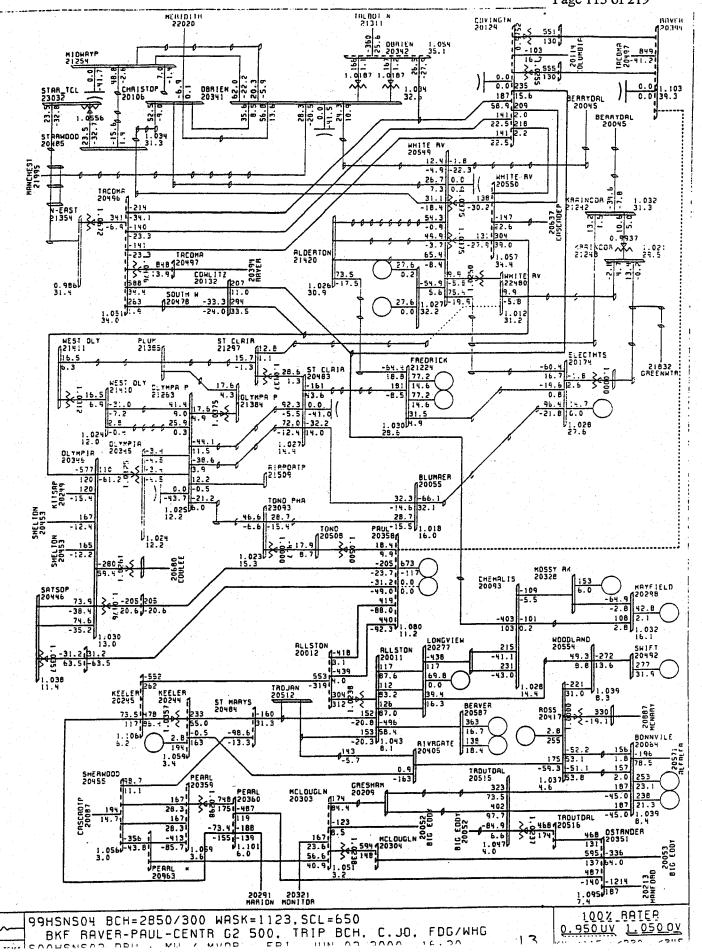
18.6

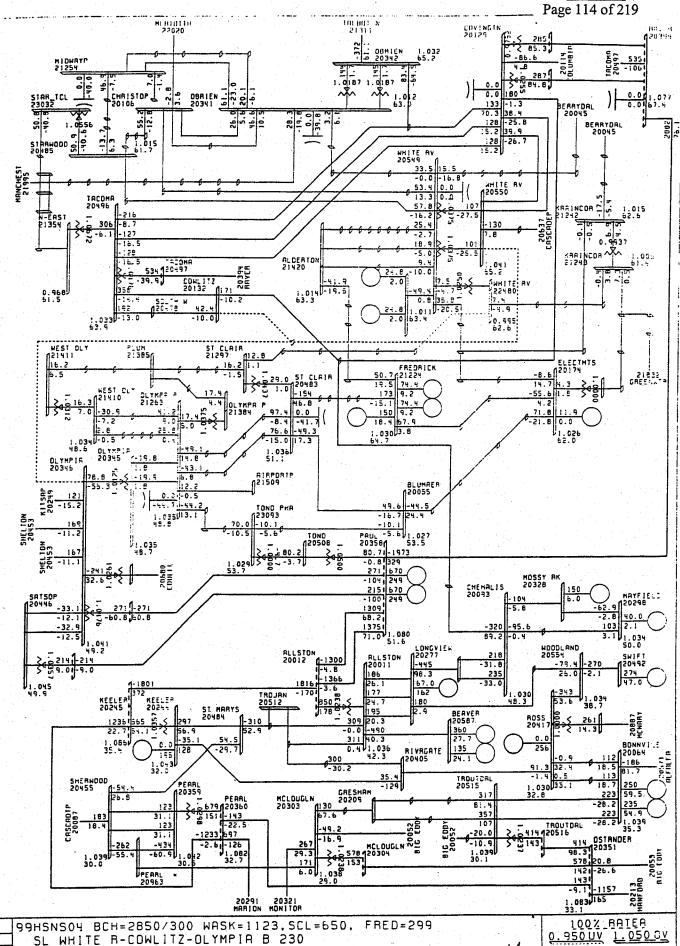
THIN US SUUV 16,28

100% BAIEA 0.950UV 1.0500V V11. -115 ~23N

158 1.083 161 32.9

17





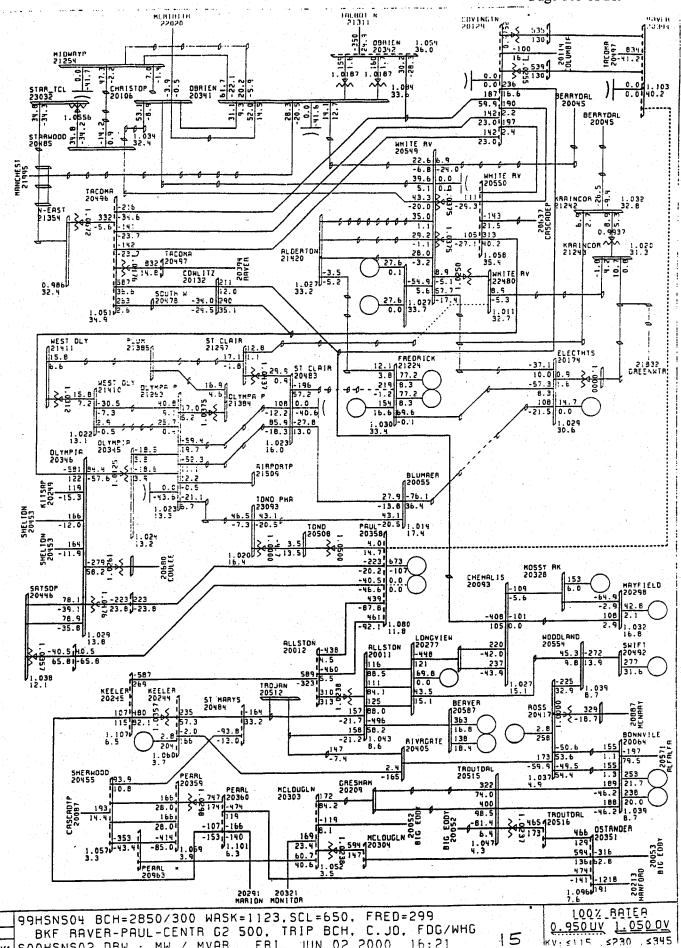
COLORES SOUHENSON DRW : MW / MVAR FRI HIN 02 2000 16-20

14

V. -115

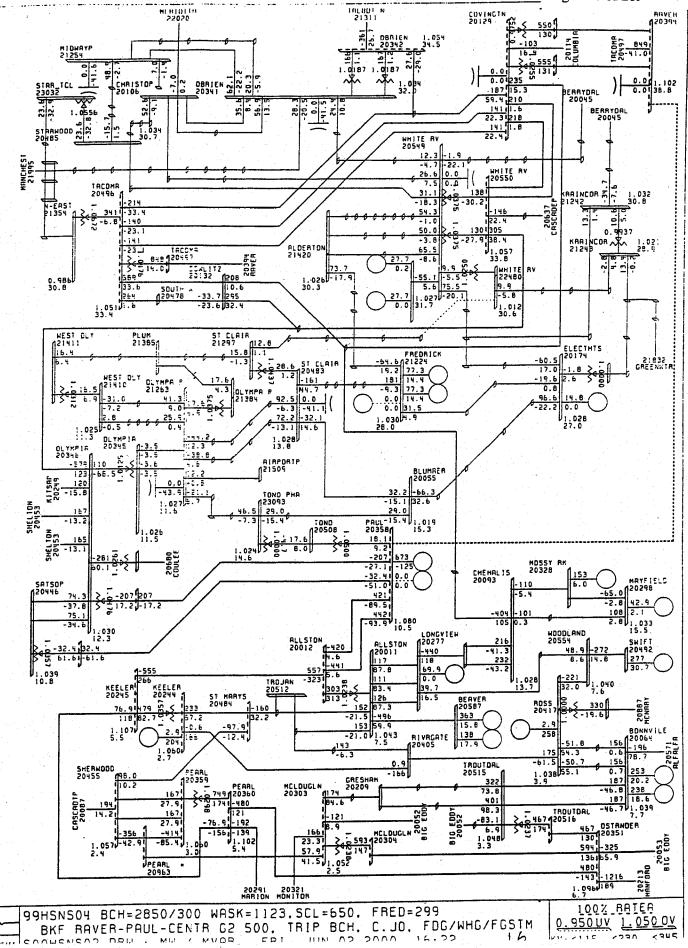
<230

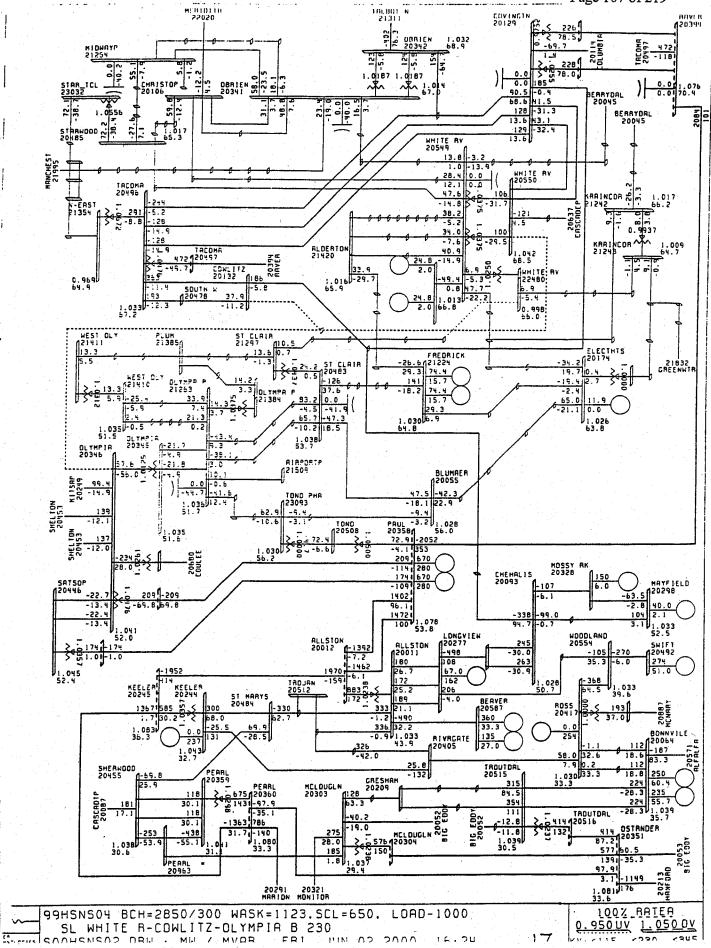
KV: \$115 . \$230 . \$345



FRI. JUN 02 2000 16:21

CHOCLOGIES SOOHSNSOZ . DRW : MW / MVAR

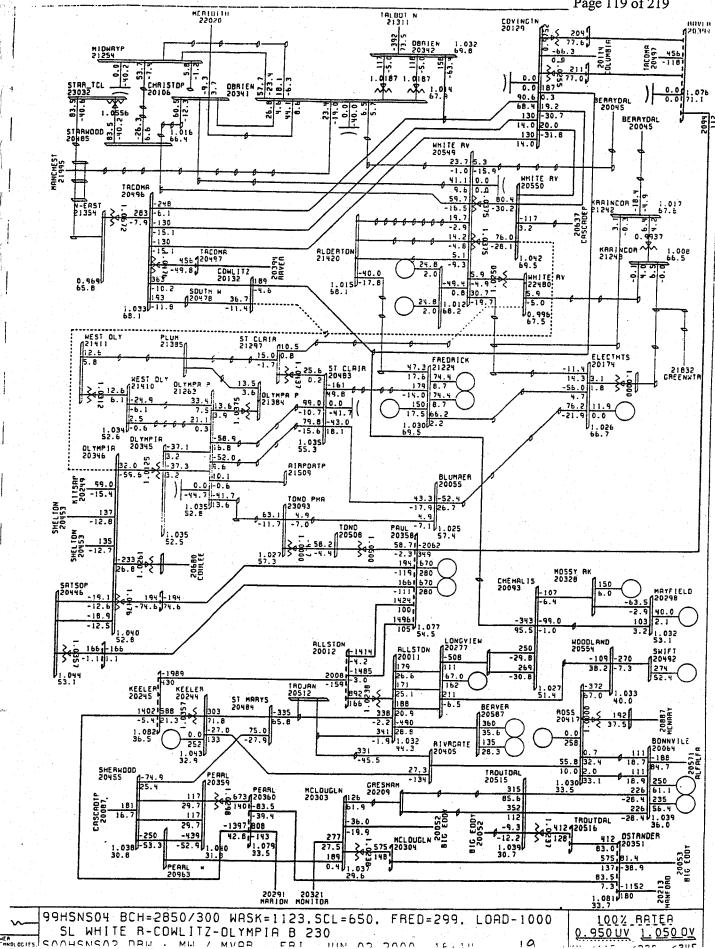


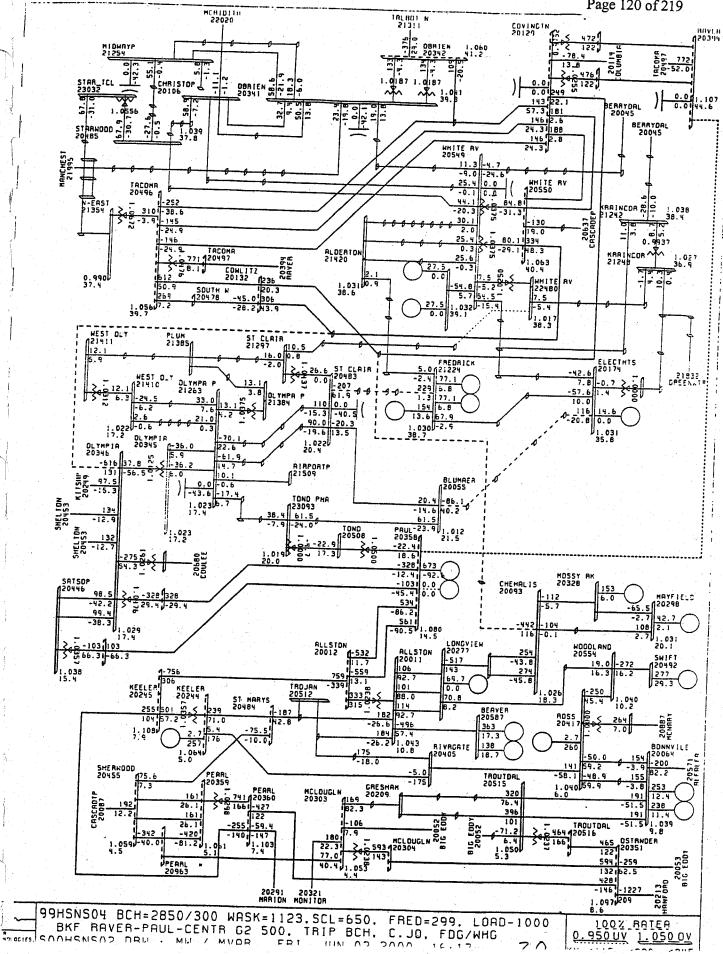


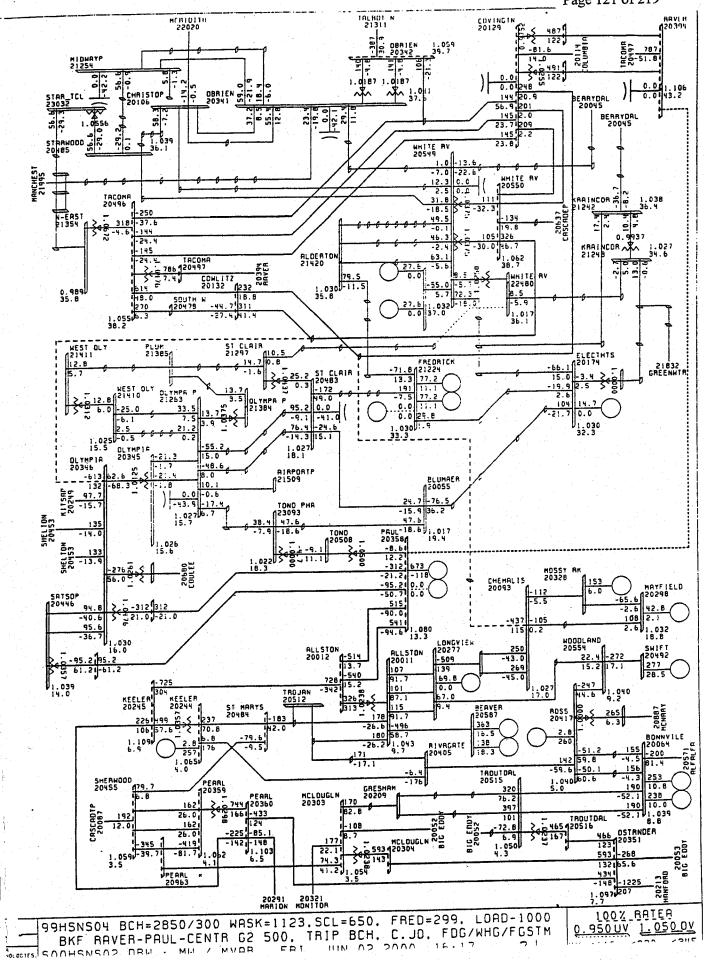
99HSNS04 BCH=2850/300 WASK=1123.SCL=650. LOAD-1000
BKF RAVER-PAUL-CENTR G2 500. TRIP BCH. C.JD. FDG/WHG

100%\_BATEA 0.950UV 1.050 OV

10







# FREDERICKSON 25 MW

Ex.			<u> </u>	(WA	G-4	1)
Page	e 1	22	of 21	9		

# SYSTEM IMPACT STUDY OASIS Reference No. 133622 25 MW GENERATION ADDITION TO FREDERICKSON 115 kV BUS

May 21, 2001 PSE Electric Transmission

#### INTRODUCTION

This study is in response to OASIS Reference No. 133622 and the System Impact Study Agreement executed by PSE's merchant function on April 24, 2001 requesting 25 MW of Firm Point-to-Point Transmission Service by Electricity Capital (E.C.) for proposed new generation located near PSE's 115 kV Frederickson Substation located in Pierce County, Washington. The generation would consist of several reciprocating engine powered generators, each producing approximately 1.9 MW. This study summarizes the results of analyses done to evaluate transmission requirements to integrate this proposed generation at or near Frederickson. This 25 MW proposed generation is in addition to the 149 MW (summer) existing PSE generation, and the planned 154 MW generation owned by MEGA.

### CONCLUSION

If 25 MW of generator is tapped to the Frederickson-Boeing Puyallup 115 kV line, then impacts to the existing transmission system are expected to be minimal. A requirement for this addition is that during conditions of high north to south flow on the Raver-Paul 500 kV line, the generation may need to be tripped automatically if an outage of the Raver-Paul 500 kV line were to occur. The only line requiring conductor temperature upgrade as a result of the 25 MW addition is the PSE Dieringer-Boeing Auburn 115 kV line. This assumes that the Electron Heights-Boeing Puyallup-Frederickson 115 kV line is upgraded for the MEGA project to 100C conductor temperature rating.

Also, a Remedial Action Scheme (RAS) should be employed to trip or ramp generation at MEGA and E.C. in the event that two of the three 115 kV lines to Frederickson go out-of-service, or for loss of the Raver-Paul 500 kV line at high Raver-Paul path flows. For redundancy, the RAS will use both overload monitoring relays on three lines out of Frederickson, and the Boeing Puyallup-Electron Heights line, and a trip signal from BPA in the event the Raver-Paul line is forced out of service. The cost estimate for transmission interconnection and facilities improvements is \$300,000 - \$500,000. E.C. will need to acquire electrical equipment including a generator step-up 115-13 kV transformer and a 115 kV breaker to interconnect with PSE Frederickson-Boeing Puyallup 115 kV line.

#### STUDY ASSUMPTIONS

The results of a prior study were used along with additional study work. The prior study is on PSE's OASIS site (oasis.puget.com), and it is attached as an appendix to this document. That work explored summer and winter seasons, with Northern Intertie flows in a north to south direction. The prior study covered a range of generation at Frederickson that included the existing generators at 149 MW, plus levels of 50, 100, 150, and 200 additional MW. The total generation addition including the proposed 25 MW in this study and MEGA's planned 154 MW, is between 150 and 200 MW additional generation at Frederickson. The totals become:

Table 1. Total Frederickson Generation Output

Generating facility	MW per facility	Total MW
Existing PSE CT's	149	149
Addition in prior study	50	199
4 4 4	100	249
4 4	150	299
66 66 64	200	349
MEGA	154	303
Electricity Capital	25	328

For the additional studies, only the heavy summer season was studied because the prior study had shown the summer had the most critical loading conditions. The through-flow conditions studied included both high Raver-Paul north to south loading, and high Northern Intertie south to north loading. The lines in the Raver-Paul path through Pierce County are:

Raver-Paul 500 kV line White River-Cowlitz-Olympia 230 kV line Covington-Cowlitz-Chehalis 230 kV line Frederickson-St. Clair 115 kV line Electron Heights-Blumaer 115 kV line White River-Fern Hill 57.5 kV line

The total MW output of the E.C. generators was modeled as 25 MW. Each generator consists of a natural gas reciprocating engine and generator producing approximately 1.9 MW. The generators are assumed to have capability to produce at least 0.9 power factor lagging (VARS supplied to PSE's system by E.C. generators), and 0.95 power factor leading, at full rated power. The generators are assumed to be operating in automatic voltage control mode according to the PSE Interconnection Standard.

The time frame was 2002 and 2003. The planned West Coast generators were modeled as in-service, generating 270 MW, and connected to the BPA South Tacoma Switch B 230 kV bus. This bus has three 230 kV lines connected to it from White River, Cowlitz, and BPA Olympia.

Reactive power margin and voltage stability were not determined because it is anticipated that addition of generation with full reactive capability at Frederickson will improve voltage regulation in the area. This can be confirmed with reactive margin studies. Transient stability was not confirmed, but it can be done when stability models and machine specific parameters are provided.

#### **OUTAGE ASSUMPTIONS**

Outages taken included single contingency (N-1) outages and common mode outages. The outage conditions used are to meet PSE's reliability criteria, the NERC Planning Standards and the WSCC Reliability Criteria. The single contingency outages are taken automatically, and include all lines in southern King, Pierce and Thurston Counties. The common mode outages are:

For south to north – Talbot 230 & 115 bus segments,
O'Brien 230 & 115 bus segments, Asbury 115 bus, Midway 115 bus
Christopher 115 bus, Starwood 115 bus, Berrydale 115 kV bus
Monroe 230 bus & breaker failures, Monroe 500 breaker failures
Snohomish 230 bus segments, Snoking 230 bus segments

Ex.	• ' '	_ (W.	AG-4)
Page	124 of	219	

Bothell 230 bus segments, SCL 230 and 115 kV double lines Maple Valley 230 bus segments, Covington 230 bus segments Echo Lake 500 breaker failures, Raver 500 breaker failures Raver-Paul-Centralia G2 500 BKF

For both south to north and north to south -

White River north 230 bus, south 230 bus, north115 bus, and south 115 bus Krain Corner 115 bus, Alderton 115 bus, Frederickson 115 bus Electron Heights 115 bus, Saint Clair 115bus, Blumaer 115 bus West Olympia 115 bus, Plum Street 57.5 bus PSE Olympia north 115 bus, and south 115 bus. Topo phase shifter

PSE Olympia north 115 bus, and south 115 bus, Tono phase shifter BPA Olympia east 230 bus, west 230 bus, and 115 bus

<u>For north to south</u> – governor load-flow is used, following WSCC guidelines.

Raver-Paul 500 line; Trip BC Hydro

Raver-Paul 500 line; Trip BC Hydro, MEGA, WC

Raver-Paul-Centralia G2 500 BKF; Trip BC Hydro

Raver-Paul-Centralia G2 500 BKF; Trip BC Hydro, MEGA, WC Raver-Paul-Centralia G2 500 BKF & Centralia G1; Trip BC Hydro

Raver-Paul-Centralia G2 500 BKF & Centralia G1; Trip BC Hydro, MEGA, WC

Paul-Allston 1&2 500 lines on common right-of-way; Trip BC Hydro

The formula for tripping BC Hydro generation is:

Trip generation = 1.3 x (Westside NI north-to-south – 1450 MW) MEGA stands for tripping the proposed MEGA generators at Frederickson. WC stands for tripping the proposed West Coast generator. BKF stands for breaker failure.

# **FINDINGS**

#### <u>Summer</u>

Loading on lines in the Raver-Paul path are closer to their ratings during the summer season than during other seasons because of transmission through-flow, and because the ratings are significantly lower in the summer than the winter on most lines. Flows on selected paths are given in Table 2 for the heavy summer case with high Northern Intertie flows in north to south.

Table 2. Line flows with Frederickson Total Generation

2002 Heavy Summer (N to S)	Frederickson total (includes MEGA & E.C.)					
	149 MW	303 MW	328 MW			
Element or Path	Fa	cility loading in M\	/A			
West Side NI, Ingledow-Custer 1&2	2850	2850	2850			
Raver-Paul 500	1867	1877	1880			
Olympia-Tacoma B 230	374	377	378			
Tacoma A-Centralia SS 230	321	325	326			
Frederickson-Boeing Puyallup 115	34	70	78			
Frederickson-Alderton 115	30	68	84			
Frederickson-St. Clair 115	120	158	162			

The results of the prior Frederickson study indicate that the Frederickson-St. Clair 115 kV line exceeds its maximum load capability for an outage of the Frederickson-Alderton 115 kV line if the combined generation at Frederickson is 349 MW. For the same outage at a combined generation of 328 MW, loading on the Frederickson-St. Clair 115 kV line is 97%.

Ex	(WAG-4)
Page 125 of 2	19

If the Frederickson-Boeing Puyallup-Electron Heights line were not upgraded, it would overload to 111% at the 328 MW generation level for an outage of the Frederickson-St. Clair 115 kV line. It would overload to 102% at the 303 MW level for the same outage. The double line loss of the Alderton-Frederickson and Frederickson-St. Clair 115 kV lines overloads the Frederickson-Boeing Puyallup-Electron Heights line to 250% of its existing rating at 303 MW generation level. This outage is an N-1 outage if one of the other two lines to Frederickson is already out for some reason. This line is being uprated, increasing the threshold levels of allowable generation during conditions such as line maintenance, unplanned outages, and the double line outage.

A RAS is being deployed with the MEGA project that will monitor line flows on the three 115 kV lines out of Frederickson Substation. When the flows on any one line are high enough to cause the computed conductor temperature rating of that line to be exceeded, then the RAS will trip or fast ramp MEGA generation to 0 MW. The RAS scheme trip signal should be sent to the E.C. generation also. The line monitoring point for the Frederickson-Boeing Puyallup-Electron Heights line should be at Boeing Puyallup Substation on the Boeing Puyallup-Electron Heights line, and not at the Frederickson bus. The RAS will also receive a trip signal for Raver-Paul 500 kV line outages, discussed later under Raver-Paul 500 kV Outage.

The results of heavy summer conditions with high south to north flows on the Northern Intertie is that the Dieringer-Boeing Auburn 115 kV line overloads and must be up-rated to avoid curtailing Frederickson generation during those conditions. The level of overload is 103%, and at a Westside Northern Intertie south-to-north export level of 1700 MW. The 795 kcmil Tern conductor in this line should be up-rated from 55C to a minimum 75C conductor rating. The White River-Dieringer 115 kV line has already been up-rated to 100C.

## Raver-Paul 500 kV Outage

The following discussion is based on prior studies and reconfirmed with current simulations. The most severe outage is the Raver-Paul 500 kV outage, and combination outages that include the Raver-Paul 500 kV line. The combination outages studied are a breaker failure at Paul that trips both the Raver-Paul line and the Centralia #2 generator, and the same breaker failure when the Centralia #1 generator is also out of service. Results are given in Table 3, and include the planned West Coast IPP connected to BPA South Tacoma Switch. The table shows when PSE lines will overload without tripping MEGA and E.C. generation, or an equivalent amount in MW at Frederickson.

BPA arms a RAS when there are high north to south flows on the Raver-Paul 500 kV line. The RAS sends trip signals to selected generators north of this line when the RAS detects that the line is tripped out of service. The generators that are armed are determined according to the flow level on the Raver-Paul line, and other factors, as described in BPA Dispatcher Standing Order (DSO) 307. In the power system simulations, for high flow levels on the Raver-Paul line, the generators that were tripped included Whitehorn, Fredonia, 1024 MW at Chief Joseph, and units in Canada following the formula:

MWtoTrip = 1.3(IngledowCusterflow - 1450MW)

The results indicate that for the Raver-Paul 500 kV line outage, assuming the West Coast generation is armed to trip, one PSE line is at 100% of its thermal rating. That line is the Frederickson-St. Clair 115 kV line. It will be protected by a thermal overload relay that will trip MEGA and E.C. generation if it does exceed its rating, and by a trip signal

from BPA that will trip MEGA and E.C. generation. No PSE lines overload after the MEGA and E.C. generation is tripped. The RAS is redundant in that either the overload relays can trip generation, or the BPA trip signal can trip generation. The RAS will normally be armed to trip generation on line overloads. It will be armed to trip generation from the BPA trip signal only when BPA and PSE determine that flows on the Raver-Paul line are sufficiently high. The trip signal from BPA will be received only for outages that include the Raver-Paul 500 kV line outage.

Table 3. Raver-Paul 500 kV Related Outages, 2850 MW Northern Intertie

Electht	s-Kapow	/115↓	Fredric	k-Tilcm	T 115 ↓	Dupon	t-Quarry	115↓	Tacom	a A-Cer	ıtr 230 ↓	
Frederickson	Yelm-L	ongmr T	115↓	Tilom 1	-Gravel	ly 115↓	Quarry	-St. Clai	r 115↓	Centr-	Chehalis	230 ↓
tot. gen 328 MW		Longm	r T-OlyV	'ail115↓	Gravel	ly-Dupoi	nt 115 ↓	Tacom	a B-Oly	230↓		
<u>Outages</u>			% line k	oading o	n above	lines, V	√ithout tr	ipping V	/estcoas	st, MEG	4 & E.C.	
Raver-Paul 500 k	V				102.1	99.8	97.9	96.4	95.4	95.4		
BKF Raver-Paul &	& Ctr2	104.4	106.4	104.5	112.1	109.8	107.9	106.4	105.3	104.9	105.6	101.8
BKF Raver-Paul & with Centralia 1 o		117.4	121.5	120.9	122.3	120.0	118.0	116.6	115.5	118.6	116.0	112.2
% line loading on above lines, With tripping Westcoast, but not MEGA & E.C.												
Raver-Paul 500 k	٧				100.3	98.0	96.1					
BKF Raver-Paul &	k Ctr2	101.8	103.4	101.3	110.2	107.9	106.0	104.5	103.4	96.2	100.9	97.1
BKF Raver-Paul & with Centralia 1 o		114.9	118.6	117.8	120.4	118.1	116.2	114.7	113.7	109.7	111.3	107.5
			% line	loading	on abov	e lines,	With trip	ping We	stcoast,	MEGA	& E.C.	
Raver-Paul 500 k	V											
BKF Raver-Paul &	L Ctr2									95.6	99.6	95.9
BKF Raver-Paul & with Centralia 1 o		102.9	104.7	102.9	98.3	95.9				109.1	110.0	106.7

For the breaker failure outage of both the Raver-Paul 500 kV line, and the Centralia generator unit #2, PSE lines overload. The Frederickson-St. Clair 115 kV line overloads the highest at 110% of its rating. After tripping MEGA and E.C. generation, there are no more PSE overloads remaining.

For the condition where the Centralia generator unit #1 is already out of service, and the breaker failure occurs, the simulation showed an overload of 120% on the Frederickson-St. Clair 115 kV line. After tripping MEGA and E.C. generation, there would be overloads remaining on the Electron Heights-Blumaer 115 kV line. The highest PSE overload then is 105%, that is half of the highest BPA overload at 110%. In this simulation, the Raver-Paul pre-outage loading is at 2080 MW, that is higher than allowed by the previous and current BPA DSO 307. In practice, BPA would reduce the flow on the Raver-Paul 500 kV line, following DSO 307 for Level 4, so that the overloads would not happen if the outage were to occur. By reducing the pre-outage flow down to a level studied for the other outages, about 1900 MW, there would be no overloads on PSE lines. Running the outage at this high level illustrates the need for a Raver-Paul flow threshold that results in significant overloads if violated.

The prior study results indicate that for light summer loads, using peak summer line ratings, PSE lines overload for the breaker failure outage of the Raver-Paul 500 kV line and Centralia generator unit #2, unless the MEGA and E.C. generation is tripped. The RAS scheme can protect PSE lines from overloading. During light summer load periods, line ratings will actually be higher than those used, because during off-peak periods air temperatures are lower, and sun radiation is lower. Tripping will not be needed during winter conditions because the Raver-Paul line loading is low.

Ex.			(V	VÄG	-4)
Page	12	27 o	f 219		

The White River-Fern Hill 57.5 kV line overloads with outages of the Raver-Paul line. A relay has been installed at White River to detect when the line is being overloaded and the relay will sent a signal to automatically trip the line breaker at White River. All the power system simulations were done with either the White River-Fern Hill line open, or with the relay modeled to open the line up if the flow level on the line is above its seasonal rating.

# **COSTS**

The transmission facility costs to install up to 25 MW of new generation that is tapped to the Frederickson-Boeing Puyallup 115 kV line are expected to include the following:

	Low Range	High Range
RAS to add E.C. generator tripping for line overloads, and for Raver-Paul trip signal	30,000	60,000
Capacity up-rate of Dieringer-Boeing Auburn 115 kV line	75,000	100,000
Frederickson – E.C. 115 kV line extension	140,000	210,000
Protection, controls, fiber-optics additions to Frederickson & Boeing Puyallup Substations	50,000	100,000
Totals	\$295,000	\$470,000

# **POWER FLOW DRAWINGS**

Schematic type power flow drawings of selected conditions are given in post-script files. The drawings provided do not include the thousands of unique combinations of conditions that could be shown. For each season, hundreds of outages were simulated for each level of proposed generation at Frederickson, without and with the proposed West Coast project. These drawings only include summer No Outage cases without and with the MEGA project and the E.C. project.

They are given in the following order:

File Name:	Condition	Season	Generatio in MW					
riie ivailie.	Condition	Season	PSE	MEGA	E.C.	West- coast		
02hsnB4c149.PS	No Outage	HS	149			270		
02hsnB4c303.PS	No Outage	HS	149	154		270		
02hsnB4c328.PS	No Outage	HS	149	154	25	270		

		Ex	(V	VAG-4)
		Page	128 of 219	
Appen	dix to	Elect Cap.o	doc	

# SYSTEM IMPACT STUDY OASIS Reference No. 17855 150 MW GENERATION ADDITION TO FREDERICKSON 115 kV BUS

September 29, 2000 PSE Electric Transmission

### INTRODUCTION

This study is in response to OASIS Reference No. 117855 and the System Impact Study Agreement executed by PSE's merchant function on May 17, 2000 requesting, among other things, 150 MW of Firm Point-to-Point Transmission Service for proposed new steam generation located at PSE's 115 kV Frederickson Substation located in Pierce County, Washington. This study summarizes the results of analyses done to develop reliable transmission alternatives that integrate the proposed generation at Frederickson. This report summarizes studies done to find threshold levels where new generation could be added without large impacts to the existing transmission system. The added generation would be a steam unit with possible sizes being 50, 100, or 150 MW (200 MW was included to explore sensitivities).

# **CONCLUSION**

If a new generator is installed at Frederickson Generating Station and connected to the existing 115 kV bus, and if the size is 150 MW or smaller, then impacts to the existing transmission system are expected to be minimal. A requirement for this addition is that during conditions of high north to south flow on the Raver-Paul 500 kV line, some generation at Frederickson may need to be tripped automatically if an outage of the Raver-Paul 500 kV line were to occur. The only line requiring conductor temperature upgrade is the Electron Heights-Boeing Puyallup-Frederickson 115 kV line. Also, at the highest generation level, a Remedial Action Scheme should be employed to trip or ramp generation at Frederickson in the event that two of the three 115 kV lines to Frederickson becomes out-of-service. An estimate of the cost for transmission interconnection facilities and improvements is \$800,000.

#### STUDY ASSUMPTIONS

Summer and winter seasons were studied, with a focus on high Raver-Paul loading and high north to south flows on lines going through Pierce County. Load sensitivity was performed for the summer season. The lines through Pierce County are:

Raver-Paul 500 kV line White River-Cowlitz-Olympia 230 kV line Covington-Cowlitz-Chehalis 230 kV line Frederickson-St. Clair 115 kV line Electron Heights-Blumaer 115 kV line White River-Fern Hill 57.5 kV line

The time frame was 2001 with the following improvements assumed to be completed:

Chief Joe-Monroe #4 line re-converted to 345 kV operation.

Bothell-Snoking #2 and Snoking-Maple Valley #2 230 kV lines energized.

Schultz-Raver #2 500 kV line rerouted from Raver to Echo Lake.

Bothell #2 and #3 230-115 kV transformers replaced with 300 MVA transformers.

	Ex	(WAG-4)		
	Page 129	of 219		
Appendix to	Elect Cap.do	C		

Reactive power margin and voltage stability was not determined, it is anticipated that addition of generation with full reactive capability at Frederickson will improve voltage regulation in the area. This can be confirmed with reactive margin studies. Transient stability was not confirmed, and would be done when stability models, and machine specific parameters are provided.

The proposed Westcoast generator was studied as a sensitivity, to understand the combined impacts of the Frederickson steam turbine generator and the Westcoast generator. The total MW output of the Westcoast generators was modeled as 270 MW.

## **OUTAGE ASSUMPTIONS**

Outages taken included single contingency (N-1) outages and common mode outages. The single contingency outages are taken automatically, and include all lines in southern King, Pierce and Thurston Counties. The common mode outages are:

White River north 230 bus, south 230 bus, north115 bus, and south 115 bus Krain Corner 115 bus, Alderton 115 bus, Frederickson 115 bus Electron Heights 115 bus, Saint Clair 115bus, Blumaer 115 bus West Olympia 115 bus, Plum Street 57.5 bus PSE Olympia north 115 bus, and south 115 bus, Tono phase shifter BPA Olympia east 230 bus, west 230 bus, and 115 bus

The following use governor load-flow following WSCC guidelines.

Raver-Paul 500 line; Trip BC Hydro

Raver-Paul 500 line; Trip BC Hydro, FGStm, WC

Raver-Paul-Centralia G2 500 BKF; Trip BC Hydro

Raver-Paul-Centralia G2 500 BKF; Trip BC Hydro, FGStm, WC

Raver-Paul-Centralia G2 500 BKF & Centralia G1; Trip BC Hydro

Raver-Paul-Centralia G2 500 BKF & Centralia G1; Trip BC Hydro, FGStm, WC

Paul-Allston 1&2 500 lines on common right-of-way; Trip BC Hydro

The formula for tripping BC Hydro generation is:

Trip generation = 1.3 x (Westside NI north-to-south – 1450 MW)
FGStm stands for tripping the proposed Frederickson steam turbine and gen.
WC stands for tripping the proposed Westcoast generator.
BKF stands for breaker failure.

#### **FINDINGS**

The transmission through-flow can be seen in Table 1. It shows line flows before outages are taken for heavy summer, lighter summer, and heavy winter. Line flows on the Raver-Paul 500 kV line, as an example are 1800 to 1900 MW in the summer, and decrease to 1200 MW in the winter. In these seasons, the West Side Northern Intertie (WSNI) is 2850 MW in the summer cases, and is 1450 MW in the winter cases. If the winter import OTC goes above 1450 MW, then transmission through-flow will increase in the winter. Load sensitivity that was performed for the summer season was to reduce the area load by 1000 MW, from 5758 to 4758 MW, an 18% reduction. The results indicated that for lines at or near overload, the overloads increased slightly as loads were scaled down by 1000 MW. This is a favorable result because as loads go down in the summer, ambient air temperatures also cool, as in night-time conditions, and line ratings go up.

		Ex	(WAG-4)
		Page 130	
endix to	o Fle	et Cap doc	

#### <u>Summer</u>

During the summer season loading on lines can be closer to line ratings than during other seasons because of transmission through-flow, and because the line ratings are significantly lower in the summer on lines having a lower conductor temperature rating.

The results of outage simulations are given in Table 2, for single contingency outages (N-1), and common mode outages, except that the Raver-Paul 500 kV outage results are given in Tables 3-6, and are discussed later. The outage results for other than Raver-Paul 500 kV show that line loadings remain within their ratings up to an addition of 150 MW of generation. An exception is the double line loss of the Alderton-Frederickson and Frederickson-St. Clair 115 kV lines. This outage is an N-1 outage if one of the other two lines to Frederickson is already out for some reason. The temperature rating of the Electron Heights-Boeing Puyallup-Frederickson 115 kV line should be raised to significantly increase the threshold levels at which generation can safely generate during conditions such as line maintenance, unplanned outages, and the double line outage. The 1272 Kcmil Narcissus conductor portions should be uprated to 75C conductor rating, and the 795 Kcmil Tern portions to 100C conductor rating.

# Raver-Paul 500 kV Outage

The most severe outage is the Raver-Paul 500 kV outage, and combination outages, that include the Raver-Paul 500 kV line. The combination outages studied are a breaker failure at Paul that trips both the Raver-Paul line and the Centralia #2 generator, and the same breaker failure when the Centralia #1 generator is also out of service. Results are given in Tables 3-6, and include summer heavy load, summer light load, without and with a proposed Westcoast IPP connected to BPA South Tacoma Switch. The tables show when PSE lines will overload without tripping the Frederickson steam generator, or an equivalent amount in MW at Frederickson.

BPA arms a RAS when there are high north to south flows on the Raver-Paul 500 kV line. The RAS sends trip signals to selected generators north of this line when the RAS detects that the line is tripped out of service. The generators that are armed are determined according to the flow level on the Raver-Paul line, and other factors, as described in BPA Dispatcher Standing Order (DSO) 307. In the power system simulations, for high flow levels on the Raver-Paul line, the generators that were tripped included Whitehorn, Fredonia, 1024 MW at Chief Joseph, and units in Canada following the formula:

MWtoTrip = 1.3(IngledowCusterflow - 1450MW)

The results indicate that for light summer loads [using peak summer line ratings], or for Frederickson steam generator sizes above 100 MW, PSE lines overload for the breaker failure outage of the Raver-Paul 500 kV line and Centralia generator unit #2, unless the Frederickson steam generator is tripped. If the Westcoast generator is installed at about 270 MW, and if it is tripped for the same outage, then the above holds true for Frederickson steam generator sizes above 50 MW. The Frederickson steam generator, or one of the combustion turbine generators may need to be tripped during summer load and temperature conditions if the Raver-Paul 500 kV line loading is high enough. Tripping will not be needed during winter conditions because the Raver-Paul line loading is low.

The Tables 3-6 show overloads for the breaker failure outage and when the other Centralia generator unit #1 is off line. The Raver-Paul pre-outage flow is above 2000 MW. In practice, BPA would reduce the flow on the Raver-Paul 500 kV line, following

Frederickson Ldoc

Ex	(WAG-4)
Page 131	of 219

Appendix to Elect Cap.doc

DSO 307 for Level 4, so that the overloads would not happen if the outage were to occur. But running the outage at this high level illustrates the need for a Raver-Paul flow threshold that results in significant overloads if violated.

The White River-Fern Hill 57.5 kV line overloads with outages of the Raver-Paul line. A relay is being installed at White River to detect when the line is being overloaded and the relay will sent a signal to automatically trip the line breaker at White River. All the power system simulations were done with either the White River-Fern Hill line open, or with the relay modeled to open the line up if the flow level on the line is above its seasonal rating.

### Winter

Some common mode outages do not achieve a solution for winter loading conditions. The Olympia 230 kV bus is divided between east and west segments with both 230-115 kV transformers on one bus segment, the east bus. Loss of the Olympia 230 west bus results in no solution.

#### **COSTS**

Transmission costs to install up to 150 MW of new generation at Frederickson are expected to include the following:

RAS for Frederickson generator tripping for Raver-Paul outage, and for loss of two lines

\$50,000

Breaker and line bay at Frederickson for generator, 115 kV

\$300,000

Conductor temperature upgrade of Electron Heights-Boeing Puyallup-Frederickson 115 kV line

\$400,000

# **POWER FLOW DRAWINGS**

Schematic type power flow drawings of selected conditions are given following the tables. The drawings provided are a few that represent the thousands of unique combinations of conditions that could be shown. For each season, hundreds of outages were simulated for each level of proposed steam generation at Frederickson, without and with the proposed Westcoast project. The drawings include summer No Outage cases without and with Frederickson steam generator at 150 MW, and without and with the proposed Westcoast project.

They are given in the following order:

Figure	Condition	Season	Frederick-	West-
			son Steam	coast
1_	No Outage	HS	0	0
2	No Outage	HS	150	0
3	No Outage	HS	0	270
4	No Outage	HS	150	270
5	No Outage	HW	0	0
6	No Outage	HW	150	0
7	No Outage	HW	0	270
8	No Outage	HW	150	270
9	BPA Olympia 115 kV Bus	HW	0	0
10	BPA Olympia 115 kV Bus	HW	150	0
11	Freder-SW 28 Tie & Freder-Tillicum Tap	HS	150	0
12	White River-Cowlitz-Olympia B 230 kV	HS	0	0
13	Bkf Raver-Paul & Centr G2	HS	0	0

Ex. \_\_\_\_(WAG-4) Page 132 of 219

# Appendix to Elect Cap.doc

14	White River-Cowlitz-Olympia B 230 kV	HS	150	0
15	Bkf Raver-Paul & Centr G2	HS	150	1 0
16	Bkf Raver-Paul & Centr G2, trip F.Steam	HS	150	0
17	White River-Cowlitz-Olympia B 230 kV	HS -1000	0	0
18	Bkf Raver-Paul & Centr G2	HS -1000	0	1 0
19	White River-Cowlitz-Olympia B 230 kV	HS -1000	150	1 0
20	Bkf Raver-Paul & Centr G2	HS -1000	150	1 0
21	Bkf Raver-Paul & Centr G2, trip F.Steam	HS -1000	150	1 0

# FREDONIA 110 MW

# System Impact Study for Fredonia 2-55 MW Combustion Turbines

Mt. Vernon, WA

PSE OASIS Reference No. 131212 May 31, 2001

Puget Sound Energy, Inc. Electric Transmission Department

# **Table of Contents**

	Page
Executive Summary	4
Section 1. Introduction	7
Section 2. Criteria and Study Assumptions	. 8
Section 3. Study Conditions	10
Section 4. Study Results	.11
Local Network Impacts	.11
Westside Northern Intertie Impacts	18
Section 5. Conclusions and Recommendations	.20
Appendix A Contingency Analysis Detailed Report, NI flow N>S 2001 Summer Base Case, NO Fredonia Generator	22
Appendix B - Contingency Analysis Detailed Report, NI flow N>S 2001 Summer Base Case, Fredonia Generator Added July-August, 2001	.31
Appendix C – Contingency Analysis Detailed Report, NI flow S>N 2001 Summer Base Case, Fredonia Generator Added July-August, 2001	.41
Appendix D – Contingency Analysis Detailed Report, NI flow N>S 2001 Summer Base Case, Fredonia Generator Added MPCC 50 MW Generator Added, September, 2001	.45
Appendix E – Contingency Analysis Detailed Report, NI flow N>S 2001 Fall Base Case, Fredonia Generator Added MPCC 50 MW Generator Added	56
Appendix F – Contingency Analysis Detailed Report, NI flow S>N 2001 Fall Base Case, Fredonia Generator Added MPCC 50 MW Generator Added	.62
Appendix G – Contingency Analysis Detailed Report, NI flow N>S 2001-02 Winter Base Case, Fredonia Generator Added	l.64

# MPCC 50 MW Generator Added

Appendix H	<ul> <li>Contingency Analysis Detailed Report, NI flow S&gt;N</li> <li>2001-02 Winter Base Case, Fredonia Generator Added68</li> <li>MPCC 50 MW Generator Added</li> </ul>
Appendix I-	Contingency Analysis Detailed Report, NI flow N>S 2001 Summer, Fredonia Generator Added
Appendix J -	FCITC Single Study (Intertie Study) NI flow N>S 2001 Summer Case, NO Fredonia Generator83
Appendix K	- FCITC Single Study (Intertie Study) NI flow N>S 2001 Summer Case, Fredonia Generator Added100
Appendix L -	FCITC Single Study (Intertie Study) NI flow S>N 2001 Summer Case, Fredonia Generator Added118
Appendix M	- FCITC Single Study (Intertie Study) 2001 Summer Case, Fredonia Generator Added120 Light Load Hour - Peak Load
Appendix N -	- FCITC Single Study (Intertie Study) NI flow S>N 2001-02 Winter Case, Fredonia Generator Added136 MPCC 50 MW Generator Added
Appendix O -	- Contingency Analysis Detailed Report, NI flow N>S 2001 Summer Base Case, Fredonia Generator Added138 July-August, 2001, Horseranch Substation circuit breaker Op
Appendix P –	FCITC Single Study (Intertie Study), NI flow N>S 2001 Summer Base Case, Fredonia Generator Added148 July-August, 2001, Horseranch Substation circuit breaker Op
Appendix Q -	Contingency Analysis Detailed Report, NI flow N>S 2006 Summer Base Case, NO Fredonia Generator165
Appendix R –	Contingency Analysis Detailed Report, NI flow N>S 2006 Summer Base Case, Fredonia Generator Added187
Appendix S –	FCITC Single Study (Intertie Study), NI flow N>S 2006 Summer Base Case, NO Fredonia Generator213
Appendix T -	FCITC Single Study (Intertie Study), NI flow N>S 2006 Summer Base Case, Fredonia Generator Added235

#### **Executive Summary**

On January 18, 2001, the merchant function of Puget Sound Energy submitted an OASIS request (OASIS Reference No. 131212 for long term Firm Point-to-Point Transmission Service (the "Requested Service") for the purpose of integrating 110 MW, 150 MW and 200 MW's of generation at the Fredonia Generating Substation in Mt. Vernon, Washington. By letter dated April 3, 2001, the Requested Service was revised and limited to 110 MW and the start date revised from June 1, 2001 to July 1, 2001. The term of the Requested Service is for 25 years. The expected date of commercial operation is July 1, 2001.

PSE determined that a System Impact Study (the "Study") would be required to evaluate the impact of the Requested Service on PSE's Transmission System. The purpose of the Study is to identify any system constraints and redispatch options, additional Direct Assignment Facilities or Network Upgrades required to provide the Requested Service. Power flow simulation studies were performed to insure that the Requested Service was accomplished in compliance with PSE, WSCC and NERC reliability criteria. The time involved in completing the Study was a function of a pre-existing OASIS request (No. 130752) for a 50 MW generator at March Point, which also required a System Impact Study, and the complexity of the Study for the Fredonia request, the latter covering a five-year period and incorporating, among other things, the proposed generation at March Point.

The base conditions used for the Study are the following:

a) Puget Sound area HLH (heavy load hour) loads beginning the summer of 2001 through the summer 2006;

b) all existing generation in Skagit and Whatcom Counties running;

c) known industrial loads adjusted to account for their on-site generation and/or displaced load

d) maximum accepted WSCC Path Rating #3 (Northwest-Canada) for the Westside Northern Intertie ("WSNI") north to south (i.e., B.C. to U.S.) power flow (2,850 MW from BC Hydro's Ingledow Substation to BPA's Custer Substation).

The constraints and proposed system upgrades for removing the constraints are as follows:

Constraint #1: The Sedro Woolley-Sedro NT (north tap) 230 kV transmission line.

**Discussion:** Failure of any of the following lines can cause the Sedro-Sedro NT 230 kV line to exceed its maximum thermal design limit of 100C conductor temperature: a) the Horseranch Substation's 230 kV power circuit breaker, b) several 230 kV power circuit breakers failures at Sedro Woolley Substation, c) single lines such as Monroe-Custer 500 kV, d) Sedro-HRTap-SCL Bothell 230 kV, and e) the double line outage of the Sedro-Hrtap-SCL Bothell and Bothell-Sammamish 230 kV.

Constraint Mitigation: Uprate the line to a 115C conductor temperature, or higher. This should produce a line rating of at least 442 MVA, summer emergency.

Ex		(	WA	G-4)
Page	137	of 219		

Constraint #2: The Texaco East Substation to March Point Substation 115 kV transmission line.

**Discussion:** Since 1993-94, when the original MPCC Phase I and later Phase II was added, a loss of the March Point-Texaco West 115 kV line or a line breaker failure at the March Point Substation south 115 kV bus would cause very high thermal overloads on the Texaco East-March Point 115 kV line. This condition needs to be corrected as it exists with or without the proposed Fredonia 110 MW generation addition (even after the existing two Fredonia CT's are moved to the 230 kV).

Constraint Mitigation: Uprate the Texaco East-March Point 115 kV, 55C line to a 100C conductor temperature rating. By connecting the two existing Fredonia CT's to the Sedro-March Point 230 kV line the Texaco East-March Point 115 kV overload decreases to the point where the line does not have to be reconductored (as recommended in the MPCC SIS).

Constraint #3: The March Point-Beaver Lake 115 kV line between Peth Corner Substation and Mt. Vernon Substation.

**Discussion:** Failure of any of the following Substation can cause sections of the March Point-Beaver Lake 115 kV line between Peth Corner and Mt. Vernon Substations to exceed their maximum thermal design limit of 55 C conductor temperature: a) the Sedro Woolley-Fredonia 230 kV line, b) Sedro-HRTap-SCL Bothell 230 kV line, c) the double line outage of the Sedro-Hrtap-SCL Bothell and Bothell-Sammamish 230kV lines, and d) several 230 kV power circuit breakers at Sedro Woolley Substation and March Point. The line section between Mt. Vernon Substation and Big Rock Substation can exceed 98% of its maximum thermal design limit of 55 C conductor temperature.

Constraint Mitigation: Uprate the March Point-Beaver Lake 115 kV line to at least a 65C conductor temperature rating between Peth Corner Substation and Mt. Vernon Substation. It would be prudent to include the line section from Mt. Vernon Substation to Big Rock Substation because many contingencies cause this line to carry loads over 90% of its thermal rating. It is generally understood that the line will probably be uprated to 100C.

# Constraint #4: WSNI and BPA's Transmission System

**Discussion:** The study results show that there could be a 1338 MW reduction to the WSNI (north to south) Operational Transfer Capability ("OTC") after the addition of the proposed 2-Fredonia 55 MW generators and moving the two existing Fredonia CT's to the Sedro-March Point 230 kV line. A new bottleneck (limiting element) appears to have been created with this project. The new bottleneck becomes the 0.18 mile long Sedro-Sedro NT 230 kV line which overloads due to a 230 kV power circuit breaker failure at the Horseranch Substation. This line also overloads for other outages (see Constraint #1, above).

Ex		(W	'AG-4)
Page	138 o		

The study results show that the WSNI could be decreased by only 424 MW's (instead of the 1338 MW's) if the 0.18 mile long Sedro-Sedro NT 230 kV, 1-795 kcmil ACSR, 100C line could be replaced by a larger diameter conductor. The bottleneck (after the Sedro-Sedro NT line is reconductored) would be the BPA Sedro NT-Murray 230 kV line, which happens to be the bottleneck in the system today for north to south WSNI power transfers.

Note: Depending on system conditions, the Study indicated that additional power could flow out of the PSE Sedro Woolley 230 kV bus into the Sedro NT bus after construction of the proposed project.

Constraint Mitigation: Install RAS (remedial action scheme) by adding line loss logic that will trip the existing two Fredonia CT's in the event of a Horseranch Substation 230 kV circuit breaker failure or loss of the Sedro-HRTap-SCL Bothell 230 kV line. Installing RAS can be made by adding Line Loss Logic to the Sedro-HRTap-SCL Bothell 230 kV line at Sedro Woolley Substation [PDN 3158 and PDN 734] which can then be used to successfully integrate the proposed new Fredonia generation.

The Study concluded that with the <u>existing</u> transmission system and committed transfers the Fredonia 110 MW Requested Service cannot be accomplished on a year round firm basis without interruptions. Local area network upgrades and resolution of the impacts on the WSNI and on BPA's transmission system are recommended.

Ex	(WAG-4)
Page	139 of 219

#### 1. Introduction

On January 18, 2001, PSE's merchant function submitted an OASIS request (Reference No. 131212) for 110 MW, 150 MW and 200 MW's (subsequently revised to a single request of 110 MW's) of long term Firm Point-to-Point Transmission Service from the existing PSE Fredonia generation site into PSE's transmission network, as a network resource, for the period June 1, 2001 (subsequently revised to July 1, 2001) through December 31, 2025, (the "Requested Service"). PSE determined that a System Impact Study (the "Study") would be required to evaluate the impact of the Requested Service on PSE's Transmission System. On or about January 25, 2001, the parties executed a System Impact Study Agreement. Power flow studies were performed to examine whether the Requested Service could be accommodated while remaining in compliance with PSE, WSCC and NERC reliability criteria.

Ex	-	٠.	_ (V	VAG-4)
Page	140	of	219	

#### 2. Study Criteria and Assumptions

The Study incorporated existing planning and operating criteria, standards and procedures in conformance with WSCC Reliability Criteria in order to determine necessary Transmission System reinforcements and re-dispatch requirements.

The Study included a number of individual power flow simulation studies (thermal) to determine the system capabilities with and without the 110 MW Fredonia generation. The power flow simulation studies were conducted with the following assumptions and goals:

#### **Assumptions**

- Assume the proposed Fredonia 2-55 MW generators will be running from July 1, 2001 through the summer 2006.
- Assume all existing generation in Whatcom and Skagit Counties is on line.
- Assume known customer-owned generation in Whatcom and Skagit Counties is on line.
- Assume the full WSCC accepted path rating for the Northwest-Canada Path #3 where up to 2,850 MW of power is flowing from BC Hydro's Ingledow Substation near Vancouver, B.C. toward BPA's Custer Substation near Ferndale, WA.
- Assume that the impacts and required network upgrades to the local area system and the WSCC Northwest-Canada Path #3 are brought about solely by the addition of the proposed 2-55 MW's of generation located at the Fredonia Generation site. This SIS does not determine the impacts and the required network upgrades for the loss of the Intalco load or generation additions at PSE's industrial customer facilities, for example.
- Assume all equipment is in service; then run contingency analysis to determine system impacts

#### **Goals**

- Identify PSE's transmission constraints in Skagit and Whatcom Counties and any network upgrades
- Identify any constraints on the Westside Northern Intertie ("WSNI").

### **Study Limitations**

Pursuant to PSE's Open Access Transmission Tariff ("OATT"), the Study is:

"An assessment by the Transmission Provider of (i) the adequacy of the
Transmission System to accommodate a request for either Firm Point-To-Point
Transmission Service or Network Integration Transmission Service and (ii)
whether any additional costs may be incurred in order to provide transmission
service."

Ex. \_\_\_\_\_(WAG-4) Page 141 of 219

"Transmission System" is defined in the OATT as: "The facilities owned, controlled or operated by the Transmission Provider that are used to provide transmission service under Part II and Part III of the Tariff."

However, PSE noted in the System Impact Study Agreement that it would extend the scope of its Study to determine if there are impacts to the WSNI capacity and neighboring systems resulting from adding the proposed Fredonia generation and the Study does that. BPA may not necessarily agree with PSE's analysis.

Lastly, much of the Intalco load has been displaced and there are a number of generation projects being added or proposed for addition by various parties in the Whatcom and Skagit county area, which could have a material impact on path ratings and transfer capabilities. The results of this Study are a snapshot in time and are based on the most current information and input assumptions available at the time the Study was conducted. Studies done at a later date will likely yield different conclusions.

Ex.		_(WAG-	4)
Page	142 of	219	

#### 3. Study Conditions

Several base cases were used in the study. The majority of the base cases were conducted using slightly modified versions of the BPA summer 2000, spring 2000 and winter 2000-01 cases. These were the base cases used by both BPA and PSE Operations Planning staff during 2000. The base case was modified to reflect completed upgrade projects and changes to the areas industrial loads and customer-owned generation. The area loads (except customer-owned substation loads, which were held constant) were grown 1.5% per year for two years to reflect annual load growth. These modifications to the 2000 base cases were necessary to fulfill the requirement of being able to have the two Fredonia 55 MW generators run through the first part of its requested time period (July 1, 2001 to July 1, 2002).

A 2006 heavy summer load base case was used to see what the potential system impacts of adding the 110 MW's of generation at the Fredonia generation site might be further out in time.

The study conditions used the summer season base case. The summer season is one of the most restrictive times of year for the transmission system, and is one of the times when the transmission system is highly stressed. This is when the equipment ratings (capabilities) are at their minimums, the WSNI is being maximized (power flows from Canada to the U.S.) and when the Puget Sound area loads, including loads in the area of the proposed Fredonia generation, are at their lowest.

Ex.			(WAG-4)
Page	143	of 21	9

#### 4. Study Results

#### **Findings**

Adding the 2-55 MW Fredonia CT's impacts both the local area PSE 115 kV and 230 kV transmission system and the bulk transmission main power grid, which is owned and operated by BPA.

#### **Local Network Impacts**

Two local area 115 kV lines can thermally overload resulting from the original (1993-94) MPCC Phase 1 and Phase 2 projects. Adding the 2-55 MW CT's at the Fredonia Generation site and moving the 2 existing Fredonia CT's to the Sedro-March Pt. 230 kV line decrease the amount of these line overloads (compared to today's system). Nevertheless, the lines remain overloaded and must be uprated to successfully run all of the generation located in west Skagit County.

The two line overloads without the proposed new 110 MW's of generation are:

- A. The 1.75 mile long Texaco East-March Point 115 kV line:
- B. The March Point Beaver Lake 115 kV line from Peth Corner Substation to the Hickox Susbstation Tap (7.1 miles) and continuing on from the Hickox Tap to the Mt. Vernon Substation (2.64 miles)

The new line overloads created by adding the proposed 2-55 MW Fredonia generators are:

- C. The 0.18 mile long Sedro Woolley-Sedro NT 230 kV line which taps the BPA Custer-Murray 230 kV line.
- D. The 38.7 mile long Sedro Woolley-HorseranchTap-SCL Bothell 230 kV line (Sedro-HRTap section)

# Discussion of Local Network Impacts

Note: The contingency numbers (shown below) match those in the summer base cases contained in the Appendix's at the end of the study.

# A. Texaco East - March Point 115 kV Line

This line consists of 1-1272 kcmil AAC rated at 55C conductor temperature. The Texaco East-March Point 115 kV line can overload today without the addition of the proposed 2-55 MW generators.

# Existing System (2001 loads) Without the 2-55 MW Generators

Contingency #1: Loss of the Texaco West-March Point 115 kV line.

Local Area Impact: Thermally overloads the Texaco East-March Point 115 kV line –

177.5% of its emergency rating.

Contingency #36: Breaker failure at Sedro Woolley 230 kV Bus which causes loss of the Sedro Woolley 230-115 kV transformer and the BPA Custer-SedroNT-Murray 230 kV line.

Local Area Impact Thermally overloads the Texaco East-March Point 115 kV line – 102.5% of its emergency rating.

Contingency #45: Line breaker failure on the March Point south 115 kV Bus. Local Area Impact: Thermally overloads the Texaco East-March Point 115 kV line – 157.8% of its emergency rating.

Contingency #376: Loss of the Sedro Woolley 230-115 kV transformer.

Local Area Impact: Thermally overloads the Texaco East-March Point 115 kV line – 100.4% of its emergency rating.

# Existing System With the 2-55 MW Generators

Contingency #1: Loss of the Texaco West-March Point 115 kV line Local Area Impact: Thermally overloads the Texaco East-March Point 115 kV line – 132.2% of its emergency rating.

Contingency #45: Line breaker failure on the March Point south 115 kV Bus Local Area Impact: Thermally overloads the Texaco East-March Point 115 kV line – 133.2% of its emergency rating.

# B. March Point - Beaver Lake 115 kV Line

These line sections consists of 1-795 kcmil ACSR rated at 55C conductor temperature. The March Point-Beaver Lake 115 kV line can overload today without the addition of the proposed 2-55 MW generators. Additional generation exacerbates the problem. Moreover, the addition of the 2-55 MW generators causes this line to overload for other contingencies that do not occur without the generators.

Contingency #5: Breaker failure at BPA's Custer 500 kV bus causes loss of the BCH Ingledow-Custer #1 500 kV line and the Custer-Monroe #1 500 kV line.

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

Without 2-55 MW After 2-55 MW
Generation Generation
March Pt-Beaver Lake 115 kV % of Line Emergency Rating
Line Section Name

Peth Corner-Hickox Tap, 7.1 mi. Hickox Tap-Mt. Vernon, 2.7 mi.

104.2% 98.1

Ex. \_\_\_\_(WAG-4) Page 145 of 219

Contingency #26: Single line loss of the BPA Custer-SedroNT-Murray 230 kV line. Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

Without 2-55 MW Generation

After 2-55 MW

March Pt-Beaver Lake 115 kV Line Section Name Generation

Generation

Generation

Keneration

Peth Corner-Hickox Tap, 7.1 mi. Hickox Tap-Mt. Vernon, 2.7 mi.

100.0% 93.9

Contingency #28: Breaker failure at BPA's Custer 230 kV Bus which causes loss of the BPA Custer-SedroNT-Murray 230 kV line and the Portal Way 230-115 kV transformer.

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

Without 2-55 MW Generation

After 2-55 MW

March Pt-Beaver Lake 115 kV Line Section Name % of Line Emergency Rating

Peth Corner-Hickox Tap, 7.1 mi. Hickox Tap-Mt. Vernon, 2.7 mi.

103.1% 97.0

Contingency #29: Breaker failure at BPA's Custer 230 kV Bus which causes loss of the BPA Custer-SedroNT-Murray 230 kV line and the Custer-Intalco #2 230 kV line.

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

Without 2-55 MW Generation

After 2-55 MW Generation

March Pt-Beaver Lake 115 kV Line Section Name % of Line Emergency Rating

Peth Corner-Hickox Tap, 7.1 mi. Hickox Tap-Mt. Vernon, 2.7 mi.

100.0% 93.9

Contingency #35: Breaker failure at Sedro Woolley 230 kV Bus which causes loss of the BPA Bellingham-Sedro Woolley 230 kV line and the Sedro-HRTap-SCL Bothell 230 kV line.

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

Without 2-55 MW

After 2-55 MW

March Pt-Beaver Lake 115 kV Line Section Name Generation

Generation

% of Line Emergency Rating

Peth Corner-Hickox Tap, 7.1 mi. Hickox Tap-Mt. Vernon, 2.7 mi.

106.4% 100.2

Contingency #36: Breaker failure at Sedro Woolley 230 kV Bus which causes loss of the Sedro Woolley 230-115 kV transformer and the BPA Custer-SedroNT-Murray 230 kV line.

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

March Pt-Beaver Lake 115 kV Line Section Name	Without 2-55 MW Generation % of Line Emergency Ratio		Generation	After 2-55 MW Generation ing	
Peth Corner-Hickox Tap, 7.1 mi. Hickox Tap-Mt. Vernon, 2.7 mi. Mt. Vernon-Big Rock, 2.7 mi.	106% 99.8		109.5% 103.4		
wit. Veriion-Big Rock, 2.7 mi.			93.0		

Contingency #37: Breaker failure at Sedro Woolley 230 kV Bus which causes loss of the Sedro Woolley-March Point 230 kV line and the BPA Custer-SedroNT-Murray 230 kV line.

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

March Pt-Beaver Lake 115 kV Line Section Name	Without 2-55 MW Generation % of Line Emergency R	After 2-55 MW Generation ating
Peth Corner-Hickox Tap, 7.1 mi.	103.1%	127,3%
Hickox Tap-Mt. Vernon, 2.7 mi.	96.9	121.2
Mt. Vernon-Big Rock, 2.7 mi.		110.8
Big Rock-Beaver Lake, 2.6 mi.		105.0
Beaver Lake-Beverly Park, 39 mi.		105.0

Contingency #38: Breaker failure at Sedro Woolley 230 kV Bus which causes loss of the Sedro Woolley-Fredonia 230 kV line and the BPA Custer-SedroNT-Murray 230 kV line.

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

March Pt-Beaver Lake 115 kV Line Section Name	Without 2-55 MW Generation % of Line Emergency	After 2-55 MW Generation Rating
Peth Corner-Hickox Tap, 7.1 mi. Hickox Tap-Mt. Vernon, 2.7 mi. Mt. Vernon-Big Rock, 2.7 mi.	103.1% 96.9	112.8% 106.6 96.2

Contingency #39: Breaker failure at Sedro Woolley 230 kV Bus which causes loss of the Sedro Woolley 230-115 kV transformer and the Sedro-Hranch-SCL Bothell 230 kV line. Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

March Pt-Beaver Lake 115 kV	Without 2-55 MW Generation % of Line Emergency R	After 2-55 MW Generation Rating
Line Section Name		ta di Santa da Santa Santa da Santa da Sa
Peth Corner-Hickox Tap, 7.1 mi.	114.1%	118.6%
Hickox Tap-Mt. Vernon, 2.7 mi.	107.9	112.5
Mt.Vernon-Big Rock, 2.7 mi.	97.4	102.0
Big Rock-Beaver Lake, 2.6 mi.		96.2

Contingency #46: Single line loss of the Sedro-Hranch-SCL Bothell 230 kV line - all 3-legs.

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

	Without 2- 55 MW Generation	After 2-55 MW Generation
March Pt-Beaver Lake 115 kV Line Section Name	% of Line Emergency R	ating
Peth Corner-Hickox Tap, 7.1 mi. Hickox Tap-Mt. Vernon, 2.7 mi. Mt.Vernon-Big Rock, 2.7 mi.	104.2% 98.1	111.0% 104.8 94.4

Contingency #47: Double circuit line loss of both the Sedro-Hranch-SCL Bothell 230 kV line and the SCL Bothell-Sammamish 230 kV line. Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

March Pt-Beaver Lake 115 kV Line Section Name	Without 2-55 MW Generation % of Line Emergency F	After 2-55 MW Generation Rating
Peth Corner-Hickox Tap, 7.1 mi. Hickox Tap-Mt. Vernon, 2.7 mi.	104.0% 98.0	110.9% 104.7
Mt.Vernon-Big Rock, 2.7 mi.		94.3

Contingency #48: Breaker failure causing the loss of the BPA Murray 230 kV bus. Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

Without 2-55 MW After 2-55 MW

March Pt-Beaver Lake 115 kV Generation

March Pt-Beaver Lake 115 kV % of Line Emergency Rating

Line Section Name

 Peth Corner-Hickox Tap, 7.1 mi.
 100.5%
 105.9%

 Hickox Tap-Mt. Vernon, 2.7 mi.
 94.4
 99.8

Contingency #50: Breaker failure (on SedroNT line) causing the loss of the BPA Murray 230 kV bus.

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

Without 2-55 MW
Generation

March Pt-Beaver Lake 115 kV
Line Section Name

Without 2-55 MW
Generation
Generation
% of Line Emergency Rating

Peth Corner-Hickox Tap, 7.1 mi.

Hickox Tap-Mt. Vernon, 2.7 mi.

101.1%
95.0

Contingency #51: Breaker failure at the PSE Horseranch 230 kV Substation.

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

Without 2-55 MW
Generation

March Pt-Beaver Lake 115 kV
Line Section Name

Without 2-55 MW
Generation
% of Line Emergency Rating

108.4%
Hickox Tap-Mt. Vernon, 2.7 mi.
108.4%
102.2
108.8

Contingency #2228: Loss of the BPA Custer-Monroe #1 500 kV line. Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

98.4

91.7

Mt. Vernon-Big Rock, 2.7 mi.

Without 2-55 MW
Generation
March Pt-Beaver Lake 115 kV
Generation
% of Line Emergency Rating

Peth Corner-Hickox Tap, 7.1 mi. (less than 90%) 105.0% Hickox Tap-Mt. Vernon, 2.7 mi. 98.8

Contingency #4920: Open the BPA Custer-SedroNT-Murray 230 kV line at Murray Substation.

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

Without 2-55 MW

After 2-55 MW

Generation

Generation

March Pt-Beaver Lake 115 kV Line Section Name % of Line Emergency Rating

Peth Corner-Hickox Tap, 7.1 mi.

(less than 90%)

104.8%

Hickox Tap-Mt. Vernon, 2.7 mi.

98.7

Contingency #5976: Open the Sedro-HRTap-SCL Bothell 230 kV line at Sedro Woolley

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

Without 2-55 MW

After 2-55 MW

Generation

Generation

March Pt-Beaver Lake 115 kV Line Section Name % of Line Emergency Rating

Peth Corner-Hickox Tap, 7.1 mi.

(less than 90%)

111.2%

Hickox Tap-Mt. Vernon, 2.7 mi. Mt. Vernon-Big Rock, 2.7 mi.

105.1 94.6

Contingency #5977: Loss of the Sedro-Fredonia 230 kV line.

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

Without 2-55 MW

After 2-55 MW

Generation

Generation

March Pt-Beaver Lake 115 kV

Line Section Name

% of Line Emergency Rating

Peth Corner-Hickox Tap, 7.1 mi. Hickox Tap-Mt. Vernon, 2.7 mi. Mt. Vernon-Big Rock, 2.7 mi. 114.6%

108.4 98.0

-J-- 337 - 11 --- C - 1 - 3777 - 200 1 37 7

#### C. Sedro Woolley-SedroNT 230 kV line

This 0.18-mile line consists of 1-795 kcmil ACSR rated at 100C conductor temperature.

Contingency #39: Breaker failure at Sedro Woolley 230 kV Bus which causes loss of the Sedro Woolley 230-115 kV transformer and the Sedro-Hranch-SCL Bothell 230 kV line. Local Area Impact: Thermally overloads the Sedro-SedroNT 230 kV line (105.9% of its emergency rating).

Contingency #46: Single line loss of the Sedro-Hranch-SCL Bothell 230 kV line – all 3-legs.

Ex.		(WAG-4	4)
Page	150 of	219	

Local Area Impact: Thermally overloads the Sedro-SedroNT 230 kV line (114.5% of its emergency rating).

Contingency #47: Double circuit line loss of both the Sedro-Hranch-SCL Bothell 230 kV line and the SCL Bothell-Sammamish 230 kV line.

Local Area Impact: Thermally overloads the Sedro-SedroNT 230 kV line (113.8% of its emergency rating).

Contingency #51: Breaker failure at the PSE Horseranch 230 kV Substation.

Local Area Impact: Thermally overloads the Sedro-SedroNT 230 kV line (119.0% of its emergency rating).

Contingency #5976: Open the Sedro-HRTap-SCL Bothell 230 kV line at Sedro Woolley Substation.

Local Area Impact: Thermally overloads the Sedro-SedroNT 230 kV line (115.1% of its emergency rating).

## D. Sedro Woollev-HorseranchTap-SCL Bothell 230 kV line (Sedro-HRTap section)

This 38.7 mile long line consists of 2-795 kcmil ACSR rated at 75C conductor temperature.

Contingency #48: Breaker failure causing the loss of the BPA Murray 230 kV bus.

<u>Local Area Impact:</u> Thermally overloads the Sedro-HRTap-SCL Bothell 230 kV line from Sedro to the Horseranch Tap (105.4% of its emergency rating).

Contingency #2228: Loss of the BPA Custer-Monroe #1 500 kV line. Local Area Impact: Thermally overloads the Sedro-HRTap-SCL Bothell 230 kV line from Sedro Woolley Substation to the Horseranch Tap (105.3% of its emergency rating).

Contingency #4920: Open the BPA Custer-SedroNT-Murray 230 kV line at Murray Substation.

Local Area Impact: Thermally overloads the Sedro-HRTap-SCL Bothell 230 kV line from Sedro Woolley Substation to the Horseranch Tap (105.6% of its emergency rating).

The effects of lower Puget Sound area loads (LLH, Light Load Hour) were also studied to see if the addition of the Fredonia generators would create additional problems or worsen the ones found above. No new line sections (not already identified in the HLH studies) were found and many of those identified with the heavier load level were reduced.

# Discussion of Non-PSE; Neighboring Systems; Main Grid Network Impacts

The power flow study results indicate impacts on BPA's 230 kV system. It appears that there are contingencies that will cause the BPA SedroNT-Murray 230 kV line to overload. Some of these contingencies do not cause line overloads today (without the Fredonia 2-55 MW generators).

Ex	(WAG-4)
Page	151 of 219

There are other contingencies that can cause the BPA line(s) to overload even in today's system, but overloads of this particular line increase with the addition of the Fredonia generators.

Today's limiting facility (i.e., constraint) that restricts WSNI OTC is the same line that will be forced to carry some of the additional power of the proposed Fredonia generator. If the WSNI path is to be used to protect the Sedro-SedroNT 230 kV line from overloading (so the Fredonia generation can run) the analysis in this Study indicates that the WSNI OTC would have to be restricted by 1338 MW's. If the Sedro-SedroNT 230 kV were reconductored with a higher capacity conductor, then the limiting element (restricting the intertie) would become the SedroNT-Murray 230 kV line. The study results show that the WSNI could be decreased by only 424 MW's (instead of the 1338 MW's) if the 0.18 mile long Sedro-Sedro NT 230 kV line could be uprated to a higher conductor temperature. A RAS could be installed with line loss logic on the Sedro-HRTap-SCL Bothell 230 kV line that would trip the two existing Fredonia CT's decreasing the power flow on the SedroNT-Murray 230 kV line. This would result in increasing the WSNI north to south OTC.

Negative impacts to the WSNI OTC during LLH (light load hour) generally appear to be lower for the same contingencies as at the HLH. However, the overload of the Sedro-Sedro NT 230 kV line seems like it can be worse and could limit the WSNI OTC even more than during HLH. Removing the bottleneck, which consists of uprating it to a higher conductor temperature, can eliminate this constraint.

Adding the Fredonia generators will increase the WSNI OTC when the power flow is moving from the U.S. to B.C. This effect (adding south-to-north OTC) appears to occur for most of the seasons (winter, spring/fall, and summer). The Portal Way-ARCO Central 115 kV line looks like it could become the limiting element for the summer south to north base case. This happens with or without the addition of the 2-55 MW Fredonia CT's.

#### 5. Conclusions and Recommendations

#### **Conclusions**

The Study indicates that with the existing transmission system and WSCC accepted path rating(s) for the WSNI (WSCC Path #3), the Requested Service cannot be accommodated. There are impacts to: (a) the local area transmission system, (b) the WSNI (joint ownership) and (c) BPA's transmission system. The local area facilities impacted involve power flows (resulting from contingencies) exceeding their thermal design limits. These facilities can probably be upgraded to higher capacities.

The non-PSE owned (BPA) facilities impacted: (a) depending on system conditions some of the Fredonia generators power could flow on BPA transmission system, and (b) power flows (resulting from contingencies) on BPA's SedroNT-Murray 230 kV line exceeding its design limit and thus limiting the WSNI (WSCC Path #3). The SedroNT-Murray 230 kV line may already be at BPA's maximum desired capacity rating. Adding the Fredonia generation will increase the capacity of the WSNI when the power is moving from the U.S. to B.C.

Higher Puget Sound area loads would appear to cause the line overloads shown from the power flow studies to become worse. This conclusion is based on the power flow comparison of heavier load base case results versus the lighter-load base case results.

All of the power studies assumed that all other lines were in service. System outages, such as for maintenance and construction, may cause the local network and the WSNI to become much more constrained, beyond what was found and presented in this study.

#### Recommendations

A. PSE Facilities (Local Area Network, Estimated to be valid through summer, 2002)

Complete the following upgrades.

Overloads	Proposed System Upgrade
Sedro-SedroNT 230 kV Line	Uprate 0.18 miles of 1-795 kcmil ACSR @ 100C to 115C conductor temperature, or higher
Texaco East-March Pt 115 kV	Upgrade the existing 1-1272 kcmil AAC, 55C to 100C, 1.7 mi.
Beaver Lake-March Pt 115 kV A) PethCrn-HickoxTap B) Hickox Tap-Mt. Vernon	Upgrade to 65C from 55C, 7.08 mi. Upgrade to 65C from 55C, 2.64 mi.
Sedro-HRTap 230 kV Line	Upgrade line to 80C or higher from 75C, 39 mi., OR Run back generation via Power Dispatcher control if upgrading the line is not feasible

Ex		(WAG-4	)
Page	153	of 219	•

# B. BPA Facilities (Main Grid; Neighboring Systems, Estimated to be valid through summer, 2002)

Install RAS (remedial action scheme) in Sedro Woolley Substation to add Line Loss Logic to the Sedro-HRTap-SCL Bothell 230 kV line to trip the existing 2-Fredonia CT's. It may be necessary to occasionally (summer) operate the Horseranch Substation 230 kV circuit breaker open until the RAS in installed. This may have contract implications, however.

# C. PSE Facilities (Local Area Network, Estimated to be valid through summer, 2006)

The only new local area impact found by adding the Fredonia generation to the summer 2006 base case was a 102.3% overload of the Sedro-Horseranch tap 230 kV line caused by a BPA Murray 230 kV breaker failure and subsequent loss of all the Murray 230 kV lines. This potential line overload can be removed by having the PSE Load Dispatchers reschedule generation, as necessary.

# D. BPA Facilities (Main Grid; Neighboring Systems, Estimated to be valid through summer, 2006)

The summer 2006 base case shows that the BPA Snohomish-Bothell #2 230 kV line (which currently connects to BPA Snoking Substation and not Bothell Substation) is loaded to 95% of its emergency summer rating before contingencies and no additional Fredonia generation. The Snohomish-Bothell #2 230 kV line loads to 97% of its emergency rating after the addition of the Fredonia generation, a 2% increase.

The line overloads after many contingencies even without the addition of the proposed Fredonia generation. The line needs to be uprated regardless of the decision whether to add generation at Fredonia.

#### APPENDIX A

#### Contingency Analysis Detailed Report

```
*** MUST 4.00 *** THU, APR 19 2001 7:15 ***
     01HSNS02BCH=2850/300WASK=1223,SCL=100,NO NEW FREDONIA(BASE)
     ALL WA/SK GEN ON, INDUSTRIAL LD ADJ., NO LINE UPRATES, NO MPCC
Subsys.File D:\Summer-2000\subni-us.sub
Monit.File D:\Summer-2000\monzonepsregion-Fredonia100MW-pti-VER5.mon
Contin.File D:\Summer-2000\NIandSINGLE-ALL-Fredonia100MW.con
Exclud.File D:\Summer-2000\PTI-EXCLUDE.EXC
                    Summer 2001 Without Fredonia and Without MPCC
 Detailed report on selected contingencies. Total 6866. Selected 38
Study transfer not defined
 ****** Contingency 3 BKFCUSMON2T1
 Branches with MW flow more than 90.0 % of nominal rating
** From bus ** ** To bus ** CKT InitFlow Rating IntLd% BaseFlow
21870 HICKOX T 115 22163 PETHCORN 115 1 -105.1 110.0 95.5
                                                              -92.6
20330 MURRAY 230 21282 SEDRO NT 230 1 -430.3
                                                 426.3 100.9 -355.0
 ****** Contingency
                       5 BKFINGCUS1M1
 Branches with MW flow more than 90.0 % of nominal rating
** From bus ** ** To bus ** CKT InitFlow Rating IntLd% BaseFlow
21870 HICKOX T 115 22057 MTVERNON 115 1 106.7
                                                110.0 97.0
21870 HICKOX T 115 22163 PETHCORN 115 1 -113.4
                                                110.0 103.1
                                                                -92.6
20330 MURRAY 230 21282 SEDRO NT 230 1
                                      -480.5
                                               426.3 112.7 -355.0
20449 SEDRO 230 23097 HRNCHTAP 230 1
                                       631.5
                                                 638.2 98.9
                                                                459.6
****** Contingency 22 BKRPWAYLYNN
```

Branches with MW flow more than 90.0 % of nominal rating From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21183 ARCO C	115 21268	PORTALWY	115	1 .	146.6	159.0	92.2	100.8
21239 KENDALL	115 21438	SUMAS CG	115	1	-101.9	46.0	221.5	-33.1
21239 KENDALL	115 22113	NUGENT	115	1	97.9	46.0	212.8	29.1

\*\*\*\*\*\* Contingency 24 BKRPWAY115S

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 21941 LABOUNTY 115 21541 BAKERVUE 115 1 125.9 129.1 97.5 77.3 22179 PLYMOUTH 115 21541 BAKERVUE 115 1 -111.1 110.0 101.0 -62.6 21239 KENDALL 115 21438 SUMAS CG 115 1 -43.5 46.0 94.5 -33.1

\*\*\*\*\*\* Contingency 25 BKRPWAYVISS

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd\* BaseFlow 21941 LABOUNTY 115 21541 BAKERVUE 115 1 125.0 129.1 96.8 77.3 22179 PLYMOUTH 115 21541 BAKERVUE 115 1 -110.2 110.0 100.2 -62.6 21239 KENDALL 115 21438 SUMAS CG 115 1 -43.1 46.0 93.8 -33.1

\*\*\*\*\*\* Contingency 28 BKFCUSMURPWY

## Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21870 HICKOX T 115 22057 MTVERNON 115 1 103.3 110.0 94.0 85.8

21870 HICKOX T 115 22163 PETHCORN 115 1 -110.1 110.0 100.1 -92.6

20449 SEDRO 230 23097 HRNCHTAP 230 1 590.2 638.2 92.5 459.6

\*\*\*\*\*\* Contingency 31 DCCUSMURSED

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

22097 NORLUM 115 21514 ALGER 115 1 -102.9 108.0 95.3 -40.7

20039 BELNGM P 115 21514 ALGER 115 1 106.5 108.0 98.6 44.3

20039 BELNGM P 115 22507 WOBURN 115 1 121.9 115.9 105.1 54.0

21963 LKLOUIST 115 22507 WOBURN 115 1 -115.3 115.9 99.5 -47.4

20448 SEDRO 115 21963 LKLOUIST 115 1 -112.3 108.0 104.0 -44.4

\*\*\*\*\*\* Contingency 35 BKFSEDBOTBHM

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 21870 HICKOX T 115 22057 MTVERNON 115 1 106.6 110.0 96.9 85.8 21870 HICKOX T 115 22163 PETHCORN 115 1 -113.3 110.0 103.0 -92.6 20330 MURRAY 230 21282 SEDRO NT 230 1 -487.8 426.3 114.4 -355.0 20467 SNOHOMSH 230 98766 SBTPTI&1 230 1 439.5 426.3 103.1 314.5

\*\*\*\*\*\* Contingency 36 BKFSEDTXCUSM

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 22057 MTVERNON 115 21563 BIGROCK 115 1 101.8 110.0 92.6 74.4 21870 HICKOX T 115 22057 MTVERNON 115 1 113.3 110.0 103.0 85.8 21870 HICKOX T 115 22163 PETHCORN 115 1 -120.0 110.0 109.1 -92.6 21250 MARCHPT 115 22150 PADILTAP 115 1 -143.4 143.0 100.3 -106.4 22150 PADILTAP 115 21439 TEXACO E 115 1 -147.1 143.0 102.9 -110.1

\*\*\*\*\*\* Contingency 37 BKFMPTTXCUSM

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 21870 HICKOX T 115 22057 MTVERNON 115 1 109.4 110.0 99.4 85.8 21870 HICKOX T 115 22163 PETHCORN 115 1 -116.1 110.0 105.6 -92.6

\*\*\*\*\*\* Contingency 39 BKFSEDTXHRBO

Branches with MW flow more than 90.0 % of nominal rating \*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 21529 ARLNGTON 115 20033 BEAVERLK 115 1 -105.6 110.0 96.0 -67.9 20033 BEAVERLK 115 21563 BIGROCK 115 1 -105.7 110.0 96.1 -68.0 22057 MTVERNON 115 21563 BIGROCK 115 1 112.1 110.0 101.9 74.4 21870 HICKOX T 115 22057 MTVERNON 115 1 123.6 110.0 112.3 21870 HICKOX T 115 22163 PETHCORN 115 1 -130.3 110.0 118.4 -92.6 21250 MARCHPT 115 22150 PADILTAP 115 1 -135.5 143.0 94.7 -106.4 20330 MURRAY 230 21282 SEDRO NT 230 1 -520.6 426.3 122.1 -355.0 20467 SNOHOMSH 230 98766 SBTPTI&1 230 1 447.7 426.3 105.0 314.5 22150 PADILTAP 115 21439 TEXACO E 115 1 -139.1 143.0 97.3 -110.1

\*\*\*\*\*\*\* Contingency 40 BKRSEDROW115

## From bus | \*\* \*\* To bus | \*\* CKT InitFlow | Rating IntLd% | BaseFlow |
20448 | SEDRO | 115 | 20026 | BAKER | SW | 115 | 1 | -119.2 | 98.0 | 121.7 | -60.1 |
21870 | HICKOX T | 115 | 22057 | MTVERNON | 115 | 1 | 101.3 | 110.0 | 92.1 | 85.8 |
21870 | HICKOX T | 115 | 22163 | PETHCORN | 115 | 1 | -108.0 | 110.0 | 98.2 | -92.6 |
21250 | MARCHPT | 115 | 22150 | PADILTAP | 115 | 1 | -141.1 | 143.0 | 98.7 | -106.4 |
22150 | PADILTAP | 115 | 21439 | TEXACO | E | 115 | 1 | -144.8 | 143.0 | 101.2 | -110.1

\*\*\*\*\*\* Contingency 42 BKRSEDROE115

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 20448 SEDRO 115 20026 BAKER SW 115 2 -119.2 98.0 121.7 -59.1 21250 MARCHPT 115 22150 PADILTAP 115 1 -129.8 143.0 90.8 -106.4 22150 PADILTAP 115 21439 TEXACO E 115 1 -133.5 143.0 93.4 -110.1

\*\*\*\*\*\*\* Contingency 45 BKRMARPTS115

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21870 HICKOX T 115 22163 PETHCORN 115 1 -101.7 110.0 92.5 -92.6

21250 MARCHPT 115 22150 PADILTAP 115 1 -219.8 143.0 153.7 -106.4

22150 PADILTAP 115 21439 TEXACO E 115 1 -223.5 143.0 156.3 -110.1

\*\*\*\*\*\* Contingency 46 SLSEDROHRBOT

Branches with MW flow more than 90.0 % of nominal rating \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow \*\* From bus 22057 MTVERNON 115 21563 BIGROCK 115 1 101.2 110.0 92.0 74.4 21870 HICKOX T 115 22057 MTVERNON 115 1 112.6 110.0 102.4 85.8 21870 HICKOX T 115 22163 PETHCORN 115 1 -119.3 110.0 108.5 20330 MURRAY 230 21282 SEDRO NT 230 1 -540.3 426.3 126.7 -355.0 230 99882 SEDPTI&1 230 1 396.0 20449 SEDRO 402.0 98.5 105.5 20467 SNOHOMSH 230 98766 SBTPTI&1 230 1 450.0 426.3 105.6

\*\*\*\*\*\* Contingency 47 DCBOTSAMSEDH

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 22057 MTVERNON 115 21563 BIGROCK 115 1 101.1 110.0 91.9 74.4 21870 HICKOX T 115 22057 MTVERNON 115 1 112.5 110.0 102.3 85.8

21870	HICKOX T	115	22163	PETHCORN	115	1		-119.2	110.0	108.4	-92.6
20330	MURRAY	230	21282	SEDRO NT	230	1		-535.8			
20449	SEDRO	230	99882	SEDPTI&1	230	1		393.4			105.5
20467	SNOHOMSH	230	98766	SBTPTI&1	230	1	-	399.5	426.3	93.7	314.5

\*\*\*\*\*\* Contingency 48 BUSMURRAY230

\*\*\*\*\*\* Contingency 51 BKFHRSUB

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21529 ARLNGTON 115 20033 BEAVERLK 115 1 -99.2 110.0 90.1 -67.9

20033 BEAVERLK 115 21563 BIGROCK 115 1 -99.3 110.0 90.2 -68.0

22057 MTVERNON 115 21563 BIGROCK 115 1 105.7 110.0 96.1 74.4

21870 HICKOX T 115 22057 MTVERNON 115 1 117.1 110.0 106.5 85.8

21870 HICKOX T 115 22163 PETHCORN 115 1 -123.8 110.0 112.6 -92.6

20330 MURRAY 230 21282 SEDRO NT 230 1 -576.4 426.3 135.2 -355.0

20449 SEDRO 230 99882 SEDPTI&1 230 1 414.7 402.0 103.2 105.5

\*\*\*\*\*\* Contingency 53 BKFMONTAP230

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21870 HICKOX T 115 22163 PETHCORN 115 1 -103.5 110.0 94.1 -92.6

20330 MURRAY 230 21282 SEDRO NT 230 1 -429.9 426.3 100.9 -355.0

\*\*\*\*\*\* Contingency 67 BKRBOT4230

Part of Contrasts

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 20467 SNOHOMSH 230 98766 SETPTI&1 230 1 481.5 426.3 113.0 314.5 20467 SNOHOMSH 230 9993 SNOSNO&1 230 1 343.5 364.1 94.3 263.4

\*\*\*\*\*\*\*\* Contingency 320 20011 ALLSTON 230 20012 ALLSTON 500 1

\*\*\*\*\*\*\* Contingency 498 21183 ARCO C 115 21525 ARCO N 115 1

## Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21183 ARCO C 115 21268 PORTALWY 115 1 160.9 159.0 101.2 100.8

\*\*\*\*\*\*\* Contingency 602 21534 AVON PMP 115 22494 WILSN TP 115 1

\*\*\*\*\*\*\* Contingency 644 20026 BAKER SW 115 20448 SEDRO 115 1

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

20448 SEDRO 115 20026 BAKER SW 115 2 -119.2 98.0 121.7 -59.1

\*\*\*\*\*\*\* Contingency 645 20026 BAKER SW 115 20448 SEDRO 115 2

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 20448 SEDRO 115 20026 BAKER SW 115 1 -119.2 98.0 121.7 -60.1

\*\*\*\*\*\*\* Contingency 1159 20065 BOTHELL 230 23097 HRNCHTAP 230 1

## Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

20467 SNOHOMSH 230 98766 SBTPTI&1 230 1 490.3 426.3 115.0 314.5

20467 SNOHOMSH 230 9993 SNOSNO&1 230 1 344.2 364.1 94.5 263.4

\*\*\*\*\*\*\*\* Contingency 1700 20647 CHEHALIS 115 20961 PE ELL 115 1

## Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

20678 COSMOPLS 115 20997 RAYMOND 115 1 58.6 55.8 105.1 41.2

\*\*\*\*\*\*\* Contingency 1705 20093 CHEHALIS 230 20647 CHEHALIS 115 1

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 20678 COSMOPLS 115 20997 RAYMOND 115 1 58.8 55.8 105.4 41.2

\*\*\*\*\*\*\* Contingency 2225 20137 CUSTER W 500 20323 MONROE 500 &2

 Branches with
 MW
 flow
 more than
 90.0 % of nominal rating

 \*\* From bus
 \*\* \*\* To bus
 \*\* CKT InitFlow
 Rating IntLd% BaseFlow

 21870 HICKOX T 115
 22057 MTVERNON 115
 1 100.5
 110.0
 91.4
 85.8

 21870 HICKOX T 115
 22163 PETHCORN 115
 1 -107.3
 110.0
 97.5
 -92.6

 20330 MURRAY
 230
 21282 SEDRO NT 230
 1 -443.6
 426.3
 104.0
 -355.0

 20449 SEDRO
 230
 23097 HRNCHTAP
 230
 1 580.9
 638.2
 91.0
 459.6

\*\*\*\*\*\*\* Contingency 2226 20137 CUSTER W 500 20323 MONROE 500 &1

 Branches with MW flow more than
 90.0 % of nominal rating

 \*\* From bus
 \*\* \*\*
 To bus
 \*\* CKT InitFlow
 Rating IntLd%
 BaseFlow

 20137 CUSTER W 500 23629 CUSMON&2 500 2 1870.3 2061.2 90.7 1028.6
 21870.3 2061.2 90.7 1028.6
 21870.3 110.0 97.7 85.8

 21870 HICKOX T 115 22163 PETHCORN 115 1 -114.2 110.0 103.8 -92.6
 20330 MURRAY 230 21282 SEDRO NT 230 1 -485.4 426.3 113.9 -355.0
 20449 SEDRO 230 23097 HRNCHTAP 230 1 638.2 638.2 100.0 459.6

\*\*\*\*\*\*\* Contingency 3614 20812 HOLCOMB 115 20961 PE ELL 115 1

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 20678 COSMOPLS 115 20997 RAYMOND 115 1 57.3 55.8 102.7 41.2

\*\*\*\*\*\*\* Contingency 4348 21249 LYNDEN 115 22272 SCHUETT 115 1

 Branches with
 MW
 flow
 more than
 90.0 % of nominal rating

 \*\*
 From bus
 \*\*
 \*\*
 To bus
 \*\*
 CKT InitFlow
 Rating IntLd% BaseFlow

 21239 KENDALL
 115 21438 SUMAS CG 115 1 -101.9
 46.0 221.5 -33.1

 21239 KENDALL
 115 22113 NUGENT 115 1 97.9 46.0 212.8 29.1

\*\*\*\*\*\*\* Contingency 4419 21250 MARCHPT 115 21440 TEX\_WEST 115 1

 Branches with MW flow more than
 90.0 % of nominal rating

 \*\* From bus
 \*\* \*\* To bus
 \*\* CRT InitFlow Rating IntLd% BaseFlow

 21250 MARCHPT
 115 22150 PADILTAP 115 1 -247.2 143.0 172.9 -106.4

 22150 PADILTAP 115 21439 TEXACO E 115 1 -250.9 143.0 175.4 -110.1

\*\*\*\*\*\*\*\* Contingency 4919 20330 MURRAY 230 21282 SEDRO NT 230 1

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow
21870 HICKOX T 115 22057 MTVERNON 115 1 106.4 110.0 96.7 85.8
21870 HICKOX T 115 22163 PETHCORN 115 1 -113.1 110.0 102.8 -92.6
20449 SEDRO 230 23097 HRNCHTAP 230 1 632.5 638.2 99.1 459.6

\*\*\*\*\*\*\* Contingency 5970 20448 SEDRO 115 20449 SEDRO 230 1

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 21870 HICKOX T 115 22057 MTVERNON 115 1 100.7 110.0 91.5 85.8 21870 HICKOX T 115 22163 PETHCORN 115 1 -107.4 110.0 97.6 -92.6 21250 MARCHPT 115 22150 PADILTAP 115 1 -140.1 143.0 98.0 -106.4 22150 PADILTAP 115 21439 TEXACO E 115 1 -143.7 143.0 100.5 -110.1

\*\*\*\*\*\*\* Contingency 5975 20449 SEDRO 230 23097 HRNCHTAP 230 1

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

22057 MTVERNON 115 21563 BIGROCK 115 1 101.4 110.0 92.2 74.4

21870 HICKOX T 115 22057 MTVERNON 115 1 112.9 110.0 102.6 85.8

21870 HICKOX T 115 22163 PETHCORN 115 1 -119.6 110.0 108.7 -92.6

20330 MURRAY 230 21282 SEDRO NT 230 1 -544.7 426.3 127.8 -355.0

20449 SEDRO 230 99882 SEDPTI&1 230 1 398.4 402.0 99.1 105.5

# \*\*\*\*\*\*\* Contingency 6311 21438 SUMAS CG 115 22272 SCHUETT 115 1

Branches with	MW	flow-	more than	n 90	0.0 % of n	ominal rat	ing	
** From bus	**	**	To bus	** CKT	InitFlow	Rating	IntLd%	BaseFlow
21595 BRITTON	115	22443	VANWYCK	115 1	-102.2	109.0		-23.5
21239 KENDALL	115	21438	SUMAS CG	115 1	-111.9	46.0	243.3	-33.1
21239 KENDALL						46.0	234.6	29.1
22443 VANWYCK	115	22113	NUGENT	115 1	-104.2	109.0	95.6	-25.4

\*\*\*\*\*\*\* Contingency 6447 21439 TEXACO E 115 22494 WILSN TP 115 1

Branches with M	W flow	more than 90.0 % of nominal rating
** From bus *	* **	To bus ** CKT InitFlow Rating IntLd% BaseFlow
21607 BURLIGTN 11	5 23004	RITA 115 1 172.2 143.0 120.4 40.1
20448 SEDRO 11	5 23004	RITA 115 1 -170.2 143.0 119.0 -38.1

# MARCH POINT 50 MW

System Impact Study for

MPCC 50 MW Combustion Turbine

At Texaco West Substation

Near Anacortes, WA

PSE OASIS Reference No. 130752 March 7, 2001

Puget Sound Energy, Inc.
Electric Transmission Department

# Table of Contents

	age
	3
Section 1. Introduction	6
Section 2. Criteria and Study Assumptions	7
Section 3. Study Conditions	9
Section 4. Study Results	.10
Local Network Impacts	.10
Westside Northern Intertie Impacts	
Section 5. Conclusions and Recommendations	.16
Appendix A – Contingency Analysis Detailed Report – Single Contingence 2002 Base Case, NO MPCC Generator	ies .17
Appendix B – Contingency Analysis Detailed Report – Single Contingenc 2002 Base Case, MPCC Generator Added	ies 19
Appendix C – Contingency Analysis Detailed Report – Common Mode Contingencies	
2002 Base Case, NO MPCC Generator	22
Appendix D – Contingency Analysis Detailed Report – Common Mode Contingencies	
2002 Base Case, MPCC Generator Added	26
Appendix E – FCITC Single Study (Intertie Study) 2002 Base Case, NO MPCC Generator	31
Appendix F – FCITC Single Study (Intertie Study) 2002 Base Case, MPCC Generator Added	33
Appendix G – Contingency Analysis Detailed Report – Single Contingency 2002 Base Case, MPCC Generator Added	ies .35

Ex. \_\_\_\_\_(WAG-4) Page 165 of 219

Appendix H - Contingency Analysis Detailed Report - Common Mode Contingencies 2002 Base Case, MPCC Generator Added......38 Light Load

Ex.		(WAG-4)
Page	166	of 219

#### **Executive Summary**

On December 27, 2000, March Point Cogeneration Company ("MPCC") submitted an OASIS request (OASIS Reference No. 130752) to Puget Sound Energy, Inc. ("PSE") for long term Firm Point-to-Point Transmission Service (the "Requested Service") from a proposed 50 MW generator located at the Texaco West substation near Anacortes, Washington to Bonneville Power Administration's ("BPA") Mid-Columbia bus. The term of the Requested Service is one year, from September 1, 2001 through September 1, 2002.

PSE determined that a System Impact Study (the "Study") would be required to evaluate the impact of the Requested Service on PSE's Transmission System. The purpose of the Study is to identify any system constraints and redispatch options, additional Direct Assignment Facilities or Network Upgrades required to provide the Requested Service. Power flow simulation studies were performed to ensure that the MPCC transmission request was accomplished in compliance with PSE, WSCC and NERC reliability criteria.

The base conditions used for the Study are the following:

a) PSE's native load requirements for the summer of 2002;

b) all existing generation in Skagit and Whatcom Counties running; and

c) maximum accepted WSCC Path Rating #3 (Northwest-Canada) for the Westside Northern Intertie ("WSNI") north to south (i.e., B.C. to U.S.) power flow (2,850 MW from BC Hydro's Ingledow Substation to BPA's Custer Substation).

The constraints and proposed system upgrades for removing the constraints are as follows:

Constraint #1: The Texaco West Substation to March Point Substation 115 kV transmission line.

**Discussion:** During summer heavy load hours (i.e. hours between 0700 – 2200), opening the Texaco East-March Point 115 kV line at Texaco East Substation causes the Texaco West-March Point 115 kV line to exceed its maximum thermal design limit of 100C conductor temperature.

Constraint Mitigation: Reconductor the Texaco West-March Point 115 kV line using 1-1590 kcmil ACSR, Lapwing with a 100C conductor temperature rating.

Note: Outages of this line (to reconductor it) must not interfere with PSE's obligations to run its owned and contracted generation.

Constraint #2: The Texaco East Substation to March Point Substation 115 kV transmission line.

Ex.	(V	VAG-4)
Page	167 of 219	

**Discussion:** Since 1993-94, when the original MPCC Phase I and later Phase II was added, a loss of the March Point-Texaco West 115 kV line or a line breaker failure at the March Point Substation south 115 kV bus would cause very high thermal overloads on the Texaco East-March Point 115 kV line. This condition needs to be corrected as it exists with or without the proposed MPCC 50 MW generation addition.

Constraint Mitigation: Reconductor the Texaco East-March Point 115 kV line using 1-1590 kcmil ACSR, Lapwing with a 100C conductor temperature rating.

Note: Outages of this line (to reconductor it) must not interfere with PSE's obligations to run its owned and contracted generation.

Constraint #3: The March Point-Beaver Lake 115 kV line between Peth Corner Substation and Mt. Vernon Substation.

**Discussion:** During summer HLH (heavy load hours between 0700 – 2200) a forced outage of the Sedro-Horseranch-SCL Bothell 230 kV line can cause sections of the March Point-Beaver Lake 115 kV line between Peth Corner and Mt. Vernon Substations to exceed their maximum thermal design limit of 55 C conductor temperature. Loss of the Sedro Woolley-Rita 115 kV line will overload this line during LLH (light load hours, 2300-0600).

Constraint Mitigation: Uprate the March Point-Beaver Lake 115 kV line to 65C conductor temperature rating between Peth Corner Substation and the Hickox Tap; and, uprate the line section from the Hickox Tap to Mt. Vernon Substation to 60C conductor temperature rating.

# Constraint #4: WSNI and BPA's Transmission System

**Discussion:** The study results show that there could be a 173 MW reduction to the WSNI (north to south) Operational Transfer Capability ("OTC") after the addition of the proposed MPCC 50 MW generator.

Note: In addition to the impact on the WSNI OTC, the Study indicated that an additional 17.1 MW of power will move through BPA's transmission system after the addition of the MPCC 50 MW generator. This is the difference in power flow through the PSE Sedro Woolley 230 kV (connecting to BPA's Custer-SedroNT-Murray 230 kV line) before and after the MPCC 50 MW generator integration. This condition occurs with all lines in service.

Constraint Mitigation: PSE recommends that MPCC contact BPA, perhaps via an OASIS request, to get additional information regarding impacts of the MPCC 50 MW generation on the WSNI and on BPA's transmission system.

Ex. (WAG-4) Page 168 of 219

The Study concluded that with the <u>existing</u> transmission system and committed transfers the MPCC Requested Service cannot be accomplished. Local area network upgrades and resolution of the impacts on the WSNI and on BPA's transmission system are recommended.

There are no Direct Assignment Facilities associated with this request for Transmission Service.

Ex			(W	AG-4)
Page	169	of	219	

#### 1. Introduction

On December 27, 2000, March Point Cogeneration Company ("MPCC") submitted an OASIS request (Reference No. 130752) for 50 MW of long term Firm Point-to-Point Transmission Service from March Point's West Substation to the Mid-Columbia bus for the period September 1, 2001 through September 1, 2002, (the "Requested Service"). PSE determined that a System Impact Study (the "Study") would be required to evaluate the impact of the Requested Service on PSE's Transmission System. On or about January 19, 2001, the parties executed a System Impact Study Agreement. Power flow studies were performed to examine whether the MPCC transmission request could be accommodated while remaining in compliance with PSE, WSCC and NERC reliability criteria.

Ex	(	WAG-4)
Page 170		

## 2. Study Criteria and Assumptions

The Study incorporated existing planning and operating criteria, standards and procedures in conformance with WSCC Reliability Criteria in order to determine necessary Transmission System reinforcements and re-dispatch requirements.

The Study included a number of individual power flow simulation studies (thermal) to determine the system capabilities with and without the 50 MW MPCC generator. The power flow simulation studies were conducted with the following assumptions and goals:

#### **Assumptions**

- Assume the proposed MPCC 50 MW generator will be running from September 1, 2001 through August 31, 2002.
- Assume all existing generation in Whatcom and Skagit Counties is on line.
- Assume the full WSCC accepted path rating for the Northwest-Canada Path #3
  where up to 2,850 MW of power is flowing from BC Hydro's Ingledow
  Substation near Vancouver, B.C. toward BPA's Custer Substation near Ferndale,
  WA.
- Assume all equipment is in service; then run contingency analysis to determine system impacts

#### Goals

- Identify PSE's transmission constraints in Skagit and Whatcom Counties and any network upgrades
- Identify any constraints on the Westside Northern Intertie ("WSNI").

#### **Study Limitations**

Pursuant to PSE's Open Access Transmission Tariff ("OATT"), the Study is:

"An assessment by the Transmission Provider of (i) the adequacy of the
Transmission System to accommodate a request for either Firm Point-ToPoint Transmission Service or Network Integration Transmission Service
and (ii) whether any additional costs may be incurred in order to provide
transmission service."

"Transmission System" is defined in the OATT as: "The facilities owned, controlled or operated by the Transmission Provider that are used to provide transmission service under Part II and Part III of the Tariff."

However, PSE noted in the System Impact Study Agreement that it would extend the scope of its Study to determine if there are impacts to the WSNI capacity and neighboring systems resulting from adding the proposed MPCC generation and the Study does that. BPA may not necessarily agree with PSE's analysis.

Ex. (WAG-4) Page 171 of 219

Lastly, there are a number of generation projects being added or proposed for addition by various parties in the Whatcom and Skagit county area, which could have a material impact on path ratings and transfer capabilities. The results of this Study are a snapshot in time and are based on the most current information and input assumptions available at the time the Study was conducted. Studies done at a later date will likely yield different conclusions.

#### 3. Study Conditions

The power flow studies were conducted using a slightly modified version of the BPA summer 2000, spring 2000 and winter 2000-01 cases. These were the base cases used by both BPA and PSE Operations Planning staff during 2000. The base case was modified to reflect completed upgrade projects and changes to the areas industrial loads. The area loads (except customer-owned substation loads, which were held constant) were grown 1.5% per year for two years to reflect annual load growth. These modifications to the 2000 base cases were necessary to fulfill the requirement of being able to have the MPCC 50 MW generator run through its entire requested time period (September 1, 2001 to September 1, 2002).

The study conditions used the summer season base case. The summer season is one of the most restrictive times of year for the transmission system, and is one of the times when the transmission system is highly stressed. This is when the equipment ratings (capabilities) are at their minimums, the WSNI is being maximized (power flows from Canada to the U.S.) and when the Puget Sound area loads, including loads in the area of the proposed MPCC generation, are at their lowest.

Ex.		<u> </u>	(W	ÅG-	4)
Page	173	of 2	<u> </u>		. •

#### 4. Study Results

**Findings** 

Adding the 50 MW of MPCC generation impacts both the local area PSE 115 kV transmission system and the bulk transmission main power grid which is owned and operated by BPA.

**Local Network Impacts** 

Two local area 115 kV lines can thermally overload resulting from the original (1993-94) MPCC Phase 1 and Phase 2 projects. Adding the 50 MW of generation at Texaco West Substation increases the amount of these line overloads and creates a new line overload condition.

The two line overloads without the proposed new 50 MW's of generation are:

- A. The 1.75 mile long Texaco East-March Point 115 kV line;
- B. The March Point Beaver Lake 115 kV line from Peth Corner Substation to the Hickox Susbstation Tap (7.1 miles) and continuing on from the Hickox Tap to the Mt. Vernon Substation (2.64 miles)

The new line overload created by adding the proposed 50 MW generator is:

C. The 1.14 mile long Texaco West-March Point 115 kV line.

#### **Discussion of Local Network Impacts**

### A. Texaco East - March Point 115 kV Line

This line consists of 1-1272 kcmil AAC rated at 55C conductor temperature. The Texaco East-March Point 115 kV line can overload today without the addition of the proposed MPCC 50 MW generator. Additional generation exacerbates the problem. (Contingency numbers shown below match those found in the Appendices.)

## Existing System (2002 loads) Without the MPCC 50 MW Generator

Contingency #1: Loss of the Texaco West-March Point 115 kV line. Local Area Impact: Thermally overloads the Texaco East-March Point 115 kV line – 177.5% of its emergency rating.

Contingency #36: Breaker failure at Sedro Woolley 230 kV Bus which causes loss of the Sedro Woolley 230-115 kV transformer and the BPA Custer-SedroNT-Murray 230 kV line.

Local Area Impact: Thermally overloads the Texaco East-March Point 115 kV line - 102.5% of its emergency rating.

Contingency #45: Line breaker failure on the March Point south 115 kV Bus. Local Area Impact: Thermally overloads the Texaco East-March Point 115 kV line – 157.8% of its emergency rating.

Contingency #376: Loss of the Sedro Woolley 230-115 kV transformer. Local Area Impact: Thermally overloads the Texaco East-March Point 115 kV line - 100.4% of its emergency rating.

## Existing System With the MPCC 50 MW Generator

Contingency #1: Loss of the Texaco West-March Point 115 kV line Local Area Impact: Thermally overloads the Texaco East-March Point 115 kV line - 201.8% of its emergency rating.

Contingency #36: Breaker failure at Sedro Woolley 230 kV Bus which causes loss of the Sedro Woolley 230-115 kV transformer and the BPA Custer-SedroNT-Murray 230 kV line.

Local Area Impact: Thermally overloads the Texaco East-March Point 115 kV line - 106.3% of its emergency rating.

Contingency #45: Line breaker failure on the March Point south 115 kV Bus Local Area Impact: Thermally overloads the Texaco East-March Point 115 kV line - 175.6% of its emergency rating.

Contingency #58: Loss of the Rita-Burlington 115 kV line section.

Local Area Impact: Thermally overloads the Texaco East-March Point 115 kV line - 103.6% of its emergency rating.

Contingency #376: Loss of the Sedro Woolley 230-115 kV transformer. Local Area Impact: Thermally overloads the Texaco East-March Point 115 kV line – 104.5% of its emergency rating.

Contingency #381: Loss of the Sedro Woolley-Rita 115 kV line section.

Local Area Impact: Thermally overloads the Texaco East-March Point 115 kV line – 102.7% of its emergency rating.

## B. March Point - Beaver Lake 115 kV Line

These line sections consists of 1-795 kcmil ACSR rated at 55C conductor temperature. The March Point-Beaver Lake 115 kV line can overload today without the addition of the proposed MPCC 50 MW generator. Additional generation exacerbates the problem. Moreover, the addition of the MPCC 50 MW generator causes this line to overload for other contingencies that do not occur without the 50 MW generator.

Contingency #39: Breaker failure at Sedro Woolley 230 kV Bus which causes loss of the Sedro Woolley 230-115 kV transformer and the Sedro-Hranch-SCL Bothell 230 kV line.

Local Area Impact: Thermally overloads the March Point-Beaver Lake  $115\ kV$  line.

March Pt-Beaver Lake 115 kV Line Section Name	Without MPCC 50 MW Generation % of Line Emergency Rat	After 50 MW Generation ing
Peth Corner-Hickox Tap, 7.1 mi.	114.1%	121%
Hickox Tap-Mt. Vernon, 2.7 mi.	107.9	114.7
Mt. Vernon-Big Rock, 2.7 mi.	97.4	104.2

Contingency #382: Open Sedro-HRTap-SCL Bothell line on the Sedro Woolley Substation end.

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

March Pt-Beaver Lake 115 kV Line Section Name	Generation % of Line Emerg	Generation
Peth Corner-Hickox Tap, 7.1 mi.	104.4%	110.4%
Hickox Tap-Mt. Vernon, 2.7 mi.	(below 90%)	104.2

Contingency #36: Breaker failure at Sedro Woolley 230 kV Bus which causes loss of the Sedro Woolley 230-115 kV transformer and the BPA Custer-SedroNT-Murray 230 kV line.

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

March Pt-Beaver Lake 115 kV Line Section Name	Without MPCC 50 MW After 50 MW Generation Generation % of Line Emergency Rating		
Peth Corner-Hickox Tap, 7.1 mi.	106%	112.9%	
Hickox Tap-Mt. Vernon, 2.7 mi.	99.8	106.6	

Contingency #37: Breaker failure at Sedro Woolley 230 kV Bus which causes loss of the Sedro Woolley-March Point 230 kV line and the BPA Custer-SedroNT-Murray 230 kV line.

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

· 50 MW ration			March Pt-Beaver Lake 115 kV	
			Line Section Name	
<b>1%</b>	112	103.1%	Peth Corner-Hickox Tap, 7.1 mi.	
	105.	96.9	Hickox Tap-Mt. Vernon, 2.7 mi.	
3		96.9		

Contingency #46: Single line loss of the Sedro-Hranch-SCL Bothell 230 kV line – all 3-legs.

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

	Generation	After 50 MW Generation	
March Pt-Beaver Lake 115 kV Line Section Name	% of Line Emergency Rating		
Peth Corner-Hickox Tap, 7.1 mi.	104.2%	110.2%	
Hickox Tap-Mt. Vernon, 2.7 mi.	98.1	103.9	

Contingency #47: Double circuit line loss of both the Sedro-Hranch-SCL Bothell 230 kV line and the SCL Bothell-Sammamish 230 kV line. Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

March Pt-Beaver Lake 115 kV Line Section Name	Without MPCC 50 MW After 50 MV Generation Generation % of Line Emergency Rating		
Peth Corner-Hickox Tap, 7.1 mi.	104.0%	110.0%	
Hickox Tap-Mt. Vernon, 2.7 mi.	98.0	103.8	

Contingency #48: Breaker failure causing the loss of the BPA Murray 230 kV bus.

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

Without MPCC 50 MW After 50 MW

March Pt-Beaver Lake 115 kV
Line Section Name

Generation
% of Line Emergency Rating

Peth Corner-Hickox Tap, 7.1 mi.
Hickox Tap-Mt. Vernon, 2.7 mi.

Generation
% of Line Emergency Rating
106.2%
106.2%
100.0

Contingency #51: Breaker failure at the PSE Horseranch 230 kV Substation. Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

March Pt-Beaver Lake 115 kV	Without MPCC 50 MW Generation % of Line Emergency Rat		After 50 MW Generation ting	
Line Section Name		erika di Mayara Perendahan		
Peth Corner-Hickox Tap, 7.1 mi.	108.4%		114.3%	
Hickox Tap-Mt. Vernon, 2.7 mi.	102.2		108.1	
Mt. Vernon-Big Rock, 2.7 mi.	91.7		97.5	

Contingency #259 and #260: Loss of the Sedro-March Pt 230 kV line or Mt. Point 230-115 kV transformer.

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

	Generation Generation		After 50 MW Generation	
March Pt-Beaver Lake 115 kV Line Section Name				
Peth Corner-Hickox Tap, 7.1 mi.	(less than 90%)		100.2%	

Contingency #376: Loss of the Sedro Woolley Substation 230-115 kV transformer.

Local Area Impact: Thermally overloads the March Point-Beaver Lake 115 kV line.

	Without MPCC 50 MW	After 50 MW	
	Generation	Generation	
March Pt-Beaver Lake 115 kV	% of Line Emergency Rating		
Line Section Name			
Peth Corner-Hickox Tap, 7.1 mi.	(less than 90%)	101.3%	

### C. Texaco West - March Point 115 kV line

This 1.14-mile line consists of 1-1272 kcmil AAC rated at 100C conductor temperature.

Contingency #266: Open the Texaco East Substation end of the Texaco East-March Point 115 kV line.

Local Area Impact: Thermally overloads the Texaco West-March Point 115 kV line - 108% of its emergency rating.

Contingency #43: Line breaker failure on the March Point East 115 kV Bus. Local Area Impact: Thermally overloads the Texaco West-March Point 115 kV line – 108% of its emergency rating.

The effects of less Puget Sound area loads (LLH, Light Load Hour) were also studied to see if the addition of the MPCC generator would create additional problems or worsen the ones found above. No new line sections (not already identified in the HLH studies) were found and many of those identified with the heavier load level were reduced. Loss of either the BPA Custer-Monroe #1 500 kV line or PSE Sedro-Rita 115 kV line could overload the March Point-Beaver Lake line between Peth Corner and the Hickox Tap (102.1% and 105.6%, respectively) which did not occur at the heavier load levels.

## Discussion of Non-PSE; Neighboring Systems; Main Grid Network Impacts

The power flow study results indicate impacts on BPA's 230 kV system. It appears that there are contingencies that will cause the BPA SedroNT-Murray 230 kV line to overload. Some of these contingencies do not cause line overloads today (without the MPCC generator). There are other contingencies that can cause the BPA line(s) to overload even in today's system, but overloads of this particular line increase with the addition of the MPCC generator.

Today's limiting facility (i.e., constraint) that restricts WSNI OTC is the same line that will be forced to carry some of the additional power of the proposed MPCC generator. If the WSNI path is to be used to protect the SedroNT-Murray 230 kV line from overloading (so the MPCC generation can run) the analysis in this Study indicates that the WSNI OTC would have to be restricted by 173.3 MW's. A power flow comparison (before and after the 50 MW generation addition) showed that 17.1 MW's of additional power flowed into BPA's transmission system over the Sedro Woolley-Sedro NT 230 kV line after the addition of the generator.

#### 5. Conclusions and Recommendations

#### **Conclusions**

The Study indicates that with the existing transmission system and WSCC accepted path rating(s) for the WSNI (WSCC Path #3), the Requested Service cannot be accommodated. There are impacts to: (a) the local area transmission system, (b) the WSNI (joint ownership) and (c) BPA's transmission system. The local area facilities impacted involve power flows (resulting from contingencies) exceeding their thermal design limits. These facilities (three transmission lines) can probably be upgraded to higher capacities.

The non-PSE owned (BPA) facilities impacted involve: (a) some of the MPCC generator power using BPA transmission system, and (b) power flows (resulting from contingencies) on BPA's SedroNT-Murray 230 kV line exceeding its design limit and thus limiting the WSNI (WSCC Path #3). The SedroNT-Murray 230 kV line may already be at BPA's maximum desired capacity rating.

Higher Puget Sound area loads would appear to cause the line overloads shown from the power flow studies to become worse. This conclusion is based on the power flow comparison of heavier load base case results versus the lighter-load base case results.

#### Recommendations

#### PSE Facilities (Local Area Network)

Complete the following upgrades.

#### **Overloads**

### Proposed System Upgrade

Texaco West-March Pt 115 kV	Reconductor with 1-1590 kcmil ACSR, Lapwing
	100C, 1.2 mi.
Texaco East-March Pt 115 kV	Reconductor with 1-1590 kcmil ACSR, Lapwing 100C, 1.7 mi.
Beaver Lake-March Pt 115 kV	
A) PethCrn-HickoxTap	Upgrade to 65C from 55C, 7.08 mi.
B) Hickox Tap-Mt. Vernon	Upgrade to 60C from 55C 2 64 mi

## BPA Facilities (Main Grid; Neighboring Systems)

- 1. Contact BPA's Transmission Business Line (TBL). PSE will have to be notified by BPA that MPCC has obtained BPA transmission capacity for use of BPA's system.
- Contact BPA's TBL. PSE will have to be notified by BPA that WSNI OTC has been restored.

## **APPENDIX A**

# Contingency Analysis Detailed Report

```
*** MUST 4.00 *** MON, MAR 05 2001 11:51 ***
      02HSNS02 BCH=2850/300 WASK=1123,SCL=100, INDUSTRIAL LD ADJ. .
      ALL WA/SK GEN ON - BASE CASE MPCC 50 MW GEN. Not Running
 Subsys.File D:\Summer-2000\subni-us.sub
 Monit.File D:\Summer-2000\monzonepsregion-MPCC.mon
 Contin.File D:\Summer-2000\contzonepsregion-fredonia.con
 Exclud. File none
  Detailed report on selected contingencies. Total 465. Selected
 Study transfer not defined
 ****** Contingency 1 SLTEXWMPT115
 Branches with MW flow more than 90.0 % of nominal rating
 ** From bus ** ** To bus ** CKT InitFlow Rating IntLd% BaseFlow
21250 MARCHPT 115 22150 PADILTAP 115 1 -250.2
                                               143.0 174.9 -107.1
22150 PADILTAP 115 21439 TEXACO E 115 1 -253.8 143.0 177.5 -110.8
 ******** Contingency 15 20026 BAKER SW 115 20448 SEDRO
 Branches with MW flow more than
                                  90.0 % of nominal rating
** From bus ** ** To bus ** CKT InitFlow Rating IntLd% BaseFlow
20448 SEDRO 115 20026 BAKER SW 115 2 -119.1
                                                 98.0 121.5 -59.0
 ******** Contingency 16 20026 BAKER SW 115 20448 SEDRO
 Branches with MW flow more than 90.0 % of nominal rating
** From bus ** ** To bus ** CKT InitFlow Rating IntLd% BaseFlow
20448 SEDRO 115 20026 BAKER SW 115 1 -119.1
                                                 98.0 121.5 -60.1
```

\*\*\*\*\*\*\* Contingency 256 21249 LYNDEN 115 22272 SCHUETT 115 1

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 21438 SUMAS CG 115 21239 KENDALL 115 1 101.7 46.0 221.2 32.6 22113 NUGENT 115 21239 KENDALL 115 1 -97.7 46.0 212.4 -28.6

\*\*\*\*\*\*\* Contingency 376 20448 SEDRO 115 20449 SEDRO 230 1

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 21870 HICKOX T 115 22163 PETHCORN 115 1 -104.5 110.0 95.0 -90.0 21250 MARCHPT 115 22150 PADILTAP 115 1 -140.0 143.0 97.9 -107.1 22150 PADILTAP 115 21439 TEXACO E 115 1 -143.6 143.0 100.4 -110.8

\*\*\*\*\*\*\* Contingency 382 20449 SEDRO 230 23097 HRNCHTAP 230 1

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow Plant HICKOX T 115 22057 MTVERNON 115 1 108.1 110.0 98.3 83.3 21870 HICKOX T 115 22163 PETHCORN 115 1 -114.9 110.0 104.4 -90.0 20330 MURRAY 230 21282 SEDRO NT 230 1 -506.8 426.3 118.9 -330.3

\*\*\*\*\*\*\* Contingency 409 21438 SUMAS CG 115 22272 SCHUETT 115 1

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 22443 VANWYCK 115 21595 BRITTON 115 1 102.1 109.0 93.7 22.9 21438 SUMAS CG 115 21239 KENDALL 115 1 111.9 46.0 243.3 32.6 22113 NUGENT 115 21239 KENDALL 115 1 -107.9 46.0 234.5 -28.6 22113 NUGENT 115 22443 VANWYCK 115 1 104.1 109.0 95.5 24.8

## **APPENDIX B**

# Contingency Analysis Detailed Report

```
*** MUST 4.00 *** MON, MAR 05 2001 11:15 ***
       02HSNS02 BCH=2850/300 WASK=1173,SCL=100, INDUSTRIAL LD ADJ.
       ALL WA/SK GEN ON - BASE CASE MPCC 50 MW GEN. IN SERVICE
  Subsys.File D:\Summer-2000\subni-us.sub
  Monit.File D:\Summer-2000\monzonepsregion-MPCC.mon
  Contin.File D:\Summer-2000\contzonepsregion-fredonia.con
  Exclud.File none
   Detailed report on selected contingencies. Total 465. Selected
  Study transfer not defined
  ****** Contingency 1 SLTEXWMPT115
  Branches with MW flow more than
                                   90.0 % of nominal rating
 ** From bus ** ** To bus ** CKT InitFlow Rating IntLd% BaseFlow
 21250 MARCHPT 115 22150 PADILTAP 115 1 -284.9
                                               143.0 199.2 -110.3
 22150 PADILTAP 115 21439 TEXACO E 115 1 -288.6
                                                143.0 201.8 -114.0
 ******* Contingency 15 20026 BAKER SW 115 20448 SEDRO
 Branches with MW flow more than
                                  90.0 % of nominal rating
 ** From bus ** **
                      To bus ** CKT InitFlow Rating IntLd% BaseFlow
20448 SEDRO 115 20026 BAKER SW 115 2 -119.1
                                              98.0 121.5
 ******* Contingency 16 20026 BAKER SW 115 20448 SEDRO 115 2
 Branches with MW flow more than 90.0 % of nominal rating
** From bus ** ** To bus ** CKT InitFlow Rating IntLd% BaseFlow
20448 SEDRO 115 20026 BAKER SW 115 1 -119.1 98.0 121.5 -60.1
******* Contingency 58 21607 BURLIGTN 115 23004 RITA 115 1
```

## Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CRT InitFlow Rating IntLd% BaseFlow

21870 HICKOX T 115 22163 PETHCORN 115 1 -101.2 110.0 92.0 -95.8

21250 MARCHPT 115 22150 PADILTAP 115 1 -144.5 143.0 101.1 -110.3

22150 PADILTAP 115 21439 TEXACO E 115 1 -148.2 143.0 103.6 -114.0

\*\*\*\*\*\*\*\* Contingency 256 21249 LYNDEN 115 22272 SCHUETT 115 1

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 21438 SUMAS CG 115 21239 KENDALL 115 1 101.7 46.0 221.2 32.3 22113 NUGENT 115 21239 KENDALL 115 1 -97.7 46.0 212.4 -28.3

\*\*\*\*\*\*\*\* Contingency 259 20290 MARCH PT 230 20449 SEDRO 230 1

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21870 HICKOX T 115 22057 MTVERNON 115 1 103.3 110.0 93.9 89.0

21870 HICKOX T 115 22163 PETHCORN 115 1 -110.2 110.0 100.1 -95.8

\*\*\*\*\*\*\* Contingency 260 20290 MARCH PT 230 21250 MARCHPT 115 1

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 21870 HICKOX T 115 22163 PETHCORN 115 1 -110.3 110.0 94.0 89.0 21870 HICKOX T 115 22163 PETHCORN 115 1 -110.3 110.0 100.2 -95.8

\*\*\*\*\*\*\* Contingency 266 21250 MARCHPT 115 22150 PADILTAP 115 1

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21250 MARCHPT 115 21440 TEX\_WEST 115 1 -286.0 264.9 108.0 -186.3

\*\*\*\*\*\*\* Contingency 376 20448 SEDRO 115 20449 SEDRO 230 1

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow
21870 HICKOX T 115 22057 MTVERNON 115 1 104.6 110.0 95.1 89.0

21870 HICKOX T 115 22163 PETHCORN 115 1 -111.5 110.0 101.3 -95.8 21250 MARCHPT 115 22150 PADILTAP 115 1 -145.7 143.0 101.9 -110.3 22150 PADILTAP 115 21439 TEXACO E 115 1 -149.4 143.0 104.5 -114.0

\*\*\*\*\*\*\* Contingency 381 20448 SEDRO 115 23004 RITA 115 1

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21870 HICKOX T 115 22163 PETHCORN 115 1 -101.0 110.0 91.8 -95.8'

21250 MARCHPT 115 22150 PADILTAP 115 1 -143.2 143.0 100.2 -110.3

22150 PADILTAP 115 21439 TEXACO E 115 1 -146.9 143.0 102.7 -114.0

\*\*\*\*\*\*\* Contingency 382 20449 SEDRO 230 23097 HRNCHTAP 230 1

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21563 BIGROCK 115 22057 MTVERNON 115 1 -103.0 110.0 93.6 -77.3

21870 HICKOX T 115 22163 PETHCORN 115 1 114.6 110.0 104.2 89.0

21870 HICKOX T 115 22163 PETHCORN 115 1 -121.5 110.0 110.4 -95.8

20330 MURRAY 230 21282 SEDRO NT 230 1 -521.5 426.3 122.3 -339.5

\*\*\*\*\*\*\* Contingency 409 21438 SUMAS CG 115 22272 SCHUETT 115 1

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

22443 VANWYCK 115 21595 ERITTON 115 1 102.2 109.0 93.7 22.6

21438 SUMAS CG 115 21239 KENDALL 115 1 111.9 46.0 243.3 32.3

22113 NUGENT 115 21239 KENDALL 115 1 -107.9 46.0 234.6 -28.3

22113 NUGENT 115 22443 VANWYCK 115 1 104.1 109.0 95.5 24.5

## **APPENDIX C**

# Contingency Analysis Detailed Report

```
*** MUST 4.00 *** MON, MAR 05 2001 15:03 ***

02HSNS02 BCH=2850/300 WASK=1173,SCL=100, INDUSTRIAL LD ADJ.

ALL WA/SK GEN ON - BASE CASE MPCC 50 MW GEN. Not Running

Subsys.File D:\Summer-2000\subni-us.sub

Monit.File D:\Summer-2000\monzonepsregion-MPCC.mon

Contin.File D:\Summer-2000\NI-ALL.con

Exclud.File none
```

Detailed report on selected contingencies. Total 77. Selected 13

Study transfer not defined

\*\*\*\*\*\* Contingency 5 BKFINGCUS1M1

Branches with MW	flow more than	n 90.0% of non	inal rating
** From bus **	** To bus	** CVM T-1-5	Rating IntLd% BaseFlow
21870 HICKOX T 115	22057 MTVERNON	115 1 100 =	110.0 93.2 83.3
21870 HICKOX T 115 20330 MURRAY 230			110.0 99.3 -90.0
***	21282 SEDRO NT		426.3 104.6 -330.3
20449 SEDRO 230	23097 HRNCHTAP	230 1 579.6	638.2 90.8 422.7

\*\*\*\*\*\* Contingency 22 BKRPWAYLYNN

```
## From bus ** ** To bus ** CKT InitFlow Rating IntLd% BaseFlow

21438 SUMAS CG 115 21239 KENDALL 115 1 101.7 46.0 221.2 32.6

22113 NUGENT 115 21239 KENDALL 115 1 -97.7 46.0 212.4 -28.6
```

\*\*\*\*\*\* Contingency 24 BKRPWAY115s

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21541 BAKERVUE 115 21941 LABOUNTY 115 1 -129.5 129.1 100.3 -77.2

21541	BAKERVUE	115	22179	Df VMOrimer	·					
20030	PET NOV D		22275	PLIMOUTH	TT2	T	114.5	110.0	104.1	62.2
20039	DELINGM P	115	22179	PLYMOUTH	115	1	-101 6	110 0	00.0	
21438	SUMAS CG	115	21230	VENTO S T T		_		110.0	92.3	-49.2
			21233	KENDALL	115	1	43.8	46.0	95.3	32.6

\*\*\*\*\*\* Contingency 25 BKRPWAYVISS

Branches with My	/ flow	more than	90	).0 % of no	minal rat	ing	
** From bus **	**	To bus	** CKU	InitFlow		-	BaseFlow
21541 BAKERVUE 115	21941	LABOUNTY	115 1	-128.6			-77.2
21541 BAKERVUE 115	22179	PLYMOUTH :	115 1	113.7	110.0		
20039 BELNGM P 115	22179	PLYMOUTH :	115 1	-100.7		91.6	
21438 SUMAS CG 115	21239	KENDALL 1	L15 1	43.5		94.5	32.6

\*\*\*\*\*\*\* Contingency 35 BKFSEDBOTBHM

Branches with M	flow	more than 90.0 % of nominal	
** From bus **		To have the second real rating	
21870 HICKOX T 115		MULTERNOV 145 6	
21870 НІСКОХ Т 115	22163	DEFECTION 33.2	83.3
20330 MURRAY 230	21202	110.0 99.3	-90.0
230	41464	SEDRO NT 230 1 -455.5 426.3 106.9	-330.3

\*\*\*\*\*\* Contingency 36 BKFSEDTXCUSM

```
Branches with MW flow more than 90.0 % of nominal rating

** From bus ** ** To bus ** CKT InitFlow Rating IntLd% BaseFlow
21870 HICKOX T 115 22057 MTVERNON 115 1 109.8 110.0 99.8 83.3

21870 HICKOX T 115 22163 PETHCORN 115 1 -116.6 110.0 106.0 -90.0

21250 MARCHPT 115 22150 PADILTAP 115 1 -142.8 143.0 99.9 -107.1

22150 PADILTAP 115 21439 TEXACO E 115 1 -146.5 143.0 102.5 -110.8
```

\*\*\*\*\*\*\* Contingency 37 BKFMPTTXCUSM

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow Place Process Perfection 115 1 106.6 110.0 96.9 83.3 21870 HICKOX T 115 22163 PETHCORN 115 1 -113.4 110.0 103.1 -90.0

\*\*\*\*\*\* Contingency 39 BKFSEDTXHRBO

	ches with				n '	9	0.0 % of no	minal rat	ing	
**	From bus	**	**	To bus	**	CKT	InitFlow	Rating	IntLd%	BaseFlow
21529	ARLNGTON	115	20033	BEAVERLK	115	1	-100.5		91.4	
20033	BEAVERLK	115	21563	BIGROCK	115	1	-100.7		91.5	
	BIGROCK						-107.1	110.0	97.4	-71.6
	HICKOX T						118.7	110.0	107.9	83.3
	HICKOX T						-125.5	110.0	114.1	-90.0
	MARCHPT						-135.8	143.0	95.0	-107.1
	MURRAY						-483.4	426.3	113.4	-330.3
22150	PADILTAP	115	21439	TEXACO E	115	1	-139.5	143.0	97.6	-110.8

\*\*\*\*\*\* Contingency 45 BKRMARPTS115

Branches with	MW	flow	more than	9(	0.0 % of nom	inal rat	ina	
** From bus	**	**	To bus *	* CKT	InitFlow		-	BaseFlow
21870 HICKOX T								-90.0
21250 MARCHPT					-222.0			-107.1
22150 PADILTAP	115	21439	TEXACO E 1	15 1	-225.6			-110.8

\*\*\*\*\*\*\* Contingency 46 SLSEDROHRBOT

```
## From bus ** ** To bus ** CKT InitFlow Rating IntLd% BaseFlow Place Pl
```

\*\*\*\*\*\* Contingency 47 DCBOTSAMSEDH

```
## From bus ** ** To bus ** CKT InitFlow Rating IntLd% BaseFlow Prom bus 115 22057 MTVERNON 115 1 107.7 110.0 97.9 83.3 21870 HICKOX T 115 22163 PETHCORN 115 1 -114.4 110.0 104.0 -90.0 20330 MURRAY 230 21282 SEDRO NT 230 1 -496.8 426.3 116.5 -330.3
```

\*\*\*\*\*\* Contingency 48 BUSMURRAY230

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21870 HICKOX T 115 22057 MTVERNON 115 1 103.8 110.0 94.4 83.3

21870 HICKOX T 115 22163 PETHCORN 115 1 -110.5 110.0 100.5 -90.0

Ex. (WAG-4) Page 188 of 219

20449 SEDRO 230 23097 HRNCHTAP 230 1 582.7 638.2 91.3 422.7

\*\*\*\*\*\* Contingency 51 BKFHRSUB

Branches with	MW	flow	more than					
** From bus	, <b>*</b> *	**	To bus	** CKT	InitFlow	Rating	IntLd%	BaseFlow
21563 BIGROCK					-100.8			-71.6
21870 HICKOX T	115	22057	MIVERNON	115 1	112.5	110.0	102.2	83.3
21870 НІСКОХ Т	115	22163	PETHCORN	115 1	-119.2	110.0	108.4	-90.0
20330 MURRAY	230	21282	SEDRO NT	230 1	-540.3	426.3	126.8	-330.3

#### APPENDIX D

## Contingency Analysis Detailed Report

```
*** MUST 4.00 *** MON, MAR 05 2001 15:09 ***
     02HSNS02 BCH=2850/300 WASK=1173,SCL=100, INDUSTRIAL LD ADJ.
     ALL WA/SK GEN ON - BASE CASE MPCC 50 MW GEN. IN SERVICE
 Subsys.File D:\Summer-2000\subni-us.sub
Monit.File D:\Summer-2000\monzonepsregion-MPCC.mon
 Contin.File D:\Summer-2000\NI-ALL.con
 Exclud. File none
 Detailed report on selected contingencies. Total 77. Selected 18
Study transfer not defined
 ****** Contingency 5 BKFINGCUS1M1
 Branches with MW flow more than
                                  90.0 % of nominal rating
** From bus ** ** To bus ** CKT InitFlow Rating IntLd% BaseFlow
21870 HICKOX T 115 22057 MTVERNON 115 1 108.4 110.0 98.5 89.0
21870 HICKOX T 115 22163 PETHCORN 115 1 -115.2 110.0 104.8 -95.8
20330 MURRAY 230 21282 SEDRO NT 230 1 -456.2 426.3 107.0 -339.5
20449 SEDRO 230 23097 HRNCHTAP 230 1
                                      593.9 638.2 93.1 435.7
****** Contingency
                      22 BKRPWAYLYNN
 Branches with MW flow more than
                                  90.0 % of nominal rating
** From bus ** ** To bus ** CKT InitFlow Rating IntLd% BaseFlow
21438 SUMAS CG 115 21239 KENDALL 115 1 101.7
                                              46.0 221.2
22113 NUGENT 115 21239 KENDALL 115 1
                                      -97.7
                                               46.0 212.4
 ****** Contingency 24 BKRPWAY115S
 Branches with MW flow more than 90.0 % of nominal rating
** From bus ** ** To bus ** CKT InitFlow Rating IntLd% BaseFlow
21541 BAKERVUE 115 21941 LABOUNTY 115 1 -129.1 129.1 100.0
```

114.1

110.0 103.8

21541 BAKERVUE 115 22179 PLYMOUTH 115 1

20039 BELNGM P 115 22179 PLYMOUTH 115 1 -101.2 110.0 92.0 -48.2 21438 SUMAS CG 115 21239 KENDALL 115 1 43.7 46.0 94.9 32.3

\*\*\*\*\*\* Contingency 25 BKRPWAYVISS

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 21541 BAKERVUE 115 21941 LABOUNTY 115 1 -128.2 129.1 99.3 -76.1 21541 BAKERVUE 115 22179 PLYMOUTH 115 1 113.3 110.0 103.0 61.2 20039 BELNGM P 115 22179 PLYMOUTH 115 1 -100.3 110.0 91.2 -48.2 21438 SUMAS CG 115 21239 KENDALL 115 1 43.3 46.0 94.2 32.3

\*\*\*\*\*\* Contingency 26 SLCUSSEDMUR

## Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CRT InitFlow Rating IntLd% BaseFlow

21870 HICKOX T 115 22057 MTVERNON 115 1 103.7 110.0 94.3 89.0

21870 HICKOX T 115 22163 PETHCORN 115 1 -110.6 110.0 100.5 -95.8

\*\*\*\*\*\* Contingency 28 BKFCUSMURPWY

## Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21870 HICKOX T 115 22057 MTVERNON 115 1 107.6 110.0 97.8 89.0

21870 HICKOX T 115 22163 PETHCORN 115 1 -114.4 110.0 104.0 -95.8

20449 SEDRO 230 23097 HRNCHTAP 230 1 576.3 638.2 90.3 435.7

\*\*\*\*\*\* Contingency 29 BKFCUSMURIN2

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21870 HICKOX T 115 22057 MTVERNON 115 1 103.7 110.0 94.3 89.0

21870 HICKOX T 115 22163 PETHCORN 115 1 -110.6 110.0 100.5 -95.8

\*\*\*\*\*\* Contingency 35 BKFSEDBOTBHM

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21870 HICKOX T 115 22057 MTVERNON 115 1 109.2 110.0 99.3 89.0

21870 HICKOX T 115 22163 PETHCORN 115 1 -116.1 110.0 105.5 -95.8 20330 MURRAY 230 21282 SEDRO NT 230 1 -472.7 426.3 110.9 -339.5

\*\*\*\*\*\*\* Contingency 36 BKFSEDTXCUSM

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21529 ARLNGTON 115 20033 BEAVERLK 115 1 -99.1 110.0 90.1 -70.7

20033 BEAVERLK 115 21563 BIGROCK 115 1 -99.2 110.0 90.2 -70.9

21563 BIGROCK 115 22057 MTVERNON 115 1 -105.7 110.0 96.1 -77.3

21870 HICKOX T 115 22057 MTVERNON 115 1 117.3 110.0 106.6 89.0

21870 HICKOX T 115 22163 PETHCORN 115 1 -124.2 110.0 112.9 -95.8

21250 MARCHPT 115 22150 PADILTAP 115 1 -148.3 143.0 103.7 -110.3

22150 PADILTAP 115 21439 TEXACO E 115 1 -152.0 143.0 106.3 -114.0

\*\*\*\*\*\*\* Contingency 37 BKFMPTTXCUSM

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21563 BIGROCK 115 22057 MTVERNON 115 1 -104.8 110.0 95.2 -77.3

21870 HICKOX T 115 22163 PETHCORN 115 1 116.4 110.0 105.8 89.0

21870 HICKOX T 115 22163 PETHCORN 115 1 -123.3 110.0 112.1 -95.8

\*\*\*\*\*\* Contingency 39 BKFSEDTXHRBO

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21529 ARINGTON 115 20033 BEAVERLK 115 1 -108.0 110.0 98.1 -70.7

20033 BEAVERLK 115 21563 BIGROCK 115 1 -108.1 110.0 98.3 -70.9

21529 ARINGTON 115 21187 BEVERLY 115 1 106.0 110.0 96.4 68.8

21563 BIGROCK 115 22057 MTVERNON 115 1 -114.6 110.0 104.2 -77.3

21870 HICKOX T 115 22163 PETHCORN 115 1 126.2 110.0 114.7 89.0

21250 MARCHPT 115 22163 PETHCORN 115 1 -133.1 110.0 121.0 -95.8

21250 MARCHPT 115 22180 PADILTAP 115 1 -141.5 143.0 98.9 -110.3

20330 MURRAY 230 21282 SEDRO NT 230 1 -496.2 426.3 116.4 -339.5

22150 PADILTAP 115 21439 TEXACO E 115 1 -145.2 143.0 101.5 -114.0

\*\*\*\*\*\*\* Contingency 43 BKRMARPTE115

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21250 MARCHPT 115 21440 TEX\_WEST 115 1 -286.0 264.9 108.0 -186.3

\*\*\*\*\*\*\* Contingency 45 BKRMARPTS115

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21870 HICKOX T 115 22057 MTVERNON 115 1 101.6 110.0 92.3 89.0

21870 HICKOX T 115 22163 PETHCORN 115 1 -108.4 110.0 98.6 -95.8

21250 MARCHPT 115 22150 PADILTAP 115 1 -247.5 143.0 173.1 -110.3

22150 PADILTAP 115 21439 TEXACO E 115 1 -251.1 143.0 175.6 -114.0

\*\*\*\*\*\* Contingency 46 SLSEDROHRBOT

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21563 BIGROCK 115 22057 MTVERNON 115 1 -102.7 110.0 93.4 -77.3

21870 HICKOX T 115 22057 MTVERNON 115 1 114.3 110.0 103.9 89.0

21870 HICKOX T 115 22163 PETHCORN 115 1 -121.2 110.0 110.2 -95.8

20330 MURRAY 230 21282 SEDRO NT 230 1 -517.6 426.3 121.4 -339.5

\*\*\*\*\*\*\* Contingency 47 DCBOTSAMSEDH

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21563 BIGROCK 115 22057 MTVERNON 115 1 -102.5 110.0 93.2 -77.3

21870 HICKOX T 115 22057 MTVERNON 115 1 114.1 110.0 103.8 89.0

21870 HICKOX T 115 22163 PETHCORN 115 1 -121.0 110.0 110.0 -95.8

20330 MURRAY 230 21282 SEDRO NT 230 1 -511.4 426.3 120.0 -339.5

\*\*\*\*\*\* Contingency 48 BUSMURRAY230

## Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21870 HICKOX T 115 22057 MTVERNON 115 1 110.0 110.0 100.0 89.0

21870 HICKOX T 115 22163 PETHCORN 115 1 -116.9 110.0 106.2 -95.8

20449 SEDRO 230 23097 HRNCHTAP 230 1 600.2 638.2 94.0 435.7

\*\*\*\*\*\*\* Contingency 50 BKFMURCUSSED

## From bus \*\* \*\* To bus \*\* CRT InitFlow Rating IntLd% BaseFlow PlackOX T 115 22057 MTVERNON 115 1 105.0 110.0 95.5 89.0 21870 HICKOX T 115 22163 PETHCORN 115 1 -111.9 110.0 101.7 -95.8

\*\*\*\*\*\* Contingency 51 BKFHRSUB

Bra	nches with	MW	flow	more tha	n 9	0.0 % of no	minal rat	ina	
	from bus	* **	**	To bus	** CKT	InitFlow			BaseFlow
2152	9 ARLNGTON	115	20033	BEAVERLK	115 1	-100 6			-70.7
2003	BEAVERLK	115	21563	BIGROCK	115 1	-100 8	110.0		
21563	BIGROCK	115	22057	MTVERNON	115 1	-107.2		97.5	
21870	HICKOX T	115	22057	MTVERNON	115 1	118.9	110.0		
21870	HICKOX T	115	22163	PETHCORN	115 1	-125.7			-95.8
20330	MURRAY	230	21282	SEDRO NT	230 1	-554.5			-339.5

## **APPENDIX E**

## FCITC Single Study

\*\*\* MUST 4.00 \*\*\* MON, MAR 05 2001 12:00 \*\*\*

02HSNS02 BCH=2850/300 WASK=1173,SCL=100, INDUSTRIAL LD ADJ.

ALL WA/SK GEN ON - BASE CASE MPCC 50 MW GEN. Not Running
Subsys.File D:\Summer-2000\subni-us.sub
Monit.File D:\Summer-2000\monzonepsregion-MPCC.mon
Contin.File D:\WINTER00-01\NI-ALL.con
Exclud.File none

Study transfer level - 100.0 MW. Total violations: 6
First violation - -1265.4 MW.

Study transfer. From NIBCH To NIPNW . Transfer level - 100.0 MW

Violations report ordered by transfer capability. Total 6 violations

N Export L: Limiting constraint PTDF =Base Case Flow= PreShift MW C: Contingency description Ncon Flow Rating Init Final LODF 1 2421.7 L:20330 MURRAY 230 21282 SEDRO NT 230 1 -540.3 -426.3 -0.09013 C: BKFHRSUB Open 20324 MONROE T 230 23107 HRTAP MS 230 1 Open 20324 MONROE T 230 23107 HRTAP MS 230 2 Open 20467 SNOHOMSH 230 23107 HRTAP MS 230 1 0.45382 -Open 20467 SNOHOMSH 230 23107 HRTAP MS 230 2 0.45382 -Open 21443 HORSRNCH 230 23107 HRTAP MS 230 1 Open 20322 MONROE 230 20324 MONROE T 230 1 0.34113 Open 20065 BOTHELL 230 23097 HRNCHTAP 230 1 0.42400 -Open 20449 SEDRO 230 23097 HRNCHTAP 230 1 -0.33821 Open 21443 HORSRNCH 230 23097 HRNCHTAP 230 1 NA 2 2768.7 L:20330 MURRAY 230 21282 SEDRO NT 230 1 -503.0 -426.3 -0.08356 C:SLSEDROHRBOT 40 Open 20065 BOTHELL 230 23097 HRNCHTAP 230 1 Open 20449 SEDRO 230 23097 HRNCHTAP 230 1 -0.01405 --0.42185 Open 21443 HORSRNCH 230 23097 HRNCHTAP 230 1 3 2839.3 L:20330 MURRAY 230 21282 SEDRO NT 230 1 -496.8 -426.3 -0.08321 C:DCBOTSAMSEDH Open 20065 BOTHELL 230 23097 HRNCHTAP 230 1 -0.00681 -Open 20449 SEDRO 230 23097 HRNCHTAP 230 1 Open 21443 HORSRNCH 230 23097 HRNCHTAP 230 1 -0.42382Open 20065 BOTHELL 230 20438 SAMMAMSH 230 &1 0.07746 Open 20065 BOTHELL 230 20438 SAMMAMSH 230 &1 0.03975 4 3014.4 L:20330 MURRAY 230 21282 SEDRO NT 230 1 -483.4 -426.3 -0.08487 C:BKFSEDTXHRBO 39

				BOTHELL									-0.01387	_'
		Open	20449	SEDRO	230	23097	HRNCHTAI	230	1				-0.43242	
		Open	21443	HORSRNCH	230	23097	HRNCHTAI	230	1				0.07290	
		Open	20448	SEDRO	115	20449	SEDRO	230	1				0.12508 -	_
5	3269.7	L:2033	0 MURR	AY 230	21282	2 SEDR	O NT 230	1		-455.5	-426 3	-0 07004	0.12300 -	_
		C:BKFS								35	-20.5	0.07004		_
		Open	20065	BOTHELL	230	23097	HRNCHTAF	230	1				-0.01236 -	
				SEDRO										-
				HORSRNCH									-0.48250	
٠				BELLNGHM									0.06440	
6	3460.1			AY 230								4.21	0.26851	
		C:BKFI	7000101	41		3EDR(	NI 230	1			-426.3	-0.08665	· <del>-</del>	•
										5			1.	
		Open	4058	ING500	500	20137	CUSTER W	500	1				0.00359	
		Open	20137	CUSTER W	500	20323	MONROE	500	&1				-0.10055	
				CUSTER W									-0.00659	
													0.00033	

. 13

(market)

## **APPENDIX F**

## FCITC Single Study

\*\*\* MUST 4.00 \*\*\* MON, MAR 05 2001 12:04 \*\*\*

02HSNS02 BCH=2850/300 WASK=1173,SCL=100, INDUSTRIAL LD ADJ.

ALL WA/SK GEN ON - BASE CASE MPCC 50 MW GEN. IN SERVICE

Subsys.File D:\Summer-2000\subni-us.sub

Monit.File D:\Summer-2000\monzonepsregion-MPCC.mon

Contin.File D:\WINTER00-01\NI-ALL.con

Exclud.File none

Study transfer level - 100.0 MW. Total violations: 6
First violation - -1438.5 MW.

Study transfer. From NIBCH To NIPNW . Transfer level - 100.0 MW

Violations report ordered by transfer capability. Total 6 violations

N Export L: Limiting constraint PreShift MW TDF Case Flow= C: Contingency description Ncon Flow Rating LODE Init Final 1 2248.4 L:20330 MURRAY 230 21282 SEDRO NT 230 1 -554.5 -426.3 -0.08909 C:BKFHRSUB Open 20324 MONROE T 230 23107 HRTAP MS 230 1 Open 20324 MONROE T 230 23107 HRTAP MS 230 2 Open 20467 SNOHOMSH 230 23107 HRTAP MS 230 1 Open 20467 SNOHOMSH 230 23107 HRTAP MS 230 2 Open 21443 HORSRNCH 230 23107 HRTAP MS 230 1 Open 20322 MONROE 230 20324 MONROE T 230 1 Open 20065 BOTHELL 230 23097 HRNCHTAP 230 1 Open 20449 SEDRO 230 23097 HRNCHTAP 230 1 Open 21443 HORSRNCH 230 23097 HRNCHTAP 230 1 2 2579.6 L:20330 MURRAY 230 21282 SEDRO NT 230 1 -517.6 -426.3 -0.08249 C:SLSEDROHRBOT Open 20065 BOTHELL 230 23097 HRNCHTAP 230 1 Open 20449 SEDRO 230 23097 HRNCHTAP 230 1 Open 21443 HORSRNCH 230 23097 HRNCHTAP 230 1 3 2651.2 L:20330 MURRAY 230 21282 SEDRO NT 230 1 -511.4 -426.3 -0.08213 C:DCBOTSAMSEDH Open 20065 BOTHELL 230 23097 HRNCHTAP 230 1 Open 20449 SEDRO 230 23097 HRNCHTAP 230 1 Open 21443 HORSRNCH 230 23097 HRNCHTAP 230 1 Open 20065 BOTHELL 230 20438 SAMMAMSH 230 &1 Open 20065 BOTHELL 230 20438 SAMMAMSH 230 &1 4 2854.2 L:20330 MURRAY 230 21282 SEDRO NT 230 1 -496.2 -426.3 -0.08392

C:BKFSEDTXHRBO Open 20065 BOTHELL 230 23097 HRNCHTAP 230 1 Open 20449 SEDRO 230 23097 HRNCHTAP 230 1 Open 21443 HORSRNCH 230 23097 HRNCHTAP 230 1 Open 20448 SEDRO 115 20449 SEDRO 230 1 5 3011.8 L:20330 MURRAY 230 21282 SEDRO NT 230 1 -472.7 -426.3 -0.06877 C: BKFSEDBOTBHM 35 Open 20065 BOTHELL 230 23097 HRNCHTAP 230 1 Open 20449 SEDRO 230 23097 HRNCHTAP 230 1 Open 21443 HORSRNCH 230 23097 HRNCHTAP 230 1 Open 20038 BELLINGHM 230 20449 SEDRO 230 1 6 3338.9 L:20330 MURRAY 230 21282 SEDRO NT 230 1 -456.2 -426.3 -0.08591 C: BKFINGCUS1M1 Open 4058 ING500 500 20137 CUSTER W 500 1 Open 20137 CUSTER W 500 20323 MONROE 500 &1 Open 20137 CUSTER W 500 20323 MONROE 500 &1

## **APPENDIX G**

## Contingency Analysis Detailed Report

```
*** MUST 4.00 *** MON, MAR 05 2001 12:20 ***
      02HSNS02 BCH=2850/300 WASK=1173,SCL=100, INDUSTRIAL LD ADJ.
      ALL WA/SK GEN ON - LLH CASE, MPCC 50 MW GEN. IN SERVICE
 Subsys.File D:\Summer-2000\subni-us.sub
 Monit.File D:\Summer-2000\monzonepsregion-MPCC.mon
 Contin.File D:\Summer-2000\contzonepsregion-fredonia.con
 Exclud.File none
  Detailed report on selected contingencies. Total 465. Selected 12
 Study transfer not defined
  ******* Contingency 1 SLTEXWMPT115
 Branches with MW flow more than 90.0 % of nominal rating
 ** From bus ** ** To bus ** CKT InitFlow Rating IntLd% BaseFlow
21250 MARCHPT 115 22150 PADILTAP 115 1 -278.4 143.0 194.7 -106.2
22150 PADILTAP 115 21439 TEXACO E 115 1 -282.1 143.0 197.3 -109.9
****** Contingency 15 20026 BAKER SW 115 20448 SEDRO
 Branches with MW flow more than 90.0 % of nominal rating
** From bus ** ** To bus ** CKT InitFlow Rating IntLd% BaseFlow
20448 SEDRO 115 20026 BAKER SW 115 2
                                     -121.7
                                                 98.0 124.2
 ******* Contingency 16 20026 BAKER SW 115 20448 SEDRO
 Branches with MW flow more than
                                 90.0 % of nominal rating
** From bus ** ** To bus ** CKT InitFlow Rating IntLd% BaseFlow
20448 SEDRO 115 20026 BAKER SW 115 1 -121.7
                                               98.0 124.2 -61.4
******* Contingency 58 21607 BURLIGTN 115 23004 RITA
```

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 21250 MARCHPT 115 22150 FADILTAP 115 1 -148.2 143.0 103.7 -106.2 22150 FADILTAP 115 21439 TEXACO E 115 1 -151.9 143.0 106.2 -109.9

\*\*\*\*\*\*\* Contingency 256 21249 LYNDEN 115 22272 SCHUETT 115 1

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 21438 SUMAS CG 115 21239 KENDALL 115 1 104.8 46.0 227.7 31.4 22113 NUGENT 115 21239 KENDALL 115 1 -101.8 46.0 221.2 -28.4 22113 NUGENT 115 22443 VANWYCK 115 1 99.1 109.0 90.9 25.7

\*\*\*\*\*\*\* Contingency 259 20290 MARCH PT 230 20449 SEDRO 230 1

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21534 AVON PMP 115 22494 WILSN TP 115 1 -134.2 143.0 93.9 -83.7

21870 HICKOX T 115 22057 MTVERNON 115 1 105.2 110.0 95.6 87.2

21870 HICKOX T 115 22163 PETHCORN 115 1 -110.2 110.0 100.1 -92.2

\*\*\*\*\*\*\* Contingency 260 20290 MARCH PT 230 21250 MARCHPT 115 1

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 21534 AVON PMP 115 22494 WILSN TP 115 1 -134.6 143.0 94.1 -83.7 21870 HICKOX T 115 22163 PETHCORN 115 1 -110.3 110.0 95.7 87.2 21870 HICKOX T 115 22163 PETHCORN 115 1 -110.3 110.0 100.3 -92.2

\*\*\*\*\*\*\*\* Contingency 266 21250 MARCHPT 115 22150 PADILTAP 115 1

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21250 MARCHPT 115 21440 TEX\_WEST 115 1 -279.7 264.9 105.6 -183.7

\*\*\*\*\*\*\* Contingency 376 20448 SEDRO 115 20449 SEDRO 230 1

Branches with MW flow more than 90.0 % of nominal rating

```
** From bus ** ** To bus ** CKT InitFlow Rating IntLd% BaseFlow 21870 HICKOX T 115 22057 MTVERNON 115 1 104.7 110.0 95.2 87.2 21870 HICKOX T 115 22163 PETHCORN 115 1 -109.7 110.0 99.7 -92.2 21250 MARCHPT 115 22150 PADILTAP 115 1 -145.9 143.0 102.0 -106.2 22150 PADILTAP 115 21439 TEXACO E 115 1 -149.5 143.0 104.6 -109.9
```

\*\*\*\*\*\*\*\* Contingency 381 20448 SEDRO 115 23004 RITA 115 1

production of the state of the

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21250 MARCHPT 115 22150 PADILTAP 115 1 -147.3 143.0 103.0 -106.2

22150 PADILTAP 115 21439 TEXACO E 115 1 -151.0 143.0 105.6 -109.9

\*\*\*\*\*\*\* Contingency 382 20449 SEDRO 230 23097 HRNCHTAP 230 1

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21529 ARLNGTON 115 20033 BEAVERLK 115 1 -100.0 110.0 91.0 -74.4

20033 BEAVERLK 115 21563 BIGROCK 115 1 -100.2 110.0 91.1 -74.5

21563 BIGROCK 115 22057 MTVERNON 115 1 -104.8 110.0 95.3 -79.1

21870 HICKOX T 115 22057 MTVERNON 115 1 112.9 110.0 102.6 87.2

21870 HICKOX T 115 22163 PETHCORN 115 1 -117.9 110.0 107.2 -92.2

20330 MURRAY 230 21282 SEDRO NT 230 1 -513.8 426.3 120.5 -331.6

\*\*\*\*\*\*\*\* Contingency 409 21438 SUMAS CG 115 22272 SCHUETT 115 1

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

22443 VANWYCK 115 21595 BRITTON 115 1 104.9 109.0 96.2 24.3

21438 SUMAS CG 115 21239 KENDALL 115 1 111.9 46.0 243.3 31.4

22113 NUGENT 115 21239 KENDALL 115 1 -108.9 46.0 236.8 -28.4

22113 NUGENT 115 22443 VANWYCK 115 1 106.2 109.0 97.5 25.7

#### APPENDIX H

## Contingency Analysis Detailed Report

```
*** MUST 4.00 *** MON, MAR 05 2001 15:12 ***

02HSNS02 BCH=2850/300 WASK=1173,SCL=100, INDUSTRIAL LD ADJ.

ALL WA/SK GEN ON - LLH CASE, MPCC 50 MW GEN. IN SERVICE
Subsys.File D:\Summer-2000\subni-us.sub
Monit.File D:\Summer-2000\monzonepsregion-MPCC.mon
```

Contin.File D:\Summer-2000\NI-ALL.con

Exclud. File none

Detailed report on selected contingencies. Total 77. Selected 15

Study transfer not defined

\*\*\*\*\*\* Contingency 5 BKFINGCUS1M1

Branches with N	W flow	more than	n 90	0.0 % of no	ominal rat	ing	
** From bus *	* **	To bus	** CKT	InitFlow	Rating	IntLd%	BaseFlow
21563 BIGROCK 11							-79.1
21870 HICKOX T 11	5 22057	MIVERNON	115 1	107.3	110.0	97.6	87.2
21870 HICKOX T 11	5 22163	PETHCORN	115 1	-112.3	110.0	102.1	-92.2
20330 MURRAY 23	0 21282	SEDRO NT	230 1	-452.3	426.3	106.1	-331.6
20449 SEDRO 23	0 23097	HRNCHTAP	230 1	600.0	638.2	94.0	436.3

\*\*\*\*\*\* Contingency 22 BKRPWAYLYNN

```
Branches with MW flow more than 90.0 % of nominal rating

** From bus ** ** To bus ** CKT InitFlow Rating IntLd% BaseFlow

21438 SUMAS CG 115 21239 KENDALL 115 1 104.8 46.0 227.7 31.4

22113 NUGENT 115 21239 KENDALL 115 1 -101.8 46.0 221.2 -28.4

22113 NUGENT 115 22443 VANWYCK 115 1 99.1 109.0 90.9 25.7
```

\*\*\*\*\*\* Contingency 24 BKRPWAY115S

21541	BAKERVUE	115	22179	PLYMOUTH	115	1	120.9	110.0	109.9	61.7
20039	BELNGM P	115	22179	PLYMOUTH	115	1	-111.8	110.0	101.6	-52.7
21438	SUMAS CG	115	21239	KENDALL	115	1	44.4	46.0	96.6	31.4
22113	NUGENT	115	21239	KENDALL	115	1	-41.4	46.0	90.1	-28.4

\*\*\*\*\*\* Contingency 25 BKRPWAYVISS

. E	Branc	ches v	vith	MW	flow	more than	1	9(	0.0 % of r	imor	nal rat	ing	
**	1	From h	ous	**	** ,	To bus	**	CKT	InitFlow		Rating	IntLd%	BaseFlow
21	541	BAKE	RVUE	115	21941	LABOUNTY	115	1	-130.9		129.1	101.4	-72.3
21	541	BAKEF	RVUE	115	22179	PLYMOUTH	115	1	120.2		110.0	109.3	61.7
20	039	BELNO	M P	115	22179	PLYMOUTH	115	1	-111.2		110.0	101.1	-52.7
21	438	SUMAS	CG	115	21239	KENDALL	115	1	44.2		46.0	96.0	31.4

\*\*\*\*\*\* Contingency 28 BKFCUSMURPWY

Branches with MW							
** From bus **	**	To bus	** CKT	InitFlow	Rating	IntLd%	BaseFlow
21563 BIGROCK 115	2,2057	MIVERNON	115 1	-99.3	110.0	90.3	-79.1
21870 HICKOX T 115	22057	MIVERNON	115 1	107.5	110.0	97.7	87.2
21870 HICKOX T 115	22163	PETHCORN	115 1	-112.5	110.0	102.2	-92.2
20449 SEDRO 230	23097	HRNCHTAP	230 1	590.9	638.2	92.6	436.3

\*\*\*\*\*\* Contingency 35 BKFSEDBOTBHM

Branches with						inal rat	ing	
** From bus	**	**	To bus	** CKT	InitFlow	Rating	IntLd%	BaseFlow
21563 BIGROCK	115	22057	MIVERNON	115 1	-100.1	110.0	91.0	-79.1
21870 HICKOX T	115	22057	MTVERNON	115.1	108.2	110.0	98.4	87.2
21870 HICKOX T	115	22163	PETHCORN	115 1	-113.2	110.0	102.9	-92.2
20330 MURRAY	230	21282	SEDRO NT	230 1	-471.2	426.3	110.5	-331.6

\*\*\*\*\*\* Contingency 36 BKFSEDTXCUSM

Bran	ches with	MW	flow	more than	n.	9	0.0 % of nom	inal rat	ing	
** ]	From bus	**	**	To bus	**	CKT	InitFlow	Rating	IntLd%	BaseFlow
21529	ARLNGTON	115	20033	BEAVERLK	115	1	-104.7	110.0	95.2	-74.4
20033	BEAVERLK	115	21563	BIGROCK	115	1	-104.9	110.0	95.3	-74.5
21529	ARLNGTON	115	21187	BEVERLY	115	1	102.6	110.0	93.3	72.2
	BIGROCK							110.0	99.5	-79.1
21870	HICKOX T	115	22057	MTVERNON	115	1	117.6	110.0	106.9	87.2

									111.4	
21250	MARCHPT	115	22150	PADILTAP	115	1	-147.7	143.0	103.3	-106.2
22150	PADILTAP	115	21439	TEXACO E	115	1			105.9	

\*\*\*\*\*\* Contingency 37 BKFMPTTXCUSM

Branches with	MW	flow	more than	n 90	0.0% of non	ninal rat	ing	
** From bus	**	**	To bus	** CKT	InitFlow	Rating	IntLd%	BaseFlow
21529 ARLNGTON	115	20033	BEAVERLK	115 1	-105.7	← 110.0		
20033 BEAVERLK					-105.9	110.0		
21529 ARLNGTON					103.6	110.0	94.1	72.2
21563 BIGROCK					-110.4	110.0	100.4	-79.1
21870 HICKOX T					118.6	110.0	107.8	87.2
21870 HICKOX T	115	22163	PETHCORN	115 1	-123.6	110.0	112.3	-92.2

\*\*\*\*\*\* Contingency 39 BKFSEDTXHRBO

American Commence of the Comme

	ches with			more than	n	9	0.0 % of nor	ninal rat	ting	
	From bus			To bus	**.	CKT	InitFlow	-	-	BaseFlow
	ARLNGTON						-113.4		103.1	
20033	BEAVERLK	115	21563	BIGROCK	115	1	-113.5	110.0	103.2	-74.5
	ARLNGTON						111.2		101.1	
	BIGROCK						-118.1	110.0	107.4	-79.1
21870	HICKOX T	115	22057	MTVERNON	115	1	126.2	110.0	114.8	87.2
21870	HICKOX T	115	22163	PETHCORN	115	1	-131.2		119.3	-92.2
21250	MARCHPT	115	22150	PADILTAP	115	1	-141.7	143.0	99.1	-106.2
20330	MURRAY	230	21282	SEDRO NT	230	1 .	-485.9		114.0	-331.6
22150	PADILTAP	115	21439	TEXACO E	115	1	-145.3	143.0	101.6	-109.9
										m U J . J

\*\*\*\*\*\* Contingency 43 BKRMARPTE115

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21250 MARCHPT 115 21440 TEX\_WEST 115 1 -279.7 264.9 105.6 -183.7

\*\*\*\*\*\* Contingency 45 BKRMARPTS115

## From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow 21534 AVON PMP 115 21607 BURLIGTN 115 1 136.6 143.0 95.6 77.6 21534 AVON PMP 115 22494 WILSN TP 115 1 -142.7 143.0 99.8 -83.7

21070									
21870 HICKO							110.0	94 1	87.2
21970 87080	v m 11r	001.50				- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1		74.1	0/.2
21870 HICKO	Y T TT2	22163	PETHCORN	115	1	-108.5	110.0	98 6	-92.2
21250 MARCE	DM 115	22150			_				
21250 MARCH							143.0	161.5	-106.2
22150 PADIL	מוד מגיי	21420							
-arso Padill	TWE ITS	21439	TEXACO E	115	1	-234.6	143.0	164.1	-109.9

\*\*\*\*\*\* Contingency 46 SLSEDROHRBOT

The second secon

	ches with			more than	90	0.0% of non	ninal ras	ting	
	From bus			To bus	** CKT	InitFlow		_	BaseFlow
				BEAVERLK		-99.8	110.0		-74 4
20033	BEAVERLE	115	21563	BIGROCK	115 1	-99.9	110.0	90.9	-74.5
21563	BIGROCK	115	22057	MTVERNON	115 1	-104.5	110.0	95.0	-79.1
21870	HICKOX T	115	22057	MTVERNON :	115 1	112.7	110.0	102.4	87.2
				PETHCORN :		-117.7	110.0	107.0	-92.2
20330	MURRAY	230	21282	SEDRO NT	230 1	-510.5	426.3	119.7	-331.6

\*\*\*\*\*\* Contingency 47 DCBOTSAMSEDH

				flow	more tha	n	9	0.0 % of nom	inal rat	ting	
	From				To bus	**	CKT	InitFlow	Rating	IntLd%	BaseFlow
21529	ARLN	GTON	115	20033	BEAVERLK	115	1	-99.6			-74.4
20033	BEAV	ERLK	115	21563	BIGROCK	115	1	-99.8		90.7	-74.5
21563	BIGR	OCK	115	22057	MTVERNON	115	1	-104.4	110.0		-7 <b>4.</b> 3
21870	HICK	T XC	115	22057	MTVERNON	115	1	112.5	110.0	102.3	87.2
21870	HICK	T XC	115	22163	PETHCORN	115	1	-117.5		106.8	-92.2
20330	MURRA	AY	230	21282	SEDRO NT	230	1	-504.4		118.3	-331.6

\*\*\*\*\*\* Contingency 48 BUSMURRAY230

Branches with MW flow	more than 90.0 % of nominal rating	
** From bus ** **	To bus ** CKT InitFlow Rating Tatide	BaseFlow
21563 BIGROCK 115 22057	MTVERNON 115 1 -99 3 110 0 00 2	-79.1
21870 HICKOX T 115 22057	MTVERNON 115 1 107 4 110 0 07 7	87.2
21870 HICKOX T 115 22163	PETHCORN 115 1 -112.4 110.0 102.2	-92.2
20449 SEDRO 230 23097	HRNCHTAP 230 1 597.3 638.2 93.6	
	038.2 93.6	436.3

\*\*\*\*\*\* Contingency 51 BKFHRSUB

Branches with MW flow more than 90.0 % of nominal rating

\*\* From bus \*\* \*\* To bus \*\* CKT InitFlow Rating IntLd% BaseFlow

21529 ARLNGTON 115 20033 BEAVERLK 115 1 -103.0 110.0 93.6 -74.4

Ex. \_\_\_\_(WAG-4) Page 205 of 219

	BEAVERLK						-103.1	110.0	93.7	-74.5
	ARLNGTON						100.8	110.0	91.6	72.2
	BIGROCK						-107.7	110.0	97.9	-79.1
21870	HICKOX T	115	22057	MIVERNON	115	1	115.8	110.0	105.3	87.2
	HICKOX T					_	-120.8	110.0	109.8	-92.2
20330	MURRAY	230	21282	SEDRO NT	230	1	-536.1	426.3	125.8	-331.6

Section 18 and 1

# Sumas II - 720 MW

# SUMAS II 720 MW

# **Sumas II - Transmission Constraints Scoping Study**

Summary.

Sumas II has been proposed as a generation addition in Whatcom County, located adjacent to the existing Sumas cogeneration facility. The generation proposed has been described at two sets of CT's and steam units. Each CT and steam unit pair would generate between 355 and 370 MW. The MW output could be connected to B.C. Hydro facilities across the border with Canada, or into the Whatcom County system. This study addresses only the option to connect the generators to the Whatcom County system. Because of Initiative 4-90 in Whatcom County, the project developer has suggested the generation be integrated using 115 kV transmission facilities.

Two generation connection choices are discussed with this report, either to connect one generator pair to BPA Bellingham Substation (360 MW), or to connect one generator pair to BPA Bellingham Substation and a second generator pair to PSE Portal Way Substation (720 MW total). Each generator pair would be connected to Bellingham or Portal Way on a 115 kV radial transmission line. All the combinations and connection possibilities are not addressed. The ones used are probably the least expensive. The attention of this study is more on the transmission problems from adding 360 or 720 MW to existing North-to-South obligations from Skagit County through King County.

Because of time constraints, this is a scoping study and only addresses summer conditions for the year 2004, in the Northern Intertie North-to-South direction. While the summer is usually the most limiting, there may be other facilities that overload in association with the proposed Sumas II generation for South-to-North flows, for light summer loads, or during higher winter load conditions. This would be verified with further studies.

The projects identified in this are not the only ones that could correct system constraints, nor are they necessarily the one that would be selected as the result of a more extensive study and a complete environmental review and permitting process. They were selected so that a rough approximation of the ultimate system costs that may be associated with these generation projects could be determined.

The cost estimates are given in the following table. The table does not include costs for constructing the generating facilities or the transmission facilities to bring them to BPA Bellingham and Portal Way Substations. The generation developer will have accurate estimates through the services of consulting engineers. The table indicates a significant step to integrate the first generator pair (360 MW). This is due to facilities needed to resolve problems in Skagit and Snohomish Counties. (The estimates have been developed from experience with similar projects. They have not been reviewed by transmission and substation design engineers because of time constraints.)

Enclosure 1

Table - Cost Estimates

Table - Cost Est	mates			
Stages of Sumas II Generation Additions	· · · · · · · · · · · · · · · · · · ·	Cost E	Estimates (	\$ x1000)
Facility Additions		Low	High	Altern-
Phase 1 Improvements to Recover NI 2850 summe	<b>.</b>	,,,	9	atives
Beverly-Hilton Lake 115 kV uprate from 75 to 100C				The second second
Monroe-Snohomish #1 230 kV uprate from 90 to 100C	3.4 mi	50		
Snohomish-Bothell #1 230 kV uprate from 80 to 100C	10 mi	50		
Snohomish-Bothell #2 230 kV uprate from 90 to 100C	7.6 mi	50		
Bothell 230 kV line get-away re-arrangement	7.4 mi	30		
Sammamish 115 kV trf breakers and switch replacement	5 lines	300		
Re-terminate Snoking-Maple V #1 230 kV line onto Talbot N	2 each	600		
Subtotal	1 1 bkr	1,100	•	
		2,180	3,550	
Phase 2 Improvements for Sumas II - 360 MW				
At BPA Bellingham install #2 230-115 kV trf and breakers				
50 Mvar, 115 kV capacitor bank at BPA Bellingham		4,200	•	
Sedro-Horse Ranch #2 230 kV rebuild w/ 2-Tern on		300		
H-frame or rebuild with size to at the	39 mi	8,000	16,000	
H-frame or rebuild with single steel poles Sedro-Beaver Lake 115 kV, build Narcissus				31,200
At Sedro Woolley install 2 220 benefits a 4 11.	4.8 mi	1,200	1,600	
At Sedro Woolley install 2 230 breakers & 1 line bay		1,500	2,000	
At Horse Ranch install 2 230 breakers & 1 line bay		2,000	2,600	
Snohomish-Beverly #3 & #4 115 kV uprate 50C to 100C	1.3 mi ea	50	200	
Bothell-Sammamish 230 kV 2-Tern re-cond. on H-frame	13.4 mi	3,350	5,360	
or rebuild with steel poles				13,400
Cottage Brook-Fall City 115 kV uprate from 75C to 90C	18.2 mi	1,200	2,700	
Subtotal		21,800	36,510	65,750
Phase 2 Improvements 6 0				
Phase 3 Improvements for Sumas II - 720 MW				
At Portal Way install #2 230-115 kV trf and breakers		4,200	5,600	
50 Mvar, 115 kV capacitor bank at Portal Way		300	450	
Convert Snohomish-Boeing 115 kV to 230 kV				
Terminate at Snohomish 230 kV, bkr & line bay		1,100	1,800	
Terminate Boeing 115 at Beverly, bkr & line bay		450	800	*** **
Terminate HR, Snoh & Both 230 kV lines at Beverly	3 each	4,000	6,500	
At Beverly install #2 230-115 kV trf and breakers		3,900	5,300	
Monroe-Snohomish #1 230 kV uprate from 90 to 100C	0.75 mi	25	150	
Rebuild Samm-Lakeside #2 to 230 w/ Jefferson H-frame	7.1 mi	2,000	3,500	
or rebuild with single steel poles		_,,	0,000	7,100
Rebuild Lakeside-Talbot #2 to 230 w/ Jefferson H-frame	8.9 mi	2,500	4,400	7,100
or rebuild with single steel poles	0.0	2,000	4,400	8,900
Terminate at Sammamish 230 kV, bkr & line bay		900	1,300	0,300
Terminate at Talbot N 230 kV, bkr & line bay		900	1,300	
Re-terminate Snoking-Maple V #1 230 kV line to Talbot S	1 bkr	<b>300</b>	_	
At Lakeside, terminate Samm & Talbot 230 kV lines, and	, DAI	6,900	10,600	
install 230-115 kV trf and breakers		0,300	10,000	
Hilton Lake-Lake Leota 115 kV uprate from 75 to 100C	11.2 mi	200	750	
Cottage Brook-Fall City 115 kV leave at 75C	11.4 1111	300	750 2.700	
Subtotal		-1,200	-2,700	
		26,275	39,750	
Total - Recover NI 2850 + 720 MW		50,255	79,810	
Footnotes:				

Ex. \_\_\_\_(WAG-4) Page 208 of 219

Sumas IIc.doc

① Cost included in Phase 2, but with the Sammamish-Talbot 230 kV line, put Snoking onto Talbot South bus instead of Talbot North.

### I. Existing System Assessment.

Some facilities are near, at, or above their limits with north to south BCH flow on the West Side Northern Intertie (NI). These facilities for NtoS include:

- 1. Sedro Bellingham #3 & #4 115 lines
- 2. Sedro NT Murray 230 line
- 3. March Point Beverly 115 line
- 4. Snohomish Bothell #1 & #2 230 lines
- 5. Bothell Snoking 230 line(s)
- 6. Snoking Maple Valley 230 line(s)
- 7. Beverly Cottage Brook and Cottage Brook Fall City 115 kV lines

SCL has begun opening their transmission network north of Broad Street Substation, separating North Seattle from the downtown area and South Seattle. This action shifts power flow on to PSE and BPA facilities east of Seattle that carry power in the north / south direction.

With all PSE CT's on in the Summer, the sum of PSE and IPP generation represented in Whatcom and Skagit Counties is 1186 MW. With all CT's on in the winter, except for Whitehorn Unit 1, the sum is 1200 MW. The additional amount in the winter is because units can run at higher output levels during cooler weather. Without PSE CT's, the amounts are 774 and 817 MW. When PSE CT's are running, to mitigate overloaded facilities from certain outages when there is north to south BCH flow, the CT's are then tripped. The outages wired for generator tripping are the loss of both Custer-Monroe 500 kV lines, the loss of the Monroe-Echo Lake 500 kV line, and the loss of the Raver-Paul 500 kV line.

There are several outages that cause overloads during high north to south imports and high PSE generation. BPA has proposed several breaker additions, to use the second SCL owned 230 kV circuit between Bothell, Snoking, and Maple Valley, and to repair and re-energize the Chief Joe-Snohomish #4 line from 230 to 345 kV. BPA anticipates the Bothell-Snoking 1&2 230 and Snoking-Maple Valley 1&2 230 kV lines to be upgraded to 100C conductor rating. PSE has proposed several line upgrades, and to install a 230 kV breaker at Sammamish Substation. The tables in Appendix A assume that these breakers and line upgrades have been completed. Recently, some new outages have been identified that are quite severe. They are the bus segment outages of the SCL Bothell 230 kV bus.

After the proposed upgrades and additions have been completed, with full PSE generation during the summer and winter, there will be facility maintenance outages that will limit the north to south capability to less than 2850 MW in the summer and 1450 MW in the winter.

# II. Improvements to Recover NI 2850 Summer - Phase 1.

The following is a discussion of improvements to recover the 2850 MW NI Rating in the summer when the SCL Skagit and PSE Northern generation is fully on or at a minimum. The maximum / minimum summer generation for PSE in Whatcom and Skagit is 1186 / 260 MW, and for SCL in Skagit is 650 / 100 MW.

In the Existing System Assessment, certain facilities were assumed to have been completed. The items taking the longest time are probably connecting the Bothell-Snoking #2 and Snoking-Maple Valley #2 230 kV lines, and restoring the Chief Joe-Snohomish #4 to 345 kV operation.

#### Sumas IIc.doc

In addition to the breaker additions, upgrades and these improvements (assumed as completed in the above tables), BPA and PSE plan to replace the transformer at BPA Bellingham with a higher capacity 230-115 kV transformer. Also, BPA is proposing to move the Snoking tap from the Monroe-Sammamish 230 kV line to the Monroe-Echo Lake 500 kV line, and install a 500-230 kV transformer at Snoking Substation. The Snoking tap line is already constructed for 500 kV. A new transformer at Snoking would provide load relief to the surrounding 500-230 transformers. The following discussion and findings are made with the assumption that the Bellingham 230-115 kV transformer and the Snoking 500-230 kV transformer are installed.

An alternative that was studied was to build a second Monroe-Echo Lake 500 kV line instead of retaining the single 500 kV line configuration. This would be built on right-of-way that is separate from the existing 500 kV line, using portions of the Monroe-Sammamish and Sammamish-Maple Valley lines, with a 500-230 kV transformer at Novelty, instead of Snoking. This seems to be a better long-range plan, but is much more expensive. It does not resolve all the 230 kV problems in King County associated with the Sumas II project.

The Monroe-Snohomish 230 kV line segment that overloads (circuit #1) is one side of a 10 mile long double circuit, and it must be uprated from 90C to 100C. Circuit #2 is already 100C rated. This uprate is probably minor, and would not be required if a second Sedro Woolley-Horse Ranch 230 kV line were constructed for the proposed Sumas II generators.

The Snohomish-Bothell #1 230 kV line must be upgraded from 80C to 100C, and the Snohomish-Bothell #2 230 kV line must be upgraded from 90C to 100C. After these lines are upgraded, they will load to 105% for the double line outage.

The Bothell 230 kV bus must be rearranged. The current layout can now cause the Snohomish-Bothell #2 to overload to 140% for a loss of the Bothell #4 230 bus section. This condition is at SCL Skagit generation at 100 MW; at higher levels, the overload percent goes down. After the Snoking 500-230 kV transformer is installed, the overload goes down to 119%. A rearrangement of the lines into Bothell can resolve the overloads from bus segment outages. This includes moving the Sammamish line from the Bothell #2 bus segment to the #4 bus segment. The proposed Bothell-Snoking #2 should terminate on the #2 bus segment. The Diablo #3 line and the Snohomish #1 line should be swapped, so that Diablo #3 line terminates on #4 bus segment, and Snohomish #1 line terminates on #3 bus segment.

The Beverly-Cottage Brook 115 kV line needs to be uprated from 75C to 80C minimum.

The Sammamish 115 kV transformer breakers and disconnects load beyond their emergency ratings under a loss of the other transformer. These two 1600 A breakers and switches need to be replaced with 2000 A minimum hardware. The transformers have a higher emergency rating.

The Maple Valley 230 kV bus has two sections, with the Sammamish-Maple Valley and Snoking-Maple Valley #1 230 kV lines connected to the #2 section. An outage of the #2 section results in loss of both lines to the north. The Fall City-Cottage Brook 115 kV line overloads. When the Snoking-Maple Valley #2 230 kV line is connected to the Maple Valley #1 section, an outage of the #2 section can result in the new Snoking-Maple Valley #2 line overloading by 111% above its 1063 A (100C) rating. A solution is to relocate either the Sammamish-Maple Valley or the Snoking-Maple Valley #1 230 kV line to the Talbot North 230 kV bus. The Talbot North and South buses are such a short distance from the Maple Valley bus, that they are

Ex. \_\_\_\_(WAG-4) Page 211 of 219

Sumas IIc.doc

effectively bus sections of the Maple Valley bus. Doing this removes overloading on the Snoking-Maple Valley #2 line, and it reduces overloading on the Fall City-Cottage Brook 115 kV line to 104%.

#### III. Improvements for Sumas II at 360 MW - Phase 2.

The PSE CT's at Whitehorn and Fredonia are part of a generation dropping remedial action scheme (RAS) that is triggered when certain 500 kV facility outages occur. This must also be applied to all the Sumas II generators. The generators are tripped for Monroe-Custer #1 & #2, Monroe-Echo Lake, or Raver-Paul 500 kV outages during North to South flows, and the Sumas II connected to BPA Bellingham is tripped for BPA Bellingham 230 bus or 230-115 tx outage.

The connection studied for 360 MW is with a single 115 kV line from the Sumas II site to BPA Bellingham Substation, terminating on a 115 kV breaker. A 115 kV capacitor bank at BPA Bellingham Substation is installed to compensate the large reactive losses in the 115 kV line. The 115 kV line modeled is 22 miles of 2 Tern bundled conductor. The generators supply 368 MW, and the line has real power and reactive losses of 12.7 MW and 97 MVAR. An alternative single conductor might be Jefferson, a 1.6 inch AAC trapezoidal with lower, but adequate ampacity, higher reactance and 1/4 lower resistance.

The 360 MW of the proposed Sumas II generator causes a net increase in flow through the system for during North-to-South NI flows. The impact will be sufficient to require additional lines and some reconfiguration of buses.

A second 230-115 kV transformer must be added at BPA Bellingham or the Sedro-Bellingham #3 & #4 115 kV lines must be rebuilt to a higher capacity. The current Sedro-Bellingham RAS trips the lines for certain outages. If this happens, a single 230-115 kV transformer at BPA Bellingham would severely overload due to power flowing from the 115 kV side to the 230 side, and south on the Bellingham-Sedro 230 kV line. The second transformer reduces loading on the Sedro-Bellingham #3 & #4 115 kV lines, but also mitigates overloading on a single Bellingham transformer if the 115 kV lines do trip. A second transformer at BPA Bellingham is less expensive than rebuilding the Sedro-Bellingham 115 kV lines.

The Custer-Murray 230 kV line between its Sedro NT tap point and Murray is constructed with 795 Drake conductor, rated for 100C. This line is at 102% for a breaker failure at Horse Ranch substation. With the addition of 360 MW, it overloads to 120% for the same outage. One option is to rebuild the line from Sedro NT tap point to Murray, a distance of 26 miles. A difficulty with this option is that other lines overload from Murray to Snohomish to Bothell Substations, as well as the March Point-Beverly 115 kV line.

Another option is to rebuild the March Point-Beverly 115 kV line between Beaver Lake and Horse Ranch, and to construct new 230 and 115 kV lines back to Sedro Woolley. This results in a Sedro-March Point 115 kV line and a new second Sedro-Horse Ranch 230 kV line. The line configuration used was 2-Tern bundled conductor with restricted H-frame construction. For cost purposes, it is assumed that the existing 115 kV line will have to be replaced, and the new line moved in from the edge of the right-of-way. Two breakers are added to the Horse Ranch Substation. The Snohomish-Beverly #3 & #4 115 kV lines are upgraded to 100C because the March Point-Beverly 115 kV line no longer brings power to the Beverly 115 kV bus.

Either of the Bothell-Snoking #1 & #2 230 kV lines overloads to 113% of its 100C rating for the loss of the other line. To resolve these overloads, the lines must either be uprated to 110C, rebuilt with higher capacity conductors, or a parallel line constructed. BPA has not uprated any of their lines above 100C as a practice to avoid conductor loss of life. If BPA were able to

economically uprate these lines (not rebuilding them) then the following line uprates would be required. The Cottage Brook-Fall City 115 kV line must be uprated from 55C to 75C.

If the Bothell-Snoking #1 & #2 230 kV lines cannot be uprated above 100C, and if they were rebuilt, the impedance would likely be lower with larger conductors, and the Snoking-Maple Valley #1 & #2 230 kV lines may then overload. The cost to rebuild the Snoking-Maple Valley lines will be high, because they are 25 miles long on double circuit steel towers. The Bothell-Snoking #1 & #2 230 kV lines are 3.7 miles long. With this option, the same 115 kV lines must be uprated. This option is described in the cost estimates for Phase 3. A disadvantage with upgrading the lines to a higher temperature is that they are only marginally adequate with all lines in service. There is little room to allow for maintenance, and generation and imports will need to be curtailed more often.

The third option for the Bothell-Snoking #1 & #2 lines is to reduce their loading by building another line parallel to them. A parallel line that could be converted for 230 kV use would be either the #1 or #2 circuit of the Sammamish-Lakeside and Lakeside-Talbot 115 kV lines. With this option, overloads on the Cottage Brook-Fall City 115 kV line can be mitigated, and a shorter distance of the Beverly-Cottage Brook 115 kV line must be uprated. This option is described more fully in the following section IV on Sumas II at 720 MW.

The Bothell-Sammamish 230 kV line has one Tern 795 conductor rated for 100C. It can be reconductored, or a second conductor can be added. If a second conductor is added, it will have a lower impedance, with twice the capacity, relieving load on the Bothell-Snoking and Snoking-Maple Valley #1 & #2 230 kV lines. Any change may require moving the outside pole of the H-frame structures to the inside pole position to gain sufficient distance from the outside edge of the right-of-way. An alternative to retaining the H-frame configuration would be to use tall single steel poles at a much higher cost. If the double line outage is mitigated by other measures, there are other overloads at Monroe Substation that overload this line.

# IV. Improvements for Sumas II at 720 MW - Phase 3.

To connect an additional 360 MW of generation form Sumas II, a 115 kV line was modeled as constructed between the Sumas II site and Portal Way. The line is constructed with the same conductor and framing as the Sumas II-BPA Bellingham 115 kV line. A second 230-115 kV transformer is needed at Portal Way, and a 115 kV capacitor bank is added to the Portal Way bus.

Loading on the Custer-Murray 230 kV line between Sedro NT and Murray remains within its rating due to the second Sedro-Horse Ranch 230 kV circuit. To mitigate flows on the Monroe-Snohomish and Snohomish-Bothell #1 & #2 230 kV lines, the Snohomish-Boeing 115 kV line is converted to 230, tapped to Snohomish with a 230 kV breaker, and terminated at Beverly with the existing Horse Ranch-Bothell 230 kV line with a new three breaker 230 kV bus. To convert the line, the Boeing end is re-terminated on a 115 kV breaker at Beverly Park. A 230-115 kV transformer could be installed at Beverly Park Substation if desired by Snohomish PUD. With the addition of a Beverly 230-115 kV transformer, the Beverly-Cottage Brook 115 kV line must be uprated from 75C to 100C.

Ex.		1.	(W	AC	}	4	.)
Page	214						•

Sumas IIc.doc

The Bothell-Snoking 1&2 230 kV lines overload to 118% of their 100C rating, and the Snoking-Talbot North #1 230 kV line overloads to 109% of its 100C rating. The Beverly-Cottage Brook 115 kV line overloads to 118% before uprating, and the Cottage Brook-Fall City 115 kV line overloads to 121% before uprating.

In the Puget Sound area, there are three 500 kV line segments where parallel 500 kV lines are noticeably absent. Only a single line exists between Monroe and Echo Lake, Echo Lake and Raver, and Raver and Paul. BPA is installing a second Echo Lake-Raver 500 kV line to mitigate overloads from outages during South-to-North NI exports.

Two options can be used to mitigate parallel path outages for North-to-South flows with the Sumas II project. One is to construct a second 500 kV line from Monroe to Echo Lake, using the 345 kV line that is energized at 230 kV between Monroe, the proposed Novelty site, and the Echo Lake-Maple Valley 1&2 500 kV lines. A 500-230 kV transformer would be tapped to this line that would supply Novelty-Sammamish 230 kV lines. This would be an alternative to the Snoking 500 kV tap conversion and 500-230 kV transformer at Snoking. It also requires conversion of the Sammamish-Lakeside and Lakeside-Talbot 2 115 kV line to 230 kV. While this line can be constructed on a separate right-of-way from the existing Monroe-Echo Lake 500 kV line, the cost is very high for the benefits provided.

The second option is to convert the Sammamish-Lakeside and Lakeside-Talbot 2 115 kV line to 230 kV. By installing a 230 kV transformer at Lakeside, loading on the Sammamish and Talbot 230-115 kV transformers is reduced. This provides an additional benefit in the winter because currently the Sammamish transformers will exceed their emergency ratings in the winter for an outage of either one. With the Lakeside transformer addition, Sammamish and Talbot transformer overloading is resolved, overloading on the Beverly-Cottage Brook 115 kV line is reduced, and overloading is eliminated on Cottage Brook-Fall City 115 kV line for North-to-South outages.

To convert the Sammamish-Lakeside and Lakeside-Talbot 2 line, the existing conductor must be bundled or replaced. The conductor modeled was Lapwing ACSR with restricted H-frame construction. Lapwing was adequate, but a larger conductor would be preferable for future needs. It is expected that the outside pole nearest the edge of the right-of-way must be moved to become the inside pole to gain sufficient distance from the edge of the right-of-way.

Generation Benefits to South to North Capability:

BPA is heavily focused on Puget Sound area capability to support south to north BCH transfers. They want to achieve 1700 MW West Side south to north capability for all seasons. There are serious problems with facility overloads during south to north exports when generation in Whatcom and Skagit Counties are light. Generation in Whatcom and Skagit Counties directly offset power flowing through King and Snohomish County facilities to Canada. BPA's need for firm south to north capability would be helped if there were generation sources that they could count on running.

# Appendix A. Existing System Overloads.

## 2004 Summer, Heavy Load, North to South Limits

West Side NI at 2850 MW	SCL ②		Generati	on Level	(MW) ③	
Facility Overload ①	Skagit	1896	1541	1129	1186	260
			Percent of			
Portal Way #1 (or #2) 230-115 tx	any	107			,	104
Portal Way - Arco Central 115	650	126	134			
Terrell - PSE Bellingham 115	any		109		107	
BPA Bellingham - Tasco Ref. 115	100		108		110	
BPA Bellingham 230-115 tx	100	152 <b>④</b>	157 ④			
Sedro NT - Murray 230	100	145	130	107	111	
Sedro - Horse Ranch Tap 230	100	114				
March Point - Beverly Park 115	100	126	117		101	
Beverly Park - Cottage Brook 115	100	111	107			
Fall City - Cottage Brook 115	650	129	120	106	106	
Bothell - Sammamish 230	650	121	116	108®	108⑥	
Snoking - Maple Valley #1 230	650	105				
Snoking - Maple Valley #2 230	650	144	135	122	124	
Horse Ranch-Tap of Mon-Snoh 230	100	148	132	105	110	
Snohomish - Bothell #2 230	100	123	117	109	110	
Bothell - Snoking #1 & #2 230	650	140	132	120	121	
Snohomish - Bothell #1 230	100	160	450	440	440	44=
Snohomish - Bothell #2 230	100		152	140	142	117
Bothell - Snoking #2 230		122	118	110	111	
S Tourish Shoking #2 250	650	138	131	118	1.5	

#### Footnotes:

- ① Assumes Sumas II RAS tripping for Monroe-Custer #1 & #2, Monroe-Echo Lake, or Raver-Paul 500 kV outages, and Sumas II RAS tripping connected to Bellingham for Bellingham 230 bus or 230-115 tx outage.
- ② SCL Skagit generation level at highest facility overload (any means that overload is insensitive to SCL Skagit generation).
- 3 Columns are for different combinations of Sumas and Puget generation. Generation levels (MW) 1896 1541 1129 1186 260 Sumas at BPA Bellingham 115 kV 355 355 355 Sumas at Portal Way & 2nd PW 230-115 tx 355 PSE CT's at Whitehorn and Fredonia 412 412 412 PSE cogeneration and hydro 774 774 774 774 260
- Overload is made higher by RAS tripping of Sedro-Bellingham #3 & #4 115 kV on line overload.
- ⑤ Overloads from SCL Bothell 230 kV bus segment outages, before new arrangement.
- 6 Overloads for only Monroe-Snoking-Sammamish 230 kV outage is mitigated by tripping PSE (and SE2) combustion turbines.

Ex. (WAG-4) Page 216 of 219

Sumas IIc.doc

Reference: 04hsnsJun30B

#### 2004 Summer, Light Load, North to South Limits

West Side NI 2850 MW	SCL ②	Gen	eration Le	evel (sum	mer, MW	<b>')</b> ③	
Facility Overload ①	Skagit	1896	1541	1129	1186	260	
		Percent of emergency rating					
Portal Way #1 (or #2) 230-115 tx	any	126					
Portal Way - Arco Central 115	650	150	154		129		
Terrell - PSE Bellingham 115	any		145		154		
BPA Bellingham - Tasco Ref. 115	100		166		160		
BPA Bellingham 230-115 tx	100	115	182 ④				
Sedro NT - Murray 230	100	152	137	113	118		
Sedro - Sedro NT 230	100	133	125		101		
Sedro - Horse Ranch Tap 230	100	115	103				
March Point - Beverly Park 115	100	135	126		110		
Tolt - Cottage Brook 115	650	147	137	124	124		
Bothell - Sammamish 230	650	109	104				
Snoking - Maple Valley #2 230	650	118	110	101	103		
Horse Ranch-Tap of Mon-Snoh 230	100	163	146	118	124		
Snohomish - Bothell #2 230	100	116	110		103		
Bothell - Snoking #1 & #2 230	650	153	145	133	133		
Sedro NT - Murray 230	100	145	131	106	111		
Horse R - Tap of Mon-Snoh 230	100	160	143	115	122		
Snohomish - Bothell #1 230	100	163	155	142	145	117	
Bothell - Snoking #2 230	650	152	144	131	131		

#### Footnotes:

- Assumes Sumas II RAS tripping for Monroe-Custer #1 & #2, Monroe-Echo Lake, or Raver-Paul 500 kV outages, and Sumas II RAS tripping connected to Bellingham for Bellingham 230 bus or 230-115 tx outage.
- ② SCL Skagit generation level at highest facility overload (any means that overload is insensitive to SCL Skagit generation).
- Columns are for different combinations of Sumas and Puget generation. Generation levels (MW) 1896 1541 1129 1186 260 Sumas at BPA Bellingham 115 kV 355 355 355 Sumas at Portal Way & 2nd PW 230-115 tx 355 PSE CT's at Whitehorn and Fredonia 412 412 412 PSE cogeneration and hydro 774 774 774 260
- Overload is made higher by RAS tripping of Sedro-Bellingham #3 & #4 115 kV on line overload.
- ⑤ Overloads from SCL Bothell 230 kV bus segment outages, before new arrangement.

Ex. (WAG-4) Page 218 of 219

Sumas IIc.doc

Reference: 04lsnsJul6B

Ex	_(WAG	-4)
Page 219 of 2	19	

Sumas IIc.doc

# Appendix B. Improvements not related to the Northern Intertie.

The Portal Way-Arco 115 kV line needs to be upgraded from 75C to 90C minimum for an outage of Arco Central-Arco North 115 kV line or a RAS scheme to runback or trip Whitehom and Tenaska Generation.

The March Point-Texaco East 115 kV line needs to be upgraded from 55C to 100C for an outage of the March Point-Texaco West 115 kV line when March Point cogeneration and the Fredonia CT's are running.